Job #: 2044225*00

DRAFT APPENDICES 2020 Urban Water Management Plan Palmdale Water District







Appendix A: UWMP Checklist

Appendix A: UWMP Checklist

Checklist Arranged by Water Code.

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10608.20(e)	Retail suppliers shall provide baseline daily per capita water use, urban water use target, interim urban water use target, and compliance daily per capita water use, along with the bases for determining those estimates, including references to supporting data.	Baselines and Targets	Chapter 5	Section 3.1
10608.22	Retail suppliers' per capita daily water use reduction shall be no less than 5 percent of base daily per capita water use of the 5 year baseline. This does not apply if the suppliers base GPCD is at or below 100.	Baselines and Targets	Section 5.7.2	Section 3.1.1
10608.24(a)	Retail suppliers shall meet their water use target by December 31, 2020.	Baselines and Targets	Section 5.7	Section 3.1.2
10608.24(d)(2)	If the retail supplier adjusts its compliance GPCD using weather normalization, economic adjustment, or extraordinary events, it shall provide the basis for, and data supporting the adjustment.	Baselines and Targets	Sections 5.2 and 5.5.7	Section 3.1.2; Appendix F Table 4-D, Appendix B, Table 7-5

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10608.26(a)	Retail suppliers shall conduct a public hearing to discuss adoption, implementation, and economic impact of water use targets.	Plan Adoption, Submittal, and Implementation	Chapter 10	Appendix C
10608.4	Retail suppliers shall report on their progress in meeting their water use targets. The data shall be reported using a standardized form.	Baselines and Targets	Section 5.8 and App E	Section 3.12
10620(b)	Every person that becomes an urban water supplier shall adopt an urban water management plan within one year after it has become an urban water supplier.	Plan Preparation	Section 2.1	Section 1.1
10620(d)(2)	Coordinate the preparation of its plan with other appropriate agencies in the area, including other water suppliers that share a common source, water management agencies, and relevant public agencies, to the extent practicable.	Plan Preparation	Section 2.5.2	Section 1.5
10620(f)	Describe water management tools and options to maximize resources and minimize the need to import water from other regions.	Water Supply Reliability Assessment	Section 7.4	Section 4.2.3.5
10621(b)	Notify, at least 60 days prior to the public hearing, any city or county within which the supplier provides water that the urban water supplier will be reviewing the plan and considering amendments or changes to the plan.	Plan Adoption, Submittal, and Implementation	Section 10.2.1	Appendix C

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10621(f)	Each urban water supplier shall update and submit its 2020 plan to the department by July 1, 2021.	Plan Adoption, Submittal, and Implementation	Sections 10.3.1 and 10.4	Appendix C
10630.5	Each plan shall include a simple description of the supplier's plan including water availability, future requirements, a strategy for meeting needs, and other pertinent information.	Summary	Chapter 1	Executive Summary
10631(a)	Describe the water supplier service area.	System Description	Section 3.1	Section 1.6.1
10631(a)	Describe the climate of the service area of the supplier.	System Description	Section 3.3	Section 1.9
10631(a)		System Description and Baselines and Targets	Sections 3.4 and 5.4	Section 1.7.1
10631(a)	Provide population projections for 2025, 2030, 2035, 2040 and optionally 2045.	System Description	Section 3.4	Section 1.7.1
	Describe other social, economic, and demographic factors affecting the supplier's water management planning.	System Description	Section 3.4	Section 1.7.2

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10631(a)	Describe the land uses within the service area.	System Description	Section 3.5	Section 1.8
10631(b)	Identify and quantify the existing and planned sources of water available for 2020, 2025, 2030, 2035, 2040 and optionally 2045.	System Supplies	Section 6.2.8	Section 4.1
10631(b)	Indicate whether groundwater is an existing or planned source of water available to the supplier.	System Supplies	Section 6.2	Section 4.2.1
10631(b)(1)	Provide a discussion of anticipated supply availability under a normal, single dry year, and a drought lasting five years, as well as more frequent and severe periods of drought.	System Supplies	Section 6.2	Section 4.6
10631(b)(2)	When multiple sources of water supply are identified, describe the management of each supply in relationship to other identified supplies.	System Supplies	Section 6.1	Section 4.2.3.4
10631(b)(3)	Describe measures taken to acquire and develop planned sources of water.	System Supplies	Section 6.1	Section 4.3.2
10631(b)(4)(A)	Indicate whether a groundwater sustainability plan or groundwater management plan has been adopted by the water supplier or if there is any other specific authorization for groundwater management. Include a copy of the plan or authorization.	System Supplies	Section 6.2.2	Section 4.2.1.3

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10631(b)(4)(B)	Describe the groundwater basin.	System Supplies	Section 6.2.2	Section 4.2.1.1
10631(b)(4)(B)	Indicate if the basin has been adjudicated and include a copy of the court order or decree and a description of the amount of water the supplier has the legal right to pump.	System Supplies	Section 6.2.2	Section 4.2.1.3, Appendix G
10631(b)(4)(B)	For unadjudicated basins, indicate whether or not the department has identified the basin as a high or medium priority. Describe efforts by the supplier to coordinate with sustainability or groundwater agencies to achieve sustainable groundwater conditions.	System Supplies	Section 6.2.3	N/A
10631(b)(4)(C)	Provide a detailed description and analysis of the location, amount, and sufficiency of groundwater pumped by the urban water supplier for the past five years	System Supplies	Section 6.2.4	Section 4.2.1.2
10631(b)(4)(D)	Provide a detailed description and analysis of the amount and location of groundwater that is projected to be pumped.	System Supplies	Section 6.2	Section 4.2.1.3
10631(c)	Describe the opportunities for exchanges or transfers of water on a short-term or long- term basis.	System Supplies	Section 6.7	Section 4.3.1
10631(d)(1)	Quantify past, current, and projected water use, identifying the uses among water use sectors.	System Water Use	Section 4.2	Section 4.1, 4.2.1.2, 4.2.2.2, 4.2.3.1

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10631(d)(3)(A)	Report the distribution system water loss for each of the 5 years preceding the plan update.	System Water Use	Section 4.3	Section 2.2.2
10631(d)(3)(C)	Retail suppliers shall provide data to show the distribution loss standards were met.	System Water Use	Section 4.2	Section 2.2.2
10631(e)(1)	Retail suppliers shall provide a description of the nature and extent of each demand management measure implemented over the past five years. The description will address specific measures listed in code.	Demand	Sections 9.2 and 9.3	Section 8.2
10631(f)	Describe the expected future water supply projects and programs that may be undertaken by the water supplier to address water supply reliability in average, single-dry, and for a period of drought lasting 5 consecutive water years.	System Supplies	Section 6.8	Section 7.6
10631(g)	Describe desalinated water project opportunities for long-term supply.	System Supplies	Section 6.6	Section 4.3.3
10631(h)	Retail suppliers will include documentation that they have provided their wholesale supplier(s) - if any - with water use projections from that source.	System Supplies	Section 2.5.1	Appendix D
10631.1(a)	Include projected water use needed for lower income housing projected in the service area of the supplier.	System Water Use	Section 4.5	Section 2.5

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10631.2(a)	The UWMP must include energy intensity information as stated in the code.		Section 6.4 and Appendix O	Section 4.6
10632(a)	Provide a water shortage contingency plan (WSCP) with specified elements below.	Water Shortage Contingency Planning	Chapter 8	Appendix I
10632(a)(2)(A)	Provide the written decision-making process and other methods that the supplier will use each year to determine its water reliability.		Section 8.2	Appendix I
10632(a)(2)(B)	Provide data and methodology to evaluate the supplier's water reliability for the current year and one dry year pursuant to factors in the code.	Water Shortage Contingency Planning	Section 8.2	Appendix I
10632(a)(3)(A)	Define six standard water shortage levels of 10, 20, 30, 40, 50 percent shortage and greater than 50 percent shortage. These levels shall be based on supply conditions, including percent reductions in supply, changes in groundwater levels, changes in surface elevation, or other conditions. The shortage levels shall also apply to a catastrophic interruption of supply.	Water Shortage Contingency Planning	Section 8.3	Appendix I
10632(a)(3)(B)	Suppliers with an existing water shortage contingency plan that uses different water shortage levels must cross reference their categories with the six standard categories.	Water Shortage Contingency Planning	Section 8.3	Appendix I
10632(a)(4)(A)	Suppliers with water shortage contingency plans that align with the defined shortage levels must specify locally appropriate supply augmentation actions.	Water Shortage Contingency Planning	Section 8.4	Appendix I

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
	Specify locally appropriate demand reduction actions to adequately respond to shortages.	Water Shortage Contingency Planning		Appendix I
10632(a)(4)(B)			Section 8.4	у пропаж т
10632(a)(4)(C)	Specify locally appropriate operational changes.	Water Shortage Contingency Planning	Section 8.4	Appendix I
10632(a)(4)(D)	Specify additional mandatory prohibitions against specific water use practices that are in addition to state-mandated prohibitions are appropriate to local conditions.	Water Shortage Contingency Planning	Section 8.4	Appendix I
10632(a)(4)(E)	Estimate the extent to which the gap between supplies and demand will be reduced by implementation of the action.	Water Shortage Contingency Planning	Section 8.4	Appendix I
10632(a)(5)(A)	Suppliers must describe that they will inform customers, the public and others regarding any current or predicted water shortages.	Water Shortage Contingency Planning	Section 8.5	Appendix I
10632(a)(5)(B) 10632(a)(5)(C)	Suppliers must describe that they will inform customers, the public and others regarding any shortage response actions triggered or anticipated to be triggered and other relevant communications.	Water Shortage Contingency Planning	Section 8.5, 8.6	Appendix I
	Describe the legal authority that empowers the supplier to enforce shortage response actions.	Water Shortage Contingency Planning		Appendix I
10632(a)(7)(A)			Section 8.7	
10632(a)(7)(B)	Provide a statement that the supplier will declare a water shortage emergency Water Code Chapter 3.	Water Shortage Contingency Planning	Section 8.7	Appendix I

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10632(a)(7)(C)	Provide a statement that the supplier will coordinate with any city or county within which it provides water for the possible proclamation of a local emergency.	Water Shortage Contingency Planning	Section 8.7	Appendix I
10632(a)(8)(A)	Describe the potential revenue reductions and expense increases associated with activated shortage response actions.	Water Shortage Contingency Planning	Section 8.8	Appendix I
10632(a)(8)(B)	Provide a description of mitigation actions needed to address revenue reductions and expense increases associated with activated shortage response actions.	Water Shortage Contingency Planning	Section 8.8	Appendix I
10632(a)(8)(C)	Describe the cost of compliance with Water Code Chapter 3.3: Excessive Residential Water Use During Drought.	Water Shortage Contingency Planning	Section 8.8	Appendix I
10632(a)(9)	Retail suppliers must describe the monitoring and reporting requirements and procedures that ensure appropriate data is collected, tracked, and analyzed for purposes of monitoring customer compliance.	Water Shortage Contingency Planning	Section 8.9	Appendix I
10632(a)(10)	Describe reevaluation and improvement procedures for monitoring and evaluation the water shortage contingency plan to ensure risk tolerance is adequate and appropriate water shortage mitigation strategies are implemented.	Water Shortage Contingency Planning	Section 8.10	Appendix I
10632(b)	Analyze and define water features that are artificially supplied with water, including ponds, lakes, waterfalls, and fountains, separately from swimming pools and spas.	Water Shortage Contingency Planning	Section 8.11	Appendix I

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10633(b)	Describe the quantity of treated wastewater that meets recycled water standards, is being discharged, and is otherwise available for use in a recycled water project.	System Supplies (Recycled Water)	Section 6.2	Section 5.3
10633(c)	Describe the recycled water currently being used in the supplier's service area.	System Supplies (Recycled Water)	Section 6.2	Section 5.4
10633(d)	Describe and quantify the potential uses of recycled water and provide a determination of the technical and economic feasibility of those uses.	System Supplies (Recycled Water)	Section 6.2	Section 5.5.2
10633(e)	Describe the projected use of recycled water within the supplier's service area at the end of 5, 10, 15, and 20 years, and a description of the actual use of recycled water in comparison to uses previously projected.	System Supplies (Recycled Water)	Section 6.2	Section 5.5, Table 6-4
10633(f)	Describe the actions which may be taken to encourage the use of recycled water and the projected results of these actions in terms of acre-feet of recycled water used per year.	System Supplies (Recycled Water)	Section 6.2	Section 5.5.53
	Provide a plan for optimizing the use of recycled water in the supplier's service area.	System Supplies (Recycled Water)	Section 6.2	Section 5.5.2
10633(g)	Provide information on the quality of existing sources of water available to the supplier and the			
10634	manner in which water quality affects water management strategies and supply reliability	Water Supply Reliability Assessment	Chapter 7	Section 6.2, 6.3

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10635(a)	the water supplier with the total	Water Supply Reliability Assessment	Section 7.3	Section 7.3, 7.4, 7.5
10635(b)	Provide a drought risk assessment as part of information considered in developing the demand management measures and water supply projects.	Water Supply Reliability Assessment	Section 7.3	Section 7.6
10635(b)(1)	Include a description of the data, methodology, and basis for one or more supply shortage conditions that are necessary to conduct a drought risk assessment for a drought period that lasts 5 consecutive years.	Water Supply Reliability Assessment	Section 7.3	Section 7.6.1
10635(b)(2)	Include a determination of the reliability of each source of supply under a variety of water shortage conditions.	Water Supply Reliability Assessment	Section 7.3	Section 7.1.1, 7.1.2, 7.1.3
10635(b)(3)	Include a comparison of the total water supply sources available to the water supplier with the total projected water use for the drought period.	Water Supply Reliability Assessment	Section 7.3	Section 6.2.4
10635(b)(4)	Include considerations of the historical drought hydrology, plausible changes on projected supplies and demands under climate change condition, anticipated regulatory changes, and other locally applicable criteria.	Water Supply Reliability Assessment	Section 7.3	Section 7

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10635(c)	Provide supporting documentation that Water Shortage Contingency Plan has been, or will be, provided to any city or county within which it provides water, no later than 60 days after the submission of the plan to DWR.	Plan Adoption, Submittal, and Implementation	Sections 8.12, 10.4	Section 1.2.2
10642	Provide supporting documentation that the water supplier has encouraged active involvement of diverse social, cultural, and economic elements of the population within the service area prior to and during the preparation of the plan and contingency plan.	Plan Preparation	Section 2.6	Section 1.7.2
10642	Provide supporting documentation that the urban water supplier made the plan and contingency plan available for public inspection, published notice of the public hearing, and held a public hearing.	Plan Adoption, Submittal, and Implementation	Sections 10.2.2, 10.3, and 10.5	Section 1.4.2
10642	The water supplier is to provide the time and place of the hearing to	Plan Adoption, Submittal, and Implementation	Section 10.2	Section 1.4.2
10642		Plan Adoption, Submittal, and Implementation	Section 10.3.1	Section 1.4.3
10644(a)	Provide supporting documentation that the urban water supplier has submitted this UWMP to the California State Library.	Plan Adoption, Submittal, and Implementation	Section 10.5	Section 1.4.4
10644(a)(1)	Provide supporting documentation that the urban water supplier has submitted this UWMP to any city or county within which the supplier provides water no later than 30 days after adoption.	Plan Adoption, Submittal, and Implementation	Section 10.5	Section 1.4.4

Water Code Section	Summary as Applies to UWMP	Subject	2020 Guidebook Location	2020 UWMP Location
10644(a)(2)	The plan, or amendments to the plan, submitted to the department shall be submitted electronically.	Submittal, and	Sections 10.4.1 and 10.4.2	Section 1.4.4
10645(a)	Provide supporting documentation that, not later than 30 days after filing a copy of its plan with the department, the supplier has or will make the plan available for public review during normal business hours.	Plan Adoption, Submittal, and Implementation	Section 10.5	Section 1.4.4
10645(b)	department, the supplier has or will	Plan Adoption, Submittal, and Implementation	Section 10.5	Appendix C



Appendix B: Submittal Tables

Submittal Table 2-1 Retail Only: Public Water Systems						
Public Water System Number	Public Water System Name	Number of Municipal Connections 2020	Volume of Water Supplied 2020 *			
Add additional rows as need	ed					
CA1910102	Palmdale Water District	26,869	20,511			
	TOTAL	26,869	20,511			

^{*} Units of measure (AF, CCF, MG) must remain consistent throughout the UWMP as reported in Table 2-3.

Submittal '	Submittal Table 2-2: Plan Identification					
Select Only One	Type of Plan		Name of RUWMP or Regional Alliance if applicable (select from drop down list)			
Ø	Individual	UWMP				
	0	Water Supplier is also a member of a RUWMP				
	0	Water Supplier is also a member of a Regional Alliance				
0	Regional ((RUWMP)	Jrban Water Management Plan				

Submitta	Submittal Table 2-3: Supplier Identification			
Type of Su	upplier (select one or both)			
	Supplier is a wholesaler			
V	Supplier is a retailer			
Fiscal or C	Calendar Year (select one)			
v	UWMP Tables are in calendar years			
	UWMP Tables are in fiscal years			
If using fis	scal years provide month and date that the fiscal year begins (mm/dd)			
Units of measure used in UWMP * (select from drop down)				
Unit	AF			

Submittal Table 2-4 Retail: Water Supplier Information Exchange
The retail Supplier has informed the following wholesale supplier(s) of projected water use in accordance with Water Code Section 10631.
Wholesale Water Supplier Name
Add additional rows as needed
NOTES: Not applicable. PWD does not receive water from a wholesale supplier.
PWD is a direct contractor of the State Water Project.

Submittal Ta	able 3-1 Reta	ail: Populatio	on - Current	and Projecte	ed	
Population	2020	2025	2030	2035	2040	2045(opt)
Served	126,002	128,998	132,003	138,554	145,962	153,766

Submittal Table 4-1 Retail: Demands for Potable and Non-Potable 1 Water - Actual					
Use Type	2020 Actual				
Drop down list May select each use multiple times These are the only Use Types that will be recognized by the WUEdata online submittal tool	Additional Description (as needed)	Level of Treatment When Delivered Drop down list	Volume ²		
Add additional rows as needed					
Single Family			11,757		
Multi-Family			1,555		
Commercial			1,190		
Industrial			1,637		
Institutional/Governmental					
Landscape			1,040		
Sales/Transfers/Exchanges to other Suppliers			1,301		
Losses			1,997		
Other			34		
		TOTAL	20,511		

¹ Recycled water demands are NOT reported in this table. Recycled water demands are reported in Table 6-4. Units of measure (AF, CCF, MG) must remain consistent throughout the UWMP as reported in Table 2-3.

Submittal Table 4-2 Retail: Use for Potable and Non-Potable Water - Projected

Use Type		Rep	Projected Water Use ² Report To the Extent that Records are Available			
<u>Drop down list</u> May select each use multiple times These are the only Use Types that will be recognized by the WUEdata online submittal tool	Additional Description (as needed)	2025	2030	2035	2040	2045 (opt)
Add additional rows as needed						
Single Family		11,460	11,730	12,310	12,970	13,660
Multi-Family		1,450	1,480	1,560	1,640	1,730
Commercial	(a)	1,170	1,240	1,390	1,550	1,730
Industrial		1,350	1,390	1,480	1,590	1,700
Institutional/Governmental						
Landscape		1,050	1,130	1,300	1,490	1,690
Sales/Transfers/Exchanges to other Suppliers		1,300	1,300	1,300	1,300	1,300
Losses	(b)	1,900	2,000	2,100	2,200	2,400
Other	(c)	40	40	40	40	40
	TOTAL	19,720	20,310	21,480	22,780	24,250

Submittal Table 4-3 Retail: Total Water Use (Potable and Non-Potable)							
	2020	2025	2030	2035	2040	2045 (opt)	
Potable Water, Raw, Other Non-potable From Tables 4-1R and 4-2 R	20,511	19,720	20,310	21,480	22,780	24,250	
Recycled Water Demand ¹ From Table 6-4	70	500	1,000	1,500	2,000	2,000	
Optional Deduction of Recycled Water Put Into Long- Term Storage ²							
TOTAL WATER USE	20,581	20,220	21,310	22,980	24,780	26,250	

Submittal Table 4-4 Retail: Last Five Years of Water Loss Audit Reporting

Reporting Period Start Date (mm/yyyy)	Volume of Water Loss ^{1,2}
01/2015	1297
01/2016	1559
01/2017	1808
01/2018	1723
01/2019	1351

¹ Taken from the field "Water Losses" (a combination of apparent losses and real losses) from the AWWA worksheet.

Units of measure (AF, CCF, MG) must remain consistent throughout the UWMP as reported in Table 2-3.

Submittal Table 4-5 Retail Only: Inclusion in Water Use Projections	
Are Future Water Savings Included in Projections?	
(Refer to Appendix K of UWMP Guidebook)	
Drop down list (y/n)	No
If "Yes" to above, state the section or page number, in the cell to the right, where citations of the codes, ordinances, or otherwise are utilized in demand projections are found.	
Are Lower Income Residential Demands Included In Projections? Drop down list (y/n)	Yes

Submittal Table 5-1 Baselines and Targets Summary From SB X7-7 Verification Form

Retail Supplier or Regional Alliance Only

Baseline Period	Start Year *	End Year *	Average Baseline GPCD*	Confirmed 2020 Target*
10-15 year	SB X7-7 Table 1	SB X7-7 Table 1	SB X7-7 Table 5	SB X7-7
5 Year	SB X7-7 Table 1	SB X7-7 Table 1	SB X7-7 Table 5	Table 7-F

^{*}All cells in this table should be populated manually from the supplier's SBX7-7 Verification Form and reported in Gallons per Capita per Day (GPCD)

Submittal Table 5-2: 2020 Compliance SB X7-7 2020 Compliance Form

Retail Supplier or Regional Alliance Only

	2020 GPCD			Did Supplier
Actual 2020 GPCD*	2020 TOTAL Adjustments*	Adjusted 2020 GPCD* (Adjusted if applicable)	2020 Confirmed Target GPCD*	Achieve Targeted Reduction for 2020? Y/N
SB X7-7 Table 9	SB X7-7 Table 9	SB X7-7 Table 9	SB X7-7 Table 9	SB X7-7 Table 9

From

^{*}All cells in this table should be populated manually from the supplier's SBX7-7 2020 Compliance Form and reported in Gallons per Capita per Day (GPCD)

Submittal Table 6-1 Retail: Groundwater Volume Pumped										
	Supplier does not pump groundwater. The supplier will not complete the table below.									
п	All or part of the groundwater d	escribed belo	w is desalinat	ed.						
Groundwater Type Drop Down List May use each category multiple times	Location or Basin Name	2016*	2017*	2018*	2019*	2020*				
Add additional rows as need	ded									
Alluvial Basin	Antelope Valley Basin	8473	4355	6058	4425	7599				
	TOTAL	8,473	4,355	6,058	4,425	7,599				

Submittal Table 6-2 Retail: Wastewater Collected Within Service Area in 2020 There is no wastewater collection system. The supplier will not complete the table below. Percentage of 2020 service area covered by wastewater collection system (optional)

Percentage of 2020 service area population covered by wastewater collection system (optional)

W	astewater Collection	on		Recipient of Collected Wastewater				
Name of Wastewater Collection Agency	Wastewater Volume Metered or Estimated? Drop Down List	Volume of Wastewater Collected from UWMP Service Area 2020 *	Name of Wastewater Treatment Agency Receiving Collected Wastewater	Treatment Plant Name	Is WWTP Located Within UWMP Area? Drop Down List	Is WWTP Operation Contracted to a Third Party? (optional) Drop Down List		
Los Angeles County Sanitation Districts (LACSD)	Metered	12,140	LACSD District No. 20	Palmdale Water Reclamation Plant (WRP)	Yes	No		
Service Ar	ler Collected from ea in 2020: (AF, CCF, MG) must l	12,140						

^{*} Units of measure (AF, CCF, MG) must remain consistent throughout the UWMP as reported in Table 2-3.

Submittal Table 6	Submittal Table 6-3 Retail: Wastewater Treatment and Discharge Within Service Area in 2020										
No wastewater is treated or disposed of within the UWMP service area. The supplier will not complete the table below.											
					Does This				2020 volumes		
Wastewater Treatment Plant Name	Discharge Location Name or Identifier	Description	Wastewater Discharge ID Number (optional) ²	Method of Disposal Drop down list	Plant Treat Wastewater Generated Outside the Service Area? Drop down list	Treatment Level Drop down list	Wastewater Treated	Discharged Treated Wastewater	Recycled Within Service Area	Recycled Outside of Service Area	Instream Flow Permit Requirement
Pallinuale Water		Agricultural		Other	Yes	Tertiary	12,140	10,770	110		
1100101010101010101010101010101010101010		100.00.00									
	·	-						-			·
						Total	12,140	10,770	110	0	0

Submittal Table 6-4 Retail: Recycled Water Direct Beneficial Uses Within Service Area										
Recycled water is not used and is not planned for use within the service area of the supplier. The supplier will not complete the table below.										
Name of Supplier Producing (Treating) the Recycled	Water:	Los Angeles County Sanit	ation Districts (LACSD)							
Name of Supplier Operating the Recycled Water Dist	ribution System:									
Supplemental Water Added in 2020 (volume) Include	e units									
Source of 2020 Supplemental Water										
Beneficial Use Type Insert additional rows if needed.	Potential Beneficial Uses of Recycled Water (Describe)	Amount of Potential Uses of Recycled Water (Quantity) Include volume units ¹	General Description of 2020 Uses	Level of Treatment Drop down list	2020 ¹	2025 ¹	2030 ¹	2035 ¹	2040 ¹	2045 ¹ (opt)
Agricultural irrigation										
Landscape irrigation (exc golf courses)					70					
Golf course irrigation										
Commercial use										
Industrial use										
Geothermal and other energy production										
Seawater intrusion barrier										
Recreational impoundment										
Wetlands or wildlife habitat										
Groundwater recharge (IPR)						500	1,000	1,500	2,000	2,000
Reservoir water augmentation (IPR)										
Direct potable reuse										
Other (Description Required)										
				Total:	70	500	1,000	1,500	2,000	2,000
			202	0 Internal Reuse						

Submittal Table 6-5 Retail: 2015 UWMP Recycled Water Use Projection Compared to 2020 Actual

Recycled water was not used in 2015 nor projected for use in 2020. The supplier will not complete the table below. If recycled water was not used in 2020, and was not predicted to be in 2015, then check the box and do not complete the table.

Beneficial Use Type	2015 Projection for 2020 ¹	2020 Actual Use ¹
Insert additional rows as needed.		
Agricultural irrigation		
Landscape irrigation (exc golf courses)	1,000	70
Golf course irrigation		
Commercial use		
Industrial use		
Geothermal and other energy production		
Seawater intrusion barrier		
Recreational impoundment		
Wetlands or wildlife habitat		
Groundwater recharge (IPR)		
Reservoir water augmentation (IPR)		
Direct potable reuse		
Other (Description Required)		
Total	1,000	70

Submittal Table 6-6 R	Submittal Table 6-6 Retail: Methods to Expand Future Recycled Water Use						
	Supplier does not plan to expand recycled water use in the future. Supplier will not complete the table below but will provide narrative explanation.						
	Provide page location of narrative in UWMP						
Nome of Action	Description	Planned	Expected Increase in				
Name of Action	Description	Recycled Water Use *					
Add additional rows as nee	Add additional rows as needed						
Palmdale Regional Water Augmentation Project	The goal of the PRWAP is the beneficial use of 5,325 AFY of recycled water for either surface or groundwater augmentation to benefit the region. PRWAP is a solution that is drought resilient, provides local control of water resources, and helps meet future demands of PWD	2025	5,325				
Total 5,325							
*Units of measure (AF, CCF, MG) must remain consistent throughout the UWMP as reported in Table 2-3.							

Submittal Table 6-7 Retail: Expected Future Water Supply Projects or Programs							
	No expected future supply. Supplier wil			t provide a quantifiab	le increase to the ag	ency's water	
⊻	Some or all of the supplier's future water supply projects or programs are not compatible with this table and are described in a narrative format.						
Page 4-14	Provide page location of narrative in the UWMP						
Name of Future Projects or Programs	Joint Project with	other suppliers?	Description (if needed)	Planned Implementation Year	Planned for Use in Year Type Drop Down List	Expected Increase in Water Supply to Supplier*	
	Drop Down List (y/n)	If Yes, Supplier Name			2700 201111 2101	This may be a range	
Add additional rows as need	Add additional rows as needed						

Submittal Table 6-8 Retail: Water Supplies — Actual						
Water Supply		2020				
Drop down list May use each category multiple times.These are the only water supply categories that will be recognized by the WUEdata online submittal tool	Additional Detail on Water Supply	Actual Volume*	Water Quality Drop Down List	Total Right or Safe Yield* (optional)		
Add additional rows as needed						
Groundwater (not desalinated)	Antelope Valley Basin	7,600	Drinking Water			
Groundwater (not desalinated)	Return Flow Credit	4,090	Drinking Water			
Groundwater (not desalinated)	Groundwater Banking	0	Drinking Water			
Surface water (not desalinated)	Littlerock Reservoir	4,540	Drinking Water			
Purchased or Imported Water	SWP Table A	5,695	Drinking Water			
Purchased or Imported Water	Butte Transfer Agreement	1,320	Drinking Water			
Recycled Water		70	Other Non-Potable Water			
	Total	23,315		0		
*Units of measure (AF, CCF, MG) n	nust remain consistent throug	ghout the UWMP as re	ported in Table 2-3.			

NOTES:

Submittal Table 6-9 Retail: Water Supplies — Projected											
Water Supply			Projected Water Supply * Report To the Extent Practicable								
Drop down list May use each category multiple times.	Additional Detail on	20	25	20	30	2035		2040		2045 (opt)	
These are the only water supply categories that will be recognized by the WUEdata online submittal tool	Additional Detail on Water Supply	Reasonably Available Volume	Total Right or Safe Yield (optional)	Reasonably Available Volume	Total Right or Safe Yield (optional)	Reasonably Available Volume	Total Right or Safe Yield (optional)	Reasonably Available Volume	Total Right or Safe Yield (optional)	Reasonably Available Volume	Total Right or Safe Yield (optional)
Add additional rows as needed											
Groundwater (not desalinated)	Antelope Valley Basin	4,220		2,770		2,770		2,770		2,770	
Groundwater (not desalinated)	Return Flow Credit	5,000		5,000		5,000		5,000		5,000	
Groundwater (not desalinated)	Groundwater or Surface Water Augmentation	5,325		5,325		5,325		5,325		5,325	
Surface water (not	Littlerock Reservoir	4,000		4,000		4,000		4,000		4,000	
Purchased or Imported Water	SWP table A	12,030		11,720		11,400		11,080		11,080	
Purchased or Imported Water 1	Butte Transfer Agreement	5,650		5,500		5,350		5,200		5,200	
Recycled Water	LACSD	500		1,000		1,500		2,000		2,000	
	-	·				·		·		·	
	Total	36,725	0	35,315	0	35,345	0	35,375	0	35,375	0
*Units of measure (AF, CCF, MG) n	nust remain consistent throug		as reported in Ta								

Submittal Table 7-1 Retail: Basis of Water Year Data (Reliability Assessment)						
		Available Supplies if Year Type Repeats				
Year Type	Base Year If not using a calendar year, type in the last year of the fiscal, water year, or range of years, for example, water year 2019-2020, use 2020	Quantification of available supplies is not compatible with this table and is provided elsewhere in the UWMP. Quantification of available supplies is provided in this table as either volume only, percent only, or both.				
		Volume Available * % of Average Supply				
Average Year	1922-2003	21300 100%				
Single-Dry Year	1977	2130 10%				
Consecutive Dry Years 1st Year	1988	2130 10%				
Consecutive Dry Years 2nd Year	1989	8733 41%				
Consecutive Dry Years 3rd Year	1990	2556 12%				
Consecutive Dry Years 4th Year	1991	4260 20%				
Consecutive Dry Years 5th Year	1992	3834 18%				

Supplier may use multiple versions of Table 7-1 if different water sources have different base years and the supplier chooses to report the base years for each water source separately. If a Supplier uses multiple versions of Table 7-1, in the "Note" section of each table, state that multiple versions of Table 7-1 are being used and identify the particular water source that is being reported in each table.

*Units of measure (AF, CCF, MG) must remain consistent throughout the UWMP as reported in Table 2-3.

Submittal Table 7-2 Retail: Normal Year Supply and Demand Comparison						
	2025	2030	2035	2040	2045 (Opt)	
Supply totals (autofill from Table 6-9)	36,725	35,315	35,345	35,375	35,375	
Demand totals (autofill from Table 4-3)	20,220	21,310	22,980	24,780	26,250	
Difference	16,505	14,005	12,365	10,595	9,125	

Submittal Table 7-3 Retail: Single Dry Year Supply and Demand Comparison						
2025 2030 2035 2040 2045 (Opt						
Supply totals*	21,235	20,600	21,410	22,225	22,225	
Demand totals*	20,220	21,310	22,980	24,780	26,250	
Difference	1,015	(710)	(1,570)	(2,555)	(4,025)	

^{*}Units of measure (AF, CCF, MG) must remain consistent throughout the UWMP as reported in Table 2-3.

Submittal Table	Submittal Table 7-4 Retail: Multiple Dry Years Supply and Demand Comparison						
		2025*	2030*	2035*	2040*	2045* (Opt)	
	Supply totals	28,125	26,390	26,105	25,665	25,665	
First year	Demand totals	20,220	21,310	22,980	24,780	26,250	
	Difference	7,905	5,080	3,125	885	(585)	
	Supply totals	28,125	26,390	26,105	25,665	25,665	
Second year	Demand totals	20,220	21,310	22,980	24,780	26,250	
	Difference	7,905	5,080	3,125	885	(585)	
	Supply totals	28,125	26,390	26,105	25,665	25,665	
Third year	Demand totals	20,220	21,310	22,980	24,780	26,250	
	Difference	7,905	5,080	3,125	885	(585)	
	Supply totals	28,125	26,390	26,105	25,665	25,665	
Fourth year	Demand totals	20,220	21,310	22,980	24,780	26,250	
	Difference	7,905	5,080	3,125	885	(585)	
	Supply totals	28,125	26,390	26,105	25,665	25,665	
Fifth year	Demand totals	20,220	21,310	22,980	24,780	26,250	
	Difference	7,905	5,080	3,125	885	(585)	

Submittal Table 7-5: Five-Year Drought Risk Assessment Tables to address Water Code Section 10635(b)

2021	Total
Total Water Use	19,410
Total Supplies	16,450
Surplus/Shortfall w/o WSCP Action	(2,960)
Planned WSCP Actions (use reduction and supply augmentation)	
WSCP - supply augmentation benefit	
WSCP - use reduction savings benefit	4,270
Revised Surplus/(shortfall)	1,310
Resulting % Use Reduction from WSCP action	22%

2022	Total
Total Water Use	19,505
Total Supplies	26,155
Surplus/Shortfall w/o WSCP Action	6,650
Planned WSCP Actions (use reduction and supply augmentation)	
WSCP - supply augmentation benefit	
WSCP - use reduction savings benefit	
Revised Surplus/(shortfall)	6,650
Resulting % Use Reduction from WSCP action	0%

2023	Total
Total Water Use	19,620
Total Supplies	17,475
Surplus/Shortfall w/o WSCP Action	(2,145)
Planned WSCP Actions (use reduction and supply augmentation)	
WSCP - supply augmentation benefit	
WSCP - use reduction savings benefit	4,316
Revised Surplus/(shortfall)	2,171
Resulting % Use Reduction from WSCP action	22%

2024	Total
Total Water Use	19,715
Total Supplies	19,980
Surplus/Shortfall w/o WSCP Action	265
Planned WSCP Actions (use reduction and supply augmentation)	
WSCP - supply augmentation benefit	
WSCP - use reduction savings benefit	
Revised Surplus/(shortfall)	265
Resulting % Use Reduction from WSCP action	0%

Total	2025
20,220	Total Water Use
24,680	Total Supplies
4,460	Surplus/Shortfall w/o WSCP Action
	Planned WSCP Actions (use reduction and supply augmentation)
	WSCP - supply augmentation benefit
	WSCP - use reduction savings benefit
4,460	Revised Surplus/(shortfall)
0%	Resulting % Use Reduction from WSCP action

Submittal Table 8-1 Water Shortage Contingency Plan Levels

Shortage Level	Percent Shortage Range	Shortage Response Actions (Narrative description)
1	Up to 10%	Minor Shortage . A threatened shortage exists and a voluntary consumer demand reduction, up to ten (10%) percent, is requested to make more efficient use of water and to appropriately respond to existing water conditions.
2	Up to 20%	Moderate Shortage. A shortage exists and a mandatory demand reduction, up to twenty (20%) percent, is requested to make more efficient use of water and to appropriately respond to existing water conditions.
3	Up to 30%	Severe Shortage. A severe shortage exists and a mandatory demand reduction, up to thirty (30%) percent, is requested to make more efficient use of water and to appropriately respond to existing water conditions.
4	Up to 40%	Critical Shortage. A critical shortage exists and a mandatory demand reduction, up to forty (40%) percent, is requested to make more efficient use of water and to appropriately respond to existing water conditions.
5	Up to 50%	Emergency Shortage. An emergency shortage exists and a mandatory reduction, up to fifty (50%) percent, is requested to make more efficient use of water and to appropriately respond to existing water conditions.
6	>50%	Catastrophic Failure. A water shortage emergency exists and a mandatory reduction in consumer demand of fifty or more (50%) is necessary to maintain sufficient water supplies for public health and safety.

Submittal Ta	able 8-2: Demand Reduction Actions			
Shortage Level	Demand Reduction Actions Drop down list These are the only categories that will be accepted by the WUEdata online submittal tool. Select those that apply.	How much is this going to reduce the shortage gap? Include units used (volume type or percentage)	Additional Explanation or Reference (optional)	Penalty, Charge, Other Enforcement? For Retail Suppliers On Drop Down List
Add additional	l rows as needed			
1	Expand Public Information Campaign	Up to 10%		No
1	Provide Rebates for Landscape Irrigation Efficiency	Up to 10%		No
2	Provide Rebates for Landscape Irrigation Efficiency	Up to 20%		No
2	Expand Public Information Campaign	Up to 20%		No
2	Implement or Modify Drought Rate Structure or Surcharge	Up to 20%		Yes
3	Expand Public Information Campaign	Up to 30%		No
3	Increase Frequency of Meter Reading	Up to 30%		Yes
3	Provide Rebates on Plumbing Fixtures and Devices	Up to 30%		No
3	Provide Rebates for Landscape Irrigation Efficiency	Up to 30%		No
3	Reduce System Water Loss	Up to 30%		No
3	Increase Water Waste Patrols	Up to 30%		Yes
3	Landscape - Restrict or prohibit runoff from landscape irrigation	Up to 30%		Yes
3	Implement or Modify Drought Rate Structure or Surcharge	Up to 30%		Yes
4	Expand Public Information Campaign	Up to 40%		No
4	Increase Frequency of Meter Reading	Up to 40%		Yes
4	Provide Rebates on Plumbing Fixtures and Devices	Up to 40%		No
4	Provide Rebates for Landscape Irrigation Efficiency	Up to 40%		No
4	Reduce System Water Loss	Up to 40%		No
4	Increase Water Waste Patrols	Up to 40%		Yes
4	Implement or Modify Drought Rate Structure or Surcharge	Up to 40%		Yes
5	Landscape - Restrict or prohibit runoff from landscape irrigation	Up to 50%		Yes
5	Expand Public Information Campaign	Up to 50%		No
5	Increase Frequency of Meter Reading	Up to 50%		Yes

5	Provide Rebates on Plumbing Fixtures and Devices	Up to 50%	No
5	Provide Rebates for Landscape Irrigation Efficiency	Up to 50%	No
5	Reduce System Water Loss	Up to 50%	No
5	Increase Water Waste Patrols	Up to 50%	Yes
5	Implement or Modify Drought Rate Structure or Surcharge	Up to 50%	Yes
6	Landscape - Restrict or prohibit runoff from landscape irrigation	Over 50%	Yes
6	Expand Public Information Campaign	Over 50%	No
6	Increase Frequency of Meter Reading	Over 50%	Yes
6	Provide Rebates on Plumbing Fixtures and Devices	Over 50%	No
6	Provide Rebates for Landscape Irrigation Efficiency	Over 50%	No
6	Reduce System Water Loss	Over 50%	No
6	Increase Water Waste Patrols	Over 50%	Yes
6	Implement or Modify Drought Rate Structure or Surcharge	Over 50%	Yes
6	Moratorium or Net Zero Demand Increase on New Connections	Over 50%	Yes

Shortage Level	Supply Augmentation Methods and Other Actions by Water Supplier Drop down list These are the only categories that will be accepted by the WUEdata online submittal tool	How much is this going to reduce the shortage gap? Include units used (volume type or percentage)	Additional Explanation or Reference (optional)
dd additional row	s as needed		
4	Decrease Line Flushing	5	Decrease water distribution line flushing
5	New recycled water	4500	Expand recycled water Use
5	Transfers	9700	Activate local transfer agreements
4	Stored emergency supply	3000	Increase Lake Palmdale storage

Submittal Table 1 Counties	0-1 Retail: Notificatio	n to Cities and
City Name	60 Day Notice	Notice of Public Hearing
Д	Add additional rows as need	ded
Palmdale	Yes	Yes
Lancaster	Yes	Yes
County Name Drop Down List	60 Day Notice	Notice of Public Hearing
	Add additional rows as need	ded
Los Angeles County	Yes	Yes



Appendix C: Adoption of UWMP





Appendix D: Public Outreach Materials



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Attorneys





October 1, 2020

City of Palmdale – Planning Division 38300 Sierra Hwy # A Palmdale, CA 93550

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

To Whom It May Concern:

The Palmdale Water District (PWD) is undertaking the review, update, and revision of its Urban Water Management Plan. PWD is located in Los Angeles County and serves the residents of the City of Palmdale. The Urban Water Management Planning Act requires every "urban water supplier" of a certain size to prepare and adopt an Urban Water Management Plan (UWMP) at least once every five years. The UWMP is a planning document in which water suppliers evaluate and compare their water supply and reliability to their existing and projected demands. A complete UWMP is necessary for PWD to remain eligible for state drought water bank assistance and is a requirement of state grant and loan funding programs.

The 2020 UWMP will include an update of anticipated water demands in the PWD service area. Concurrent with the UWMP update which will be adding a Seismic Risk Assessment section, PWD will also revise its Water Shortage Contingency Plan (WSCP) and create a new document for the WSCP. PWD is encouraging participation by land use agencies, water use agencies, and other interested parties in the UWMP and WSCP and would like to extend to your agency an opportunity to meet with us and review the various elements of the two documents including assumptions about future population, future water demand, future water supplies, and upcoming water conservation programs.

We anticipate that a draft UWMP and WSCP will be available for public review starting in March 2021. PWD will hold a public hearing in June 2021, prior to adoption of the UWMP and WSCP. Hence, we would like to solicit your input in the near future.

If your agency would like to learn more about the Urban Water Management Plan and Water Shortage Contingency Plan, please contact me at 661-456-1092 or cbolanos@palmdalewater.org no later than November 16, 2021.

Very truly yours,

Claudia Bolanos

Resource and Analytics Supervisor

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October 1, 2020

City of Lancaster – Planning Department 44933 Fern Avenue Lancaster, CA 93534

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

To Whom It May Concern:

The Palmdale Water District (PWD) is undertaking the review, update, and revision of its Urban Water Management Plan. PWD is located in Los Angeles County and serves the residents of the City of Palmdale. The Urban Water Management Planning Act requires every "urban water supplier" of a certain size to prepare and adopt an Urban Water Management Plan (UWMP) at least once every five years. The UWMP is a planning document in which water suppliers evaluate and compare their water supply and reliability to their existing and projected demands. A complete UWMP is necessary for PWD to remain eligible for state drought water bank assistance and is a requirement of state grant and loan funding programs.

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ACWA PROUD MEMBER



October 1, 2020

Los Angeles County Department of Regional Planning 320 W Temple Street Los Angeles, CA 90012

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

To Whom It May Concern:

The Palmdale Water District (PWD) is undertaking the review, update, and revision of its Urban Water Management Plan. PWD is located in Los Angeles County and serves the residents of the City of Palmdale. The Urban Water Management Planning Act requires every "urban water supplier" of a certain size to prepare and adopt an Urban Water Management Plan (UWMP) at least once every five years. The UWMP is a planning document in which water suppliers evaluate and compare their water supply and reliability to their existing and projected demands. A complete UWMP is necessary for PWD to remain eligible for state drought water bank assistance and is a requirement of state grant and loan funding programs.

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PALMDALE WATER DISTRICT

A CENTURY OF SERVICE

October 1, 2020

Littlerock Creek Irrigation District Attn. James Chaisson 35141 87th St E Littlerock, CA 93543

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

To Whom It May Concern:

The Palmdale Water District (PWD) is undertaking the review, update, and revision of its Urban Water Management Plan. PWD is located in Los Angeles County and serves the residents of the City of Palmdale. The Urban Water Management Planning Act requires every "urban water supplier" of a certain size to prepare and adopt an Urban Water Management Plan (UWMP) at least once every five years. The UWMP is a planning document in which water suppliers evaluate and compare their water supply and reliability to their existing and projected demands. A complete UWMP is necessary for PWD to remain eligible for state drought water bank assistance and is a requirement of state grant and loan funding programs.

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Very truly yours,

Claudia Bolanos

Resource and Analytics Supervisor

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PALMDALE WATER DISTRICT

A CENTURY OF SERVICE

October 1, 2020

Los Angeles County Sanitation District No. 20 1955 Workman Mill Road Whittier, CA 90601

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

To Whom It May Concern:

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Very truly yours,

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PALMDALE WATER DISTRICT

A CENTURY OF SERVICE

October 1, 2020

Antelope Valley-East Kern Water Agency Attn. Dwayne Chisam 6500 W Avenue N Palmdale, CA 93551

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

To Whom It May Concern:

The Palmdale Water District (PWD) is undertaking the review, update, and revision of its Urban Water Management Plan. PWD is located in Los Angeles County and serves the residents of the City of Palmdale. The Urban Water Management Planning Act requires every "urban water supplier" of a certain size to prepare and adopt an Urban Water Management Plan (UWMP) at least once every five years. The UWMP is a planning document in which water suppliers evaluate and compare their water supply and reliability to their existing and projected demands. A complete UWMP is necessary for PWD to remain eligible for state drought water bank assistance and is a requirement of state grant and loan funding programs.

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If your agency would like to learn more about the Urban Water Management Plan and Water Shortage Contingency Plan, please contact me at 661-456-1092 or cbolanos@palmdalewater.org no later than November 16, 2021.

Very truly yours,

Claudia Bolanos



A CENTURY OF SERVICE

October 1, 2020

Quartz Hill Water District Attn. Chad Reed 5034 W. Avenue L Quartz Hill, CA 93536

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

To Whom It May Concern:

The Palmdale Water District (PWD) is undertaking the review, update, and revision of its Urban Water Management Plan. PWD is located in Los Angeles County and serves the residents of the City of Palmdale. The Urban Water Management Planning Act requires every "urban water supplier" of a certain size to prepare and adopt an Urban Water Management Plan (UWMP) at least once every five years. The UWMP is a planning document in which water suppliers evaluate and compare their water supply and reliability to their existing and projected demands. A complete UWMP is necessary for PWD to remain eligible for state drought water bank assistance and is a requirement of state grant and loan funding programs.

The 2020 UWMP will include an update of anticipated water demands in the PWD service area. Concurrent with the UWMP update which will be adding a Seismic Risk Assessment section, PWD will also revise its Water Shortage Contingency Plan (WSCP) and create a new document for the WSCP. PWD is encouraging participation by land use agencies, water use agencies, and other interested parties in the UWMP and WSCP and would like to extend to your agency an opportunity to meet with us and review the various elements of the two documents including assumptions about future population, future water demand, future water supplies, and upcoming water conservation programs.

We anticipate that a draft UWMP and WSCP will be available for public review starting in March 2021. PWD will hold a public hearing in June 2021, prior to adoption of the UWMP and WSCP. Hence, we would like to solicit your input in the near future.

If your agency would like to learn more about the Urban Water Management Plan and Water Shortage Contingency Plan, please contact me at 661-456-1092 or cbolanos@palmdalewater.org no later than November 16, 2021.

Very truly yours,

Claudia Bolanos

Resource and Analytics Supervisor

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General Manager

ALESHIRE & WYNDER LLP

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Division 5

DENNIS D. LaMOREAUXGeneral Manager

ALESHIRE & WYNDER LLP Attorneys





PALMDALE WATER DISTRICT

A CENTURY OF SERVICE

October 1, 2020

Rosamond Community Services District Attn. Steve Perez 3179 35th Street West Rosamond, CA 93560

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

To Whom It May Concern:

The Palmdale Water District (PWD) is undertaking the review, update, and revision of its Urban Water Management Plan. PWD is located in Los Angeles County and serves the residents of the City of Palmdale. The Urban Water Management Planning Act requires every "urban water supplier" of a certain size to prepare and adopt an Urban Water Management Plan (UWMP) at least once every five years. The UWMP is a planning document in which water suppliers evaluate and compare their water supply and reliability to their existing and projected demands. A complete UWMP is necessary for PWD to remain eligible for state drought water bank assistance and is a requirement of state grant and loan funding programs.

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Very truly yours,

Člaudia Bolanos



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KATHY MAC LAREN

Division 4

VINCENT DINO
Division 5

DENNIS D. LaMOREAUX General Manager

ALESHIRE & WYNDER LLP
Attorneys





PALMDALE WATER DISTRICT

A CENTURY OF SERVICE

October 1, 2020

Los Angeles County Farm Bureau Attn. Richard Miner 41228 12th Street West, Suite A Palmdale, CA 93SS1

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

To Whom it May Concern:

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VINCENT DINO
Division 5

DENNIS D. LaMOREAUX General Manager

ALESHIRE & WYNDER LLP Attorneys





PALMDALE WATER DISTRICT

A CENTURY OF SERVICE

October 1, 2020

Los Angeles World Airports Airport Environmental Manager 7301 World Way West, 3rd Floor Los Angeles, CA 90045

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

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The Palmdale Water District (PWD) is undertaking the review, update, and revision of its Urban Water Management Plan. PWD is located in Los Angeles County and serves the residents of the City of Palmdale. The Urban Water Management Planning Act requires every "urban water supplier" of a certain size to prepare and adopt an Urban Water Management Plan (UWMP) at least once every five years. The UWMP is a planning document in which water suppliers evaluate and compare their water supply and reliability to their existing and projected demands. A complete UWMP is necessary for PWD to remain eligible for state drought water bank assistance and is a requirement of state grant and loan funding programs.

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Division 5

DENNIS D. LaMOREAUX

General Manager

ALESHIRE & WYNDER LLP

Attorneys





PALMDALE WATER DISTRICT

A CENTURY OF SERVICE

October 1, 2020

Los Angeles County Waterworks District 40 900 S. Fremont St.
Alhambra, CA 91803

Subject: 2020 Urban Water Management Plan for the Palmdale Water District

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The Palmdale Water District (PWD) is undertaking the review, update, and revision of its Urban Water Management Plan. PWD is located in Los Angeles County and serves the residents of the City of Palmdale. The Urban Water Management Planning Act requires every "urban water supplier" of a certain size to prepare and adopt an Urban Water Management Plan (UWMP) at least once every five years. The UWMP is a planning document in which water suppliers evaluate and compare their water supply and reliability to their existing and projected demands. A complete UWMP is necessary for PWD to remain eligible for state drought water bank assistance and is a requirement of state grant and loan funding programs.

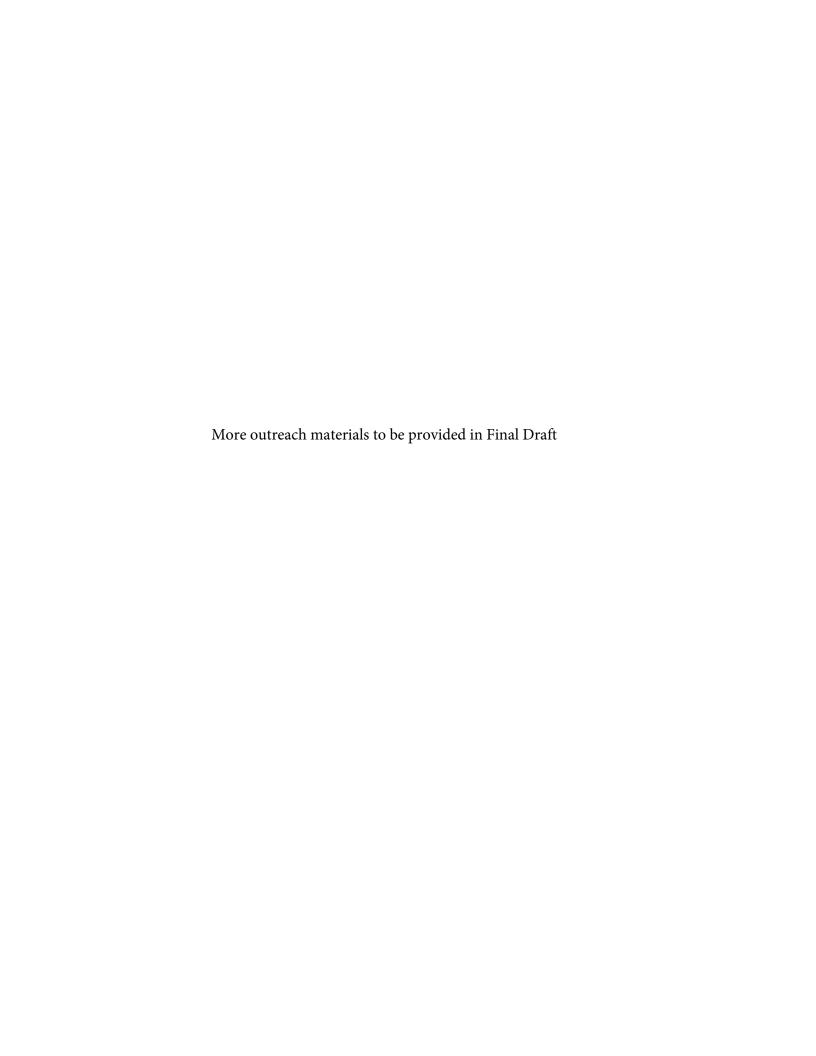
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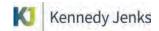
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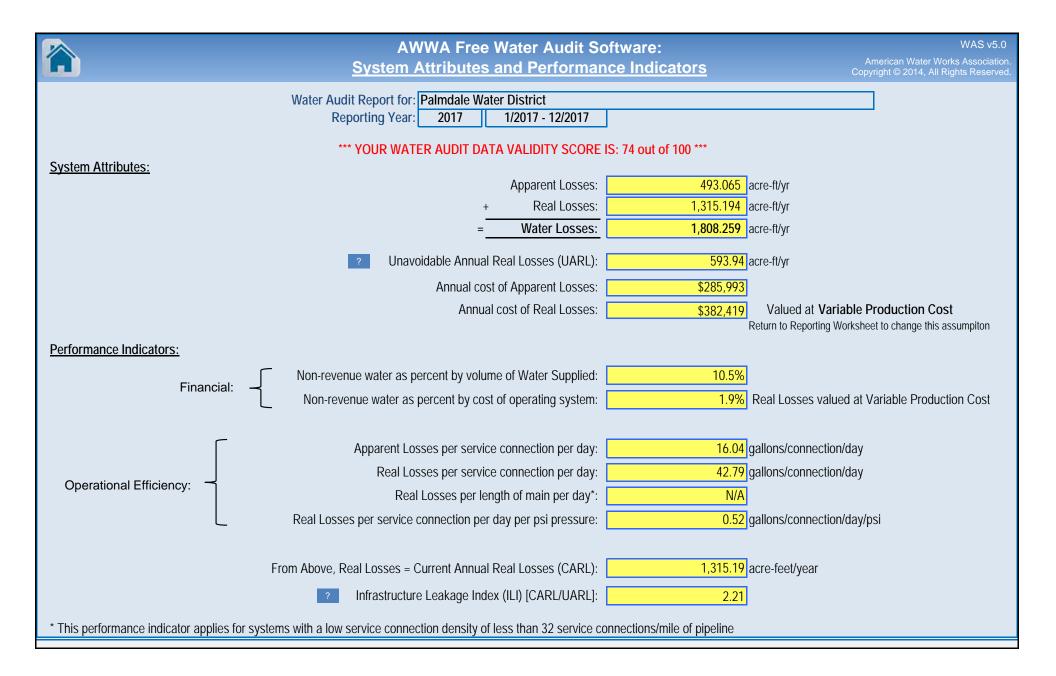




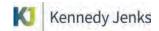
Appendix E: Water Systems Audit Output

	AWWA Fre	e Water Audit S	oftware:	WAS v5.0
	Rep	orting Workshee	<u>et</u>	American Water Works Associati Copyright © 2014, All Rights Reserv
	dit Report for: Palmdale Wa	ater District 1/2015 - 12/2015		
Please enter data in the white cells below. Where available, minput data by grading each component (n/a or 1-10) using the				
	· ·	be entered as: ACRE-I	·	Ü
To select the correct data gradin the utility meets or exce	g for each input, determine the eds all criteria for that grade a			Master Meter and Supply Error Adjustments
WATER SUPPLIED		< Enter grading	in column 'E' and 'J'	Pcnt: Value:
	n own sources: + ? 9 Vater imported: + ? n/a	17,014.560	acre-ft/yr + ?	10 -1.00% • c acre-ft/y acre-ft/y
	Vater exported: + ? 8		acre-ft/yr + ?	10 -1.00% • c acre-ft/y
WATE	ER SUPPLIED:	16,748.556	acre-ft/vr	Enter negative % or value for under-registration Enter positive % or value for over-registration
AUTHORIZED CONSUMPTION		10,140,000	4010 1891	
	Billed metered: + ? 9	15,078.000	acre-ft/yr	Click here: ? for help using option
	led unmetered: + ? n/a	0.000		buttons below
	billed metered: + ? 10		acre-ft/yr acre-ft/yr	Pcnt: Value:
	ed volume entered is greater		•	
AUTHORIZED CO		15,451.120		Use buttons to select
Actionizes	TOTAL STATE OF THE	10,1011120	uoto tuyi	percentage of water supplied
WATER LOSSES (Water Supplied - Authorized Consu	umntion)	1,297.436	acre-ft/vr	
Apparent Losses	impuonj	1,297.430	acie-ivyi	Pcnt: ▼ Value:
	d consumption: + ?	41.871	acre-ft/yr	0.25% • • acre-ft/y
Default option selected for una	uthorized consumption - a	grading of 5 is applied	but not displayed	
Customer meterin	g inaccuracies: + ? 7	308.119	acre-ft/yr	2.00% ● ○ acre-ft/y
	nandling errors: + ?		acre-ft/yr	0.25% ● o acre-ft/y
Default option selected for	· ·			
Арр	arent Losses:	387.685	асге-тиуг	
Real Losses (Current Annual Real Losses or CARL)				
Real Losses = Water Losses - App	arent Losses:	909.750	acre-ft/yr	
WA	TER LOSSES:	1,297.436	acre-ft/yr	
NON-REVENUE WATER NON-REVI	ENUE WATER:	1,670.556	acre-ft/yr	
= Water Losses + Unbilled Metered + Unbilled Unmetered				
SYSTEM DATA				
Number of active AND inactive service	ength of mains: + ? 9 ce connections: + ? 10 nection density: ?	433.0 27,481 63		
Are quotomer meters traigelly legated at the gurbaten of	r property line?	Yes		
Are customer meters typically located at the curbstop of <u>Average</u> length of custom		Tes	(length of service iii)	e, <u>beyond</u> the property eresponsibility of the utility)
Average length of customer service			e of 10 has been applied	
Average oper	ating pressure: + ? 9	80.0	psi	
COST DATA				
Total annual cost of operating	water system: + ? 10	\$32,560,448	\$/Year	
Customer retail unit cost (applied to Ap	/		\$/100 cubic feet (ccf)	
Variable production cost (applied to	Real Losses): + ? 5	\$108.26	\$/acre-ft □ Use Cus	tomer Retail Unit Cost to value real losses
WATER AUDIT DATA VALIDITY SCORE:				
	*** YOUR SCO	RE IS: 79 out of 100 **	*	
A weighted scale for the comp	onents of consumption and water	er loss is included in the ca	Iculation of the Water Audit Da	ata Validity Score
PRIORITY AREAS FOR ATTENTION:				
Based on the information provided, audit accuracy can be imp	roved by addressing the following	ng components:		
1: Customer retail unit cost (applied to Apparent Losse				
2: Variable production cost (applied to Real Losses)				
3: Volume from own sources				

	AWWA Free	e Water Audit S	oftware:		WAS v5.0
	Repo	orting Workshee	<u>et</u>		American Water Works Association. Copyright © 2014, All Rights Reserved.
Click to access definition Click to add a comment Water Audit Report fo Reporting Yea		nter District 1/2016 - 12/2016			
Please enter data in the white cells below. Where available, metered values s input data by grading each component (n/a or 1-10) using the drop-down list t					e in the accuracy of the
	All volumes to I	be entered as: ACRE-F	EET PER YEAR		
To select the correct data grading for each inp the utility meets or exceeds <u>all</u> criteria				Master Meter and S	upply Error Adjustments
WATER SUPPLIED	<	Enter grading	in column 'E' and 'J'	> Pcnt:	Value:
Volume from own source Water importe		17,367.3	acre-ft/yr + +		• -430.269 acre-ft/yr acre-ft/yr
Water exported		641.060			acre-ft/yr
WATER SUPPLIED)·	17,156.510	acre-ft/vr	-	value for under-registration value for over-registration
AUTHORIZED CONSUMPTION	<u> </u>	11,100,010	uoio ivyi	Enter positive 70 of 1	
Billed metered	d: + ? 7	15,204.000	acre-ft/yr		Click here: ? for help using option
Billed unmetere Unbilled metere		0.000	acre-ft/yr acre-ft/yr	Pcnt:	buttons below Value:
Unbilled unmetere			acre-ft/yr	PCIII.	• 366.120 acre-ft/yr
Unbilled Unmetered volume en	u		•		acie-ityi
AUTHORIZED CONSUMPTION		15,597.510		<u></u>	Use buttons to select percentage of water
					supplied OR
WATER LOSSES (Water Supplied - Authorized Consumption)		1,559.000	acre-ft/yr	<u>—</u>	value
Apparent Losses				Pcnt:	▼ Value:
Unauthorized consumption			acre-ft/yr	0.25%	o acre-ft/yr
Default option selected for unauthorized co					
Customer metering inaccuracie Systematic data handling error			acre-ft/yr acre-ft/yr	2.1170	o acre-ft/yr acre-ft/yr
Default option selected for Systematic d			•		acre-it/yi
Apparent Losses		413.981			
Real Losses (Current Annual Real Losses or CARL)					
Real Losses = Water Losses - Apparent Losses	s: ?	1,145.019	acre-ft/yr		
		1,145.019 1,559.000	•		
Real Losses = Water Losses - Apparent Losses WATER LOSSES NON-REVENUE WATER	S:	1,559.000	acre-ft/yr		
Real Losses = Water Losses - Apparent Losses WATER LOSSES	S:		acre-ft/yr		
Real Losses = Water Losses - Apparent Losses WATER LOSSES NON-REVENUE WATER NON-REVENUE WATER	S:	1,559.000	acre-ft/yr		
Real Losses = Water Losses - Apparent Losses WATER LOSSES NON-REVENUE WATER NON-REVENUE WATER = Water Losses + Unbilled Metered + Unbilled Unmetered SYSTEM DATA Length of main Number of active AND inactive service connection	S: ? 9 S: + ? 9 S: + ? 7	1,559.000 1,952.510 433.0 27,420	acre-ft/yr acre-ft/yr miles		
Real Losses = Water Losses - Apparent Losses WATER LOSSES NON-REVENUE WATER NON-REVENUE WATER = Water Losses + Unbilled Metered + Unbilled Unmetered SYSTEM DATA Length of main Number of active AND inactive service connection Service connection density	S: ? ?	1,559.000 1,952.510 433.0 27,420 63	acre-ft/yr		
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Real Losses = Water Losses - Apparent Losses WATER LOSSES NON-REVENUE WATER NON-REVENUE WATER = Water Losses + Unbilled Metered + Unbilled Unmetered SYSTEM DATA Length of main Number of active AND inactive service connection Service connection density	S:	1,559.000 1,952.510 433.0 27,420 63 Yes	acre-ft/yr acre-ft/yr miles conn./mile main (length of service boundary, that is	the responsibility of the utili	ity)
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Real Losses = Water Losses - Apparent Losses WATER LOSSES NON-REVENUE WATER = Water Losses + Unbilled Metered + Unbilled Unmetered SYSTEM DATA Length of main Number of active AND inactive service connection Service connection densit Are customer meters typically located at the curbstop or property line Average length of customer service line Average length of customer service line has been	S:	1,559.000 1,952.510 433.0 27,420 63 Yes d a data grading score	acre-ft/yr acre-ft/yr miles conn./mile main (length of service boundary, that is of 10 has been applied	the responsibility of the utili	iity)
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? Click to access	
Click to add a Reporting Year: 20	dale Water District (1910102) 019 1/2019 - 12/2019
data by grading each component (n/a or 1-10) using the drop-down list to the left of the in	
	Imes to be entered as: ACRE-FEET PER YEAR
To select the correct data grading for each input, determine the h utility meets or exceeds <u>all</u> criteria for that grade	and all grades below it. Master Meter and Supply Error Adjustments
WATER SUPPLIED	<
Volume from own sources: + 2 Water imported: + 2 Water exported: + ?	7 18,534.091 acre-ft/yr
WATER SUPPLIED:	Enter negative % or value for under-registration 17,580.905 acre-ft/yr Enter positive % or value for over-registration
AUTHORIZED CONSUMPTION	Click here:
Billed metered: + ?	8 15,853.000 acre-ft/yr for help using option
Billed unmetered: + 2 Unbilled metered: + 2	
Unbilled unmetered: + 2	
Onbined drimetered.	▲ Use buttons to select
AUTHORIZED CONSUMPTION:	16,229.640 acre-ft/yr ————————————————————————————————————
WATER LOSSES (Water Supplied - Authorized Consumption)	1,351.265 acre-ft/yr
Apparent Losses	Pcnt: ▼ Value:
Unauthorized consumption: + 22 Default option selected for unauthorized consumpt	
Customer metering inaccuracies: + ?	8 -27.478 acre-ft/yr -0.17% ● ○ acre-ft/yr
Systematic data handling errors: + ?	
Default option selected for Systematic data hand Apparent Losses:	dling errors - a grading of 5 is applied but not displayed 56.107 acre-ft/yr
Real Losses (Current Annual Real Losses or CARL)	
Real Losses = Water Losses - Apparent Losses:	1,295.158 acre-ft/yr
WATER LOSSES:	1,351.265 acre-ft/yr
NON-REVENUE WATER NON-REVENUE WATER:	1,727.905 acre-ft/yr
= Water Losses + Unbilled Metered + Unbilled Unmetered	
SYSTEM DATA	
Length of mains: + ? Number of <u>active AND inactive</u> service connections: + ? Service connection density: 2	9 433.0 miles 7 27,454 63 conn./mile main
Are customer meters typically located at the curbstop or property line?	Yes (length of service line, <u>beyond</u> the property boundary,
Average length of customer service line: + 2 Average length of customer service line has been set to a	that is the responsibility of the utility)
Average length of customer service line has been set to a Average operating pressure: + 2	
COST DATA	
Total annual cost of operating water system:	10 \$36,692,915 \$/Year
Customer retail unit cost (applied to Apparent Losses): + ?	9 \$1.37 \$/100 cubic feet (ccf)
Variable production cost (applied to Real Losses): + 2	5 \$277.03 \$/acre-ft Use Customer Retail Unit Cost to value real losses
WATER AUDIT DATA VALIDITY SCORE:	
*** YOU	UR SCORE IS: 74 out of 100 ***
A weighted scale for the components of consumption	and water loss is included in the calculation of the Water Audit Data Validity Score
PRIORITY AREAS FOR ATTENTION:	
Based on the information provided, audit accuracy can be improved by addressing the fo	ollowing components:
Based on the information provided, audit accuracy can be improved by addressing the fo	following components:
1: Volume from own sources	following components:
	following components:



Appendix F: SBX7-7 & DWR Population Tool

SB X7-7 Table 0: Units of Measure Used in UWMP* one from the drop down list)	(select
Acre Feet	
*The unit of measure must be consistent with Submittal Table	2-3
NOTES:	

SB X7-7 Table-1: Baseline Period Ranges							
Baseline	Parameter	Value	Units				
	2008 total water deliveries	25,339	Acre Feet				
	2008 total volume of delivered recycled water		Acre Feet				
10- to 15-year baseline period	2008 recycled water as a percent of total deliveries	0%	See Note 1				
	Number of years in baseline period ^{1, 2}	10	Years				
	Year beginning baseline period range	1995					
	Year ending baseline period range ³	2004					
F	Number of years in baseline period	5	Years				
5-year	Year beginning baseline period range	2003					
baseline period	Year ending baseline period range ⁴	2007					

¹ If the 2008 recycled water delivery is less than 10 percent of total water deliveries, then the 10-15year baseline period is a continuous 10-year period. If the amount of recycled water delivered in 2008 is 10 percent or greater of total deliveries, the 10-15 year baseline period is a continuous 10- to 15-year period.

SB X7-7 T	SB X7-7 Table 2: Method for Population Estimates				
	Method Used to Determine Population (may check more than one)				
	1. Department of Finance (DOF) or American Community Survey (ACS)				
	2. Persons-per-Connection Method				
V	3. DWR Population Tool				
	4. Other DWR recommends pre-review				
NOTES:					

SB X7-7 Table 3: Service Area Population					
Υ	'ear	Population			
10 to 15 Ye	ear Baseline P	opulation			
Year 1	1995	79,578			
Year 2	1996	88,785			
Year 3	1997	89,675			
Year 4	1998	90,540			
Year 5	1999	91,375			
Year 6	2000	92,172			
Year 7	2001	98,516			
Year 8	2002	99,649			
Year 9	2003	100,788			
Year 10	2004	104,237			
Year 11					
Year 12					
Year 13					
Year 14					
Year 15					
5 Year Base	eline Populati	on			
Year 1	2003	100,788			
Year 2	2004	104,237			
Year 3	2005	104,120			
Year 4	2006	105,754			
Year 5	2007	107,396			
NOTES:					

SB X7-7 Table 4: Annual Gross Water Use *								
			_	Deductions			Acre Feet	
	line Year (7-7 Table 3	Volume Into Distribution System This column will remain blank until SB X7-7 Table 4-A is completed.	Exported Water	Change in Dist. System Storage (+/-)	Indirect Recycled Water This column will remain blank until SB X7-7 Table 4-B is completed.	Water Delivered for Agricultural Use	Process Water This column will remain blank until SB X7-7 Table 4-D is completed.	Annual Gross Water Use
10 to 15 Y	ear Baseline - (Gross Water Use						
Year 1	1995	22,233			ı		-	22,233
Year 2	1996	23,514			ı		-	23,514
Year 3	1997	23,152			-		-	23,152
Year 4	1998	20,626			-		-	20,626
Year 5	1999	23,398			-		-	23,398
Year 6	2000	25,901			-		-	25,901
Year 7	2001	25,220			-		-	25,220
Year 8	2002	25,670			-		-	25,670
Year 9	2003	24,909			-		-	24,909
Year 10	2004	26,684			-		-	26,684
Year 11	0	-			-		-	-
Year 12	0	-			-		-	-
Year 13	0	-			-		-	-
Year 14	0	-			-		-	-
Year 15	0	-			-		-	-
10 - 15 yea	ar baseline ave	rage gross water use						24,131
5 Year Bas	seline - Gross V	Vater Use						
Year 1	2003	24,909			ı		-	24,909
Year 2	2004	26,684			-		-	26,684
Year 3	2005	26,128			-		-	26,128
Year 4	2006	27,934			-		-	27,934
Year 5	2007	28,152			-		-	28,152
5 year bas	eline average	gross water use						26,761

SB X7-7 Table 4-A: Volume Entering the Distribution System(s)

Complete one table for each source.

Name of Source Enter Name of Source 1

This water source is:

The supplier's own water source

A purchased or imported source

	A purchased of imported source					
Baseline Year Fm SB X7-7 Table 3		Volume Entering Distribution System ¹	Meter Error Adjustment ² Optional (+/-)	Corrected Volume Entering Distribution System		
10 to 15 Ye	ear Baseline -	Water into Distribu				
Year 1	1995	22,233		22,233		
Year 2	1996	23,514		23,514		
Year 3	1997	23,152		23,152		
Year 4	1998	20,626		20,626		
Year 5	1999	23,398		23,398		
Year 6	2000	25,901		25,901		
Year 7	2001	25,220		25,220		
Year 8	2002	25,670		25,670		
Year 9	2003	24,909		24,909		
Year 10	2004	26,684		26,684		
Year 11	0			ı		
Year 12	0			-		
Year 13	0			-		
Year 14	0			-		
Year 15	0			-		
5 Year Bas	eline - Water	into Distribution Sy	rstem			
Year 1	2003	24,909		24,909		
Year 2	2004	26,684		26,684		
Year 3	2005	26,128		26,128		
Year 4	2006	27,934		27,934		
Year 5	2007	28,152		28,152		

¹ **Units of measure** (AF, MG, or CCF) must remain consistent throughout the UWMP, as reported in Table 2-3.

² Meter Error Adjustment - See guidance in Methodology 1, Step 3 of Methodologies Document

SB X7-7 Table 4-C.1: Process Water Deduction Eligibility

Criteria 1

Industrial water use is equal to or greater than 12% of gross water use

Baseline Year Fm SB X7-7 Table 3		Gross Water Use Without Process Water Deduction	Industrial Water Use *	Percent Industrial Water	Eligible for Exclusion Y/N
10 to 15 Ye	ear Baseline -	Process Water	Deduction Eligib	oility	
Year 1	1995	22,233		0%	NO
Year 2	1996	23,514		0%	NO
Year 3	1997	23,152		0%	NO
Year 4	1998	20,626		0%	NO
Year 5	1999	23,398		0%	NO
Year 6	2000	25,901		0%	NO
Year 7	2001	25,220		0%	NO
Year 8	2002	25,670		0%	NO
Year 9	2003	24,909		0%	NO
Year 10	2004	26,684		0%	NO
Year 11	0	-			NO
Year 12	0	-			NO
Year 13	0	-			NO
Year 14	0	-			NO
Year 15	0	-			NO
5 Year Bas	eline - Proces	s Water Deduc	tion Eligibility		
Year 1	2003	24,909		0%	NO
Year 2	2004	26,684		0%	NO
Year 3	2005	26,128		0%	NO
Year 4	2006	27,934		0%	NO
Year 5	2007	28,152		0%	NO

^{*} Units of Measure (AF, MG, or CCF) must remain consistent throughout the UWMP, as reported in Table 2-3.

SB X7-7 Table 4-C.2: Process Water Deduction Eligibility

Criteria 2

Industrial water use is equal to or greater than 15 GPCD

Baseline Year Fm SB X7-7 Table 3		Industrial Water Use *	Population	Industrial GPCD	Eligible for Exclusion Y/N
10 to 15 Ye	ear Baseline - P	rocess Water De	eduction Eligibility		
Year 1	1995		79,578	ı	NO
Year 2	1996		88,785	-	NO
Year 3	1997		89,675	-	NO
Year 4	1998		90,540	-	NO
Year 5	1999		91,375	-	NO
Year 6	2000		92,172	-	NO
Year 7	2001		98,516	-	NO
Year 8	2002		99,649	-	NO
Year 9	2003		100,788	-	NO
Year 10	2004		104,237	-	NO
Year 11	0		-		NO
Year 12	0		-		NO
Year 13	0		-		NO
Year 14	0		-		NO
Year 15	0		-		NO
5 Year Bas	eline - Process	Water Deduction	n Eligibility		
Year 1	2003		100,788	-	NO
Year 2	2004		104,237	-	NO
Year 3	2005		104,120	-	NO
Year 4	2006		105,754	-	NO
Year 5	2007		107,396	-	NO

^{*} Units of Measure (AF, MG, or CCF) must remain consistent throughout the UWMP, as reported in Table 2-3.

SB X7-7 Table 4-C.3: Process Water Deduction Eligibility									
Criteria 3	Criteria 3								
Non-industria	al use is equal to o	or less than 120 GPC	D						
	ine Year 7-7 Table 3	Gross Water Use Without Process Water Deduction Fm SB X7-7 Table 4	Industrial Water Use *	Non-industrial Water Use	Population Fm SB X7-7 Table 3	Non-Industrial GPCD	Eligible for Exclusion Y/N		
10 to 15 Ye	ear Baseline - F	Process Water De	eduction Eligib	ility					
Year 1	1995	22,233		22,233	79,578	249	NO		
Year 2	1996	23,514		23,514	88,785	236	NO		
Year 3	1997	23,152		23,152	89,675	230	NO		
Year 4	1998	20,626		20,626	90,540	203	NO		
Year 5	1999	23,398		23,398	91,375	229	NO		
Year 6	2000	25,901		25,901	92,172	251	NO		
Year 7	2001	25,220		25,220	98,516	229	NO		
Year 8	2002	25,670		25,670	99,649	230	NO		
Year 9	2003	24,909		24,909	100,788	221	NO		
Year 10	2004	26,684		26,684	104,237	229	NO		
Year 11	0	ı		ı	ı		NO		
Year 12	0	ı		1	ı		NO		
Year 13	0	ı		ı	ı		NO		
Year 14	0	ı		ı	ı		NO		
Year 15	0	ı		ı	ı		NO		
5 Year Base	5 Year Baseline - Process Water Deduction Eligibility								
Year 1	2003	24,909		24,909	100,788	221	NO		
Year 2	2004	26,684		26,684	104,237	229	NO		
Year 3	2005	26,128		26,128	104,120	224	NO		
Year 4	2006	27,934		27,934	105,754	236	NO		
Year 5	2007	28,152		28,152	107,396	234	NO		

SB X7-7 T	SB X7-7 Table 5: Baseline Gallons Per Capita Per Day (GPCD)							
Base	line Year (7-7 Table 3	Service Area Population Fm SB X7-7 Table 3	Annual Gross Water Use Fm SB X7-7 Table 4	Daily Per Capita Water Use (GPCD)				
10 to 15 Year Baseline GPCD								
Year 1	1995	79,578	22,233	249				
Year 2	1996	88,785	23,514	236				
Year 3	1997	89,675	23,152	230				
Year 4	1998	90,540	20,626	203				
Year 5	1999	91,375	23,398	229				
Year 6	2000	92,172	25,901	251				
Year 7	2001	98,516	25,220	229				
Year 8	2002	99,649	25,670	230				
Year 9	2003	100,788	24,909	221				
Year 10	2004	104,237	26,684	229				
Year 11	0	-	•					
Year 12	0	1	ı					
Year 13	0	1	ı					
Year 14	0	-	1					
Year 15	0	-	-					
10-15 Yea	r Average Bas	eline GPCD		231				
5 Year Ba	seline GPCD							
	line Year 7-7 Table 3	Service Area Population Fm SB X7-7 Table 3	Gross Water Use Fm SB X7-7 Table 4	Daily Per Capita Water Use				
Year 1	2003	100,788	24,909	221				
Year 2	2004	104,237	26,684	229				
Year 3	2005	104,120	26,128	224				
Year 4	2006	105,754	27,934	236				
Year 5	2007	107,396	28,152	234				
5 Year Ave	erage Baseline	GPCD		229				

SB X7-7 Table 6: Baseline GPC From Table SB X7-7 Table 5	D Summary
10-15 Year Baseline GPCD	231
5 Year Baseline GPCD	229
NOTES:	

SB X7-7 Table 7: 2020 Target Method Select Only One						
Tar	Target Method Supporting Tables					
v	Method 1	SB X7-7 Table 7A				
	Method 2	SB X7-7 Tables 7B, 7C, and 7D				
0	Method 3	SB X7-7 Table 7-E				
	Method 4	Method 4 Calculator Located in the WUE Data Portal at wuedata.water.ca.gov Resources button				

SB X7-7 Table 7-A: Target Method 1 20% Reduction						
10-15 Year Baseline GPCD	2020 Target GPCD					
231	185					
NOTES:						

SB X7-7 Table 7-C: Target Method 2								
Target C	Target CII Water Use							
Baseline Year Fm SB X7-7 Table 3		CII Water Use ^{1,2}	Process Water Exclusion (Optional) Fm SB X7-7 Table 4	CII Water Use Minus Process Water	Population Fm SB X7-7 Table 3	CII GPCD		
		Un	it of Measure	2		Acre Feet		
Year 1	1995		0	0	79,578	0		
Year 2	1996		0	0	88,785	0		
Year 3	1997		0	0	89,675	0		
Year 4	1998		0	0	90,540	0		
Year 5	1999		0	0	91,375	0		
Year 6	2000		0	0	92,172	0		
Year 7	2001		0	0	98,516	0		
Year 8	2002		0	0	99,649	0		
Year 9	2003		0	0	100,788	0		
Year 10	2004		0	0	104,237	0		
Year 11	0		0	0	-			
Year 12	0		0	0	-			
Year 13	0		0	0	-			
Year 14	0		0	0	-			
Year 15	0		0	0	-			
Average Annual 10 to 15 Year Baseline CII Water Use (GPCD)						0		
10% Reduction						0.0		
2020 T	2020 Target CII Water Use 0							
¹ CII water	¹ CII water use for each year of the baseline period must be provided by the user.							
² Units of measure (AF, MG , or CCF) must remain consistent throughout the UWMP, as reported in Table 2-3.								

S	SB X7-7 Table 7-F: Confirm Minimum Reduction for 2020 Target							
	5 Year Baseline GPCD		2					
		Maximum 2020	As calculated by	Special Situations ³		Confirmed 2020		
	From SB X7-7 Table 5	Target ¹	supplier in this SB X7-7 Verification Form	Prorated 2020 Target	Population Weighted Average 2020 Target	Target⁴		
	229	217				217		

¹ Maximum 2020 Target is 95% of the 5 Year Baseline GPCD except for suppliers at or below 100 GPCD.

Confirmed Target is the lesser of the Calculated 2020 Target (C5, D5, or E5) or the Maximum 2020 Target (Cell B5)

² Calculated 2020 Target is the target calculated by the Supplier based on the selected Target Method, see SB X7-7 Table 7 and corresponding tables for agency's calculated target. Supplier may only enter one calculated target.

³ **Prorated targets and population weighted target** are allowed for special situations only. These situations are described in Appendix P, Section P.3

SB X7-7 Table 0: Units of Measure Used in 2020 UWMP* (select one from the drop down list)
Acre Feet
*The unit of measure must be consistent throughout the UWMP, as reported in Submittal Table 2-3.
NOTES:

SB X7-7 T	SB X7-7 Table 2: Method for 2020 Population Estimate						
	Method Used to Determine 2020 Population (may check more than one)						
	1. Department of Finance (DOF) or American Community Survey (ACS)						
	2. Persons-per-Connection Method						
Ø	3. DWR Population Tool						
	4. Other DWR recommends pre-review						
NOTES:							

SB X7-7 Table 3: 2020 Service Area Population						
2020 Compliance Year Population						
2020 126,002						
NOTES:						

SB X7-7 Table 4: 2020 Gross Water Use							
Compliance Year 2020	2020 Volume Into Distribution System This column will remain blank until SB X7-7 Table 4-A is completed.	Exported Water *	Change in Dist. System Storage* (+/-)	Indirect Recycled Water This column will remain blank until SB X7-7 Table 4-B is completed.	Water Delivered for Agricultural Use*	Process Water This column will remain blank until SB X7-7 Table 4-D is completed.	2020 Gross Water Use
	23,245			-		-	23,245

^{*} Units of measure (AF, MG, or CCF) must remain consistent throughout the UWMP, as reported in SB X7-7 Table 0 and Submittal Table 2-3.

SB X7-7 Table 4-A: 2020 Volume Entering the Distribution System(s), Meter Error Adjustment

Complete one table for each source.

Name of Source		SWP Water - Table A Amounts						
This water	This water source is (check one):							
	The suppli	er's own water source						
Ø	A purchase	ed or imported source						
Compliance Year 2020		Volume Entering Distribution System 1	Meter Error Adjustment ² Optional (+/-)	Corrected Volume Entering Distribution System				
		5,695	ı	5,695				

¹ Units of measure (AF, MG, or CCF) must remain consistent throughout the UWMP, as reported in SB X7-7 Table 0 and Submittal Table 2-3.

² Meter

Error Adjustment - See guidance in Methodology 1, Step 3 of Methodologies Document

NOTES

SB X7-7 Table 4-A: 2020 Volume Entering the Distribution System(s) Meter Error Adjustment

Complete one table for each source.

SWP Water - Butte Transfer Agreement						
This water source is (check one):						
☐ The supplier's own water source						
Ø	A purchased or imported source					
Compliance Year		Volume Entering	Meter Error Adjustment ²	Corrected Volume Entering		

1,320	Compliance Year 2020	Volume Entering Distribution System 1	Adjustment ² Optional (+/-)	Corrected Volume Entering Distribution System
_,,		1,320		1,320

Units of measure (AF, MG, or CCF) must remain consistent throughout the UWMP, as reported in SB X7-7 Table 0 and Submittal Table 2-3.
Meter Error

Adjustment - See guidance in Methodology 1, Step 3 of Methodologies Document

NOTES:

SB X7-7 Table 4-A: 2020 Volume Entering the Distribution System(s), Meter Error Adjustment

Complete one table for each source.

Name of Source Littlerock Dam Reservoir - Surface Water

This water source is (check one):						
✓	The supplie	The supplier's own water source				
	A purchase	ed or imported source				
Compliance Year 2020		Volume Entering Distribution System ¹	Meter Error Adjustment ² Optional (+/-)	Corrected Volume Entering Distribution System		
		4,540		4,540		
¹ Units of measure (AF, MG, or CCF) must remain consistent throughout the UWMP, as reported in SB						
X7-7 Table 0	and Submitta	l Table 2-3.		² Meter Error		
Adjustment NOTES:	- See guidance	e in Methodology 1, Step 3 of N	1ethodologies Docum	ent		

SB X7-7 Table 4-A: 2020 Volume Entering the Distribution System(s), Meter Error Adjustment

Complete one table for each source.

·					
Name of Source Groundwater Return Flows					
This water source is (check one):					
Ø	☐ The supplier's own water source				
	A purchase	A purchased or imported source			
•	nce Year 20	Volume Entering Distribution System 1	Meter Error Adjustment ² Optional (+/-)	Corrected Volume Entering Distribution System	
		4,090		4,090	
1					

¹ Units of measure (AF, MG, or CCF) must remain consistent throughout the UWMP, as reported in SB X7-7 Table 0 and Submittal Table 2-3.

Adjustment - See guidance in Methodology 1, Step 3 of Methodologies Document

NOTES:

SB X7-7 Table 4-A: 2020 Volume Entering the Distribution System(s), Meter Error Adjustment

Complete one table for each source.

Name of	Source	Groundwater - Antelope Valley Basin	
This water source is (check one):			
I	The suppli	The supplier's own water source	
	A purchase	ed or imported source	

Compliance Year 2020	Volume Entering Distribution System ¹	Meter Error Adjustment ² Optional (+/-)	Corrected Volume Entering Distribution System		
	7,600		7,600		
1 Units of measure (AF, MG, or CCF) must remain consistent throughout the UWMP, as reported in SB X7-7 Table 0 and Submittal Table 2-3					

Adjustment - See guidance in Methodology 1, Step 3 of Methodologies Document

NOTES:

Criteria 1 Industrial water use is equal to or greater than 12% of gross water use						
2020 Compliance Year	2020 Gross Water Use Without Process Water Deduction	2020 Industrial Water Use	Percent Industrial Water	Eligible for Exclusion Y/N		
	23,245		0%	NO		
NOTES:						

SB X7-7 Table 4-C.2 use only by agencies that	•	(For			
Criteria 2 Industrial water use is equal to or greater than 15 GPCD					
2020 Compliance Year	2020 Industrial Water Use	2020 Population	2020 Industrial GPCD	Eligible for Exclusion Y/N	
		126,002	-	NO	
NOTES:					

SB X7-7 Table 4-C.3: 2020 Process Water Deduction Eligibility

by agencies that are deducting process water using Criteria 3)

Criteria 3

Non-industrial use is equal to or less than 120 GPCD

2020 Compliance Year	2020 Gross Water Use Without Process Water Deduction Fm SB X7-7 Table 4	2020 Industrial Water Use	2020 Non- industrial Water Use	2020 Population Fm SB X7-7 Table 3	Non-Industrial GPCD	Eligible for Exclusion Y/N
	23,245		23,245	126,002	165	NO

(For use only

SB X7-7 Table 9: 2020 Compliance							
	Optional Adjustments to 2020 GPCD						
	Enter "	0" if Adjustment No	ot Used				Did Supplier
Actual 202 GPCD ¹	Extraordinary Events ¹	Weather Normalization ¹	Economic Adjustment ¹	TOTAL Adjustments ¹	Adjusted 2020 GPCD ¹ (Adjusted if applicable)	2020 Confirmed Target GPCD ^{1, 2}	Targeted
165	-	-	-	-	165		NO

¹ All values are reported in GPCD

NOTES:

² **2020 Confirmed Target GPCD** is taken from the Supplier's SB X7-7 Verification Form Table SB X7-7, 7-F.

Please print this page to a PDF and include as part of your UWMP submittal.

Confirmation Information					
Generated By	Water Supplier Name	Confirmation # 6940412223	Generated On		
Lauren Everett	Palmdale Water District		1/29/2021 1:14:15 PM		

Boundary Information			
Census Year	Census Year Boundary Filename		
1990	PWD_Boundary_1990.kml	462	
2000	PWD_Boundary_2000.kml	463	
2010	PWD_Boundary_2010.kml	464	
1990	PWD_Boundary_1990.kml	462	
2000	PWD_Boundary_2000.kml	463	
2010	PWD_Boundary_2010.kml	464	
1990	PWD_Boundary_1990.kml	462	
2000	PWD_Boundary_2000.kml	463	
2010	PWD_Boundary_2010.kml	464	
1990	PWD_Boundary_1990.kml	462	
2000	PWD_Boundary_2000.kml	463	
2010	PWD_Boundary_2010.kml	464	
1990	PWD_Boundary_1990.kml	462	
2000	PWD_Boundary_2000.kml	463	
2010	PWD_Boundary_2010.kml	464	
1990	PWD_Boundary_1990.kml	462	
2000	PWD_Boundary_2000.kml	463	
2010	PWD_Boundary_2010.kml	464	
1990	PWD_Boundary_1990.kml	462	
2000	PWD_Boundary_2000.kml	463	
2010	PWD_Boundary_2010.kml	464	

Baseline Period Ranges				
10 to 15-year baseline period				
Number of years in baseline period:	10 🕶			
Year beginning baseline period range:	1995 🗸			
Year ending baseline period range ¹ :	2004			
5-year baseline period				
Year beginning baseline period range:	2003 🕶			
Year ending baseline period range ² :	2007			
¹ The ending year must be between December 31, 2004 and December 31, 2010. ² The ending year must be between December 31, 2007 and December 31, 2010.				

Persons per Connection

	Census Block Level	Number of	Persons per
Year	Total Population	Connections *	Connection
1990	66,477	19619	3.39
1991	-	-	3.46
1992	-	-	3.53
1993	-	-	3.60
1994	-	-	3.67
1995	-	-	3.74
1996	-		3.80
1997	-	-	3.87
1998	-	-	3.94
1999	-	-	4.01
2000	92,172	22595	4.08
2001	-	-	4.11
2002	-	-	4.13
2003	-	-	4.16
2004	-		4.18
2005	-	-	4.21

2006	-	-	4.23
2007	-	-	4.25
2008		-	4.28
2009	-	-	4.30
2010	112,468	25959	4.33
2011	-	-	4.36
2012	-	-	4.38
2013	-	-	4.41
2014	-	-	4.43
2015	-	-	4.46
2020	-	-	4.59 **
	·		

Population Using Persons-Per-Connection						
Year		Number of Connections *	Persons per Connection	Total Population		
	10 to 15 Year Baseline Population Calculations					
Year 1	1995	21306	3.74	79,578		
Year 2	1996	23340	3.80	88,785		
Year 3	1997	23154	3.87	89,675		
Year 4	1998	22968	3.94	90,540		
Year 5	1999	22781	4.01	91,375		
Year 6	2000	22595	4.08	92,172		
Year 7	2001	23999	4.11	98,516		
Year 8	2002	24128	4.13	99,649		
Year 9	2003	24257	4.16	100,788		
Year 10	2004	24937	4.18	104,237		
	5 Year Baseline Population Calculations					
Year 1	2003	24257	4.16	100,788		
Year 2	2004	24937	4.18	104,237		
Year 3	2005	24761	4.21	104,120		
Year 4	2006	25001	4.23	105,754		
Year 5	2007	25240	4.25	107,396		
2020 Compliance Year Population Calculations						
2020 27479 4.59 ** 126,062			126,062			

Hide Print Confirmation



Appendix G: Groundwater Adjudication Court Order

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9	SUPERIOR COURT OF TH	E STATE OF CALIFORNIA
10	COUNTY OF LOS ANGEL	ES – CENTRAL DISTRICT
11 12	ANTELOPE VALLEY GROUNDWATER CASES	Judicial Council Coordination Proceeding No. 4408
13 14 15 16 17 18 19 20 21	Included Actions: Los Angeles County Waterworks District No. 40 v. Diamond Farming Co., Superior Court of California, County of Los Angeles, Case No. BC 325201; Los Angeles County Waterworks District No. 40 v. Diamond Farming Co., Superior Court of California, County of Kern, Case No. S-1500- CV-254-348; Wm. Bolthouse Farms, Inc. v. City of Lancaster, Diamond Farming Co. v. City of Lancaster, Diamond Farming Co. v. Palmdale Water Dist., Superior Court of California, County of Riverside, Case Nos. RIC 353 840, RIC 344 436, RIC 344 668	CLASS ACTION Santa Clara Case No. 1-05-CV-049053 Assigned to the Honorable Jack Komar (PROPOSED) JUDGMENT
222324	RICHARD WOOD, on behalf of himself and all other similarly situated v. A.V. Materials, Inc., et al., Superior Court of California, County of Los Angeles, Case No. BC509546	
25		
26		
27		
28		

The matter came on for trial in multiple phases. A large number of parties representing the majority of groundwater production in the Antelope Valley Area of Adjudication ("Basin") entered into a written stipulation to resolve their claims and requested that the Court enter their [Proposed] Judgment and Physical Solution as part of the final judgment. As to all remaining parties, including those who failed to answer or otherwise appear, the Court heard the testimony of witnesses, considered the evidence, and heard the arguments of counsel. Good cause appearing, the Court finds and orders judgment as follows:

- 1. The Second Amended Stipulation For Entry of Judgment and Physical Solution among the stated stipulating parties is accepted and approved by the Court.
- 2. Consistent with the December 23 2015 Statement of Decision ("Decision"), the Court adopts the Proposed Judgment and Physical Solution attached hereto as Exhibit A and incorporated herein by reference, as the Court's own physical solution ("Physical Solution"). The Physical Solution is binding upon all parties.
- 3. In addition to the terms and provisions of the Physical Solution the Court finds as follows:
 - a. Each of the Stipulating Parties to the Physical Solution has the right to pump groundwater from the Antelope Valley Adjudication Area as stated in the Decision and Physical Solution.
 - b. The following entities are awarded prescriptive rights from the native safe yield against the Tapia Parties, defaulted parties identified in Exhibit 1 to the Physical Solution, and parties who did not appear at trial identified in Exhibit B attached hereto, in the following amounts:

Los Angeles County Waterworks District No. 40	17,659.07 AFY
Palmdale Water District	8,297.91 AFY
Littlerock Creek Irrigation District	1,760 AFY
Quartz Hill Water District	1,413 AFY
Rosamond Community Services District	1,461.7 AFY
Palm Ranch Irrigation District	960 AFY

1		Desert	Lake Community Services District	318 AFY
2		Califor	rnia Water Service Company	655 AFY
3		North 1	Edwards Water District	111.67 AFY
4		No oth	er parties are subject to these prescriptive rights.	
5	c.	Each o	f the parties referred to in the Decision as Supporting I	Landowner
6		Parties	has the right to pump groundwater from the Antelope	Valley
7		Adjudi	cation Area as stated in the Decision and in Paragraph	5.1.10 of the
8		Physic	al Solution in the following amounts:	
9		i.	Desert Breeze MHP, LLC	18.1 AFY
10		ii.	Milana VII, LLC dba Rosamond Mobile Home Park	21.7 AFY
11		iii.	Reesdale Mutual Water Company	23 AFY
12		iv.	Juanita Eyherabide, Eyherabide Land Co., LLC	
13			and Eyherabide Sheep Company, collectively	12 AFY
14		v.	Clan Keith Real Estate Investments, LLC.,	
15			dba Leisure Lake Mobile Estates	64 AFY
16		vi.	White Fence Farms Mutual Water Co. No. 3	4 AFY
17 18	d.	vii. V (s) - Each m	LV Ritter Ranch LLC Robar Enterprises, Inc., Hi-Grade Materials Co., nember of the Small Pumper Class can exercise an over	0 AFY and CJR, a
19			nt to the Physical Solution. The Judgment Approving S	
20		-	Action Settlements is attached as Exhibit C ("Small Pur	•
21		Judgmo	ent") and is incorporated herein by reference.	•
22	e.	Cross-c	defendant Charles Tapia, as an individual and as Truste	e of Nellie
23		Tapia I	Family Trust (collectively, "The Tapia Parties") has no	right to pump
24		ground	water from the Antelope Valley Adjudication Area exc	ept under the
25		terms o	of the Physical Solution.	
26	f.	Phelan	Piñon Hills Community Services District ("Phelan") h	as no right to
27		pump g	groundwater from the Antelope Valley Adjudication Ar	ea except
28		under t	he terms of the Physical Solution.	

PROPOSED JUDGMENT

- g. The Willis Class members have an overlying right that is to be exercised in accordance with the Physical Solution.
- h. All defendants or cross-defendants who failed to appear in any of these coordinated and consolidated cases are bound by the Physical Solution and their overlying rights, if any, are subject to the prescriptive rights of the Public Water Suppliers. A list of the parties who failed to appear is attached hereto as Exhibit D.
- i. Robar Enterprises, Inc., Hi-Grade Materials Co., and CJR, a general partnership (collectively, "Robar") are

- 4. Each party shall designate the name, address and email address, to be used for all subsequent notices and service of process by a designation to be filed within thirty days after entry of this Judgment. The list attached as Exhibit A to the Small Pumper Class Judgment shall be used for notice purposes initially, until updated by the Class members and/or Watermaster. The designation may be changed from time to time by filing a written notice with the Court. Any party desiring to be relieved of receiving notice may file a waiver of notice to be approved by the Court. The Court will maintain a list of parties and their respective addresses to whom notice or service of process is to be sent. If no designation is made as required herein, a party's designee shall be deemed to be the attorney of record or, in the absence of an attorney of record, the party at its specified address.
- 5. All real property owned by the parties within the Basin is subject to this Judgment. It is binding upon all parties, their officers, agents, employees, successors and assigns. Any party, or executor of a deceased party, who transfers real property that is subject to this Judgment shall notify any transferee thereof of this Judgment.

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This Judgment shall not bind the parties that cease to own real property within the Basin, and cease to use groundwater, except to the extent required by the terms of an instrument, contract, or other agreement.

The Clerk shall enter this Judgment.

Dated: Dec 23, 2015

JUDGE OF THE SUPERIOR COURT



Appendix H: Data to Document Consistency with Delta Plan Policy WR P1

As stated in the 2020 UWMP Guidebook Appendix C (Draft version dated March 2021):

"An urban water supplier (Supplier) that anticipates participating in or receiving water supply benefits from a proposed project (covered action⁴⁾ such as a multiyear water transfer, conveyance facility, or new diversion that involves transferring water through, exporting water from, or using water in the Sacramento-San Joaquin Delta (Delta) should provide information in their 2015 and 2020 Urban Water Management Plans (UWMP's) that can then be used in the covered action process to demonstrate consistency with Delta Plan Policy WR P1, *Reduce Reliance on the Delta Through Improved Regional Water Self-Reliance* (California Code Reg., tit. 23, § 5003)."

WR P1 subsection (c)(1) further defines what adequately contributing to reduced reliance on the Delta means in terms of (a)(1) above.

- "(c)(1) Water suppliers that have done all the following are contributing to reduced reliance on the Delta and improved regional self-reliance and are therefore consistent with this policy:
 - (A) Completed a current Urban or Agricultural Water Management Plan (Plan) which has been reviewed by the California Department of Water Resources for compliance with the applicable requirements of Water Code Division 6, Parts 2.55, 2.6, and 2.8;
 - (B) Identified, evaluated, and commenced implementation, consistent with the implementation schedule set forth in the Plan, of all programs and projects included in the Plan that are locally cost effective and technically feasible which reduce reliance on the Delta; and
 - (C) Included in the Plan, commencing in 2015, the expected outcome for measurable reduction in Delta reliance and improvement in regional self-reliance. The expected outcome for measurable reduction in Delta reliance and improvement in regional self-reliance shall be reported in the Plan as the reduction in the amount of water used, or in the percentage of water used, from

⁴ Cal. Code Regs., tit. 23, § 5001, subd. (j): A "Covered action" is defined as "an activity which may cause either a direct physical change in the environment, or a reasonably foreseeable indirect physical change in the environment, or a reasonably foreseeable indirect physical change in the environment ... "directly undertaken by any public agency"" (Pub. Resources Code, § 21065) that (i) will occur, in whole or in part, within the boundaries of the Delta or Suisun Marsh, (ii) will be carried out, approved, or funded by the state or a local public agency, (iii) is covered by one or more provisions of the Delta Plan, and (iv) will have a significant impact on achievement of one or both of the coequal goals or the implementation of government-sponsored flood control programs to reduce risks to people, property, and state interest in the Delta."



the Delta watershed. For the purposes of reporting, water efficiency is considered a new source of water supply, consistent with Water Code section 1011(a)."

Preparation of UWMPs and Implementation of Projects from the UWMP

PWD completed and submitted to DWR, 2005, 2010, and 2015 Urban Water Management Plans, in addition to this 2020 UWMP. PWD has identified, evaluated and implemented projects that are locally cost effective and technically feasible which improve local reliability and reduce reliance on the Delta.

Expected Outcomes for Measurable Reduction in Delta Reliance

The expected outcomes for PWD's Delta reliance and regional self-reliance were developed based on the approach and guidance described in Appendix C of DWR's Urban Water Management Plan Guidebook 2020 (Draft version dated March 2021) and are summarized in Tables H-1 to H-3 below. This involves setting a baseline and evaluating normal year water demands (potable and non-potable), estimating service area population and water use in gallons per capita per day, evaluating and projecting water supply sources to meet estimated normal year demands including supplies from the Delta, local groundwater, conjunctive use projects, surface water, transfers and exchanges, and non-potable supplies. Inputs to Table H-1, H-2, and H-3 include:

- Baseline. In order to calculate the expected outcomes for measurable reduction in Delta reliance and improved regional self-reliance, a baseline is needed to compare against. For consistency with conversations had with DWR, PWD is using year 2010 as the baseline year. This analysis uses a normal water year representation of 2010 as the baseline. Data for the 2010 baseline were taken from PWD's 2005 UWMP as the UWMPs generally do not provide normal water year data for the year that they are adopted (i.e., 2005 UWMP forecasts normal year 2010, 2010 UWMP forecasts normal year 2015, and so on).
- Service Area Demands. Service area demands, including demands for non-potable water, for 2010, 2015, and 2020 were taken from projections from the previous (2005, 2010, and 2015) UWMPs. Service area demands 2025 to 2045 were taken from projections developed as part of the 2020 UWMP.
- Service Area Population. Consistent with the methodology for service area demands (using normal year projections from the previous UWMP), service area population for 2010 were taken from the previous (2005) UWMP. Consideration was given to using 2010 UWMP service area population projections for 2015 but because the 2015 UWMP had the benefit of complete Census data, year 2015 population data was taken from the 2015 UWMP. 2020 service area population projections were taken from the 2015 UWMP. Year 2025-2045 service area demands were taken from the 2020 UWMP.



The outcome of Table H-1 is a calculation of water use efficiency since the baseline year (2010). The calculation uses the change in gallons per capita per day and service area population to estimate water use efficiency in years 2015 through 2045 compared to the baseline year of 2010.

Supplies Contributing to Regional Self-Reliance. In Table H-2, the estimate of water
use efficiency is taken from Table H-1. Other water supplies, such as recycled water and
advanced water technologies were taken from previous UWMPs (2005 projections were
supplied for 2010 etc.). For years 2025-2045 local supplies were taken from projections
prepared for the 2020 UWMP.

The outcome of Table H-2 is an estimate of the supplies contributing to regional self-reliance.

 CVP/SWP Contract Supplies. CVP/SWP contract supplies were estimated based on the percentage of Delta supplies provided as a percent of overall imported supplies from the State Water Project. Given that all of PWD's imported supplies come directly from DWR, data provided in the 2019 Delivery and Capability Report was utilized to estimate the percentages of supplies from the Delta watershed.

The outcome of Table H-3 is a calculation of the percent change in supplies from the Delta watershed relative to the 2010 Baseline.

Table H-3 illustrates that from 2010 to 2015, PWD reduced reliance on the Delta and is projected to have a net reduction in reliance on the Delta from the baseline, through year 2045.



Table H-1: Calculation of Water Use Efficiency -To be completed if Water Supplier does <u>not</u> specifically estimate Water Use Efficiency as a supply

Service Area Water Use Efficiency Demands (Acre-Feet)	Baseline (2010)		2015	2020	2025	2030	2035	2040	2045
Service Area Water Demands with Water Use Efficiency Accounted For	31,034		35,000	22,720	19,720	20,310	21,480	22,780	24,250
Non-Potable Water Demands	2,500		1,000	2,500	500	1,000	1,500	2,000	2,000
Potable Service Area Demands with Water Use Efficiency Accounted For	28,534		34,000	20,220	19,220	19,310	19,980	20,780	22,250
Total Service Area Population	Baseline (2010)		2015	2020	2025	2030	2035	2040	2045
Service Area Population	132,801		164,312	131,200	126,002	128,998	138,554	145,962	153,76 6
	1						1	ı	
Water Use Efficiency Since Baseline (Acre-Feet)	Baseline (2010)		2015	2020	2025	2030	2035	2040	2045
Per Capita Water Use (GPCD)	192		185	138	136	134	129	127	129
Change in Per Capita Water Use from Baseline (GPCD)			(7)	(54)	(56)	(58)	(63)	(65)	(63)
Estimated Water Use Efficiency Since Baseline			1,305	7,970	7,853	8,407	9,790	10,582	10,789
							•		
Total Service Area Water Demands (Acre-Feet)	Baseline (2010)		2015	2020	2025	2030	2035	2040	2045
Service Area Water Demands with Water Use Efficiency	31,034		35,000	22,720	19,720	20,310	21,480	22,780	24,250
Reported Water Use Efficiency or Estimated Water Use Efficiency	- ,		1,305	7,970	7,853	8,407	9,790	10,582	10,789
Service Area Water Demands without Water Use Efficiency	31,034		36,305	30,690	27,573	28,717	31,270	33,362	35,039



Table H-2: Calculation of Supplies Contributing to Regional Self-Reliance

Water Supplies Contributing to Regional Self-Reliance (Acre-Feet)	Baseline (2010)		2015	2020	2025	2030	2035	2040	2045
Water Use Efficiency	0		1,305	7,970	7,853	8,407	9,790	10,582	10,789
Water Recycling	2,500		1,000	2,500	500	1,000	1,500	2,000	2,000
Stormwater Capture and Use									
Advanced Water Technologies									
Conjunctive Use Projects (Groundwater or Surface Water Augmentation)			2,600	5,000	5,325	5,325	5,325	5,325	5,325
Local and Regional Water Supply and Storage Projects (Groundwater)	10,310		12,000	6,280	4,140	2,770	2,770	2,770	2,770
Local and Regional Water Supply and Storage Project (Groundwater Return Flow Credits)					5,000	5,000	5,000	5,000	5,000
Other Programs and Projects the Contribute to Regional Self-Reliance (Surface Water)	3,405	=	4,000	4,000	4,000	4,000	4,000	4,000	4,000
Water Supplies Contributing to Regional Self-Reliance	16,215		20,905	25,750	26,898	26,502	28,385	29,677	29,884
	-			-	3	=	-	_	
Service Area Water Demands without Water Use Efficiency (Acre-Feet)	Baseline (2010)		2015	2020	2025	2030	2035	2040	2045
Service Area Water Demands without Water Use Efficiency Accounted For	31,034		36,305	30,690	27,573	28,717	31,270	33,362	35,039
				•		-	-		
Change in Regional Self Reliance (Acre-Feet)	Baseline (2010)		2015	2020	2025	2030	2035	2040	2045
Water Supplies Contributing to Regional Self-Reliance	16,215		20,905	25,750	26,898	26,502	28,385	29,677	29,884
Change in Water Supplies Contributing to Regional Self-Reliance			4,690	9,535	10,683	10,287	12,170	13,462	13,669
	I	1				Τ	I	I I	
Percent Change in Regional Self Reliance (As Percent of Demand w/out WUE)	Baseline (2010)		2015	2020	2025	2030	2035	2040	2045
Percent of Water Supplies Contributing to Regional Self-Reliance	52.2%		57.6%	83.9%	97.6%	92.3%	90.8%	89.0%	85.3%
Change in Percent of Water Supplies Contributing to Regional Self-Reliance			5.3%	31.7%	45.3%	40.0%	38.5%	36.7%	33.0%



Table H-3: Calculation of Reliance on Water Supplies from the Delta Watershed

		,		_						
Water Supplies from the De (Acre-Feet)	Ita Watershed	Baseline (2010)			2015	2015 2020	2015 2020 2025	2015 2020 2025 2030	2015 2020 2025 2030 2035	2015 2020 2025 2030 2035 2040
/P/SWP Contract Supplies		15,123		1	12,800	12,800 13,200	12,800 13,200 12,030	12,800 13,200 12,030 11,720	12,800 13,200 12,030 11,720 11,400	12,800 13,200 12,030 11,720 11,400 11,080
lta/Delta Tributary Diversions										
ansfers and Exchanges of Supplies from thansfer Agreement)	ne Delta Watershed (Butte	2,104	2	2	,600	,600 6,200	,600 6,200 5,700	,600 6,200 5,700 5,200	,600 6,200 5,700 5,200 5,200	,600 6,200 5,700 5,200 5,200 5,200
er Water Supplies from the Delta Watersh	ned	-		-						
/ater Supplies from the Delta Watersh	ed	17,227	1!	5,40	0	00 19,400	00 19,400 17,680	00 19,400 17,680 17,220	00 19,400 17,680 17,220 16,750	00 19,400 17,680 17,220 16,750 16,280
ee Area Water Demands without W Feet)	later Use Efficiency (Acre-	Baseline (2010)	2	2015		2020	2020 2025	2020 2025 2030	2020 2025 2030 2035	2020 2025 2030 2035 2040
Service Area Water Demands without Water	Use Efficiency Accounted For	31,034	3	6,305		30,690	30,690 27,573	30,690 27,573 28,717	30,690 27,573 28,717 31,270	30,690 27,573 28,717 31,270 33,362
Change in Supplies from the I (Acre-Feet)	Delta Watershed	Baseline (2010)	2	2015	202	20	20 2025	20 2025 2030	20 2025 2030 2035	20 2025 2030 2035 2040
Vater Supplies from the Delta Watershed		17,227	1!	5,400	19,400)	17,680) 17,680 17,220	17,680 17,220 16,750) 17,680 17,220 16,750 16,280
Change in Water Supplies from the Delta Wa	tershed		(1	1,827)	2,173		453	453 (7)	3 453 (7) (477)	3 453 (7) (477) (947)
							I			
Percent Change in Supplies from (As a Percent of Demand		Baseline (2010)	2	2015	2020)	2025	2025 2030	0 2025 2030 2035	0 2025 2030 2035 2040
Percent of Water Supplies from the Delta Wa	tershed	55.5%	4	12.4%	63.2%		64.1%	64.1% 60.0%	64.1% 60.0% 53.6%	64.1% 60.0% 53.6% 48.8%
Change in Percent of Water Supplies from th	e Delta Watershed		-1	13.1%	7.7%		8.6%	8.6% 4.5%	8.6% 4.5% -1.9%	8.6% 4.5% -1.9% -6.7%



Appendix I: Energy Intensity of Water System

Table O-1C: Recommen	nded Energy Reporting - Mult	tiple Water Delivery Produc	its							
Enter Start Date for Reporting Period End Date	1/1/2020		Urban Water Supplier Operational Control							
				Wa	ter Management	Process			Non-Consequential	Hydropower (if applicable)
	ls t	upstream embedded in the values reported?								
			Extract and Divert	Place into Storage	Conveyance	Treatment	Distribution	Total Utility	Hydropower	Net Utility
Water Volume Units	Total Volume of Water Ente	ering Process (volume units)	6549	0	4153	11356	0	N/A	9709	N/A
AF		Retail Potable Deliveries (%)	100%	100%	100%	100%	100%		100%	
	Ret	tail Non-Potable Deliveries (%)								
	WI	holesale Potable Deliveries(%)								
	Wholesa	ale Non-Potable Deliveries (%)								
		Agricultural Deliveries (%)								
		Environmental Deliveries (%)								
		Other (%)								
	Total Pe	ercentage [must equal 100%]	100%	100%	100%	100%	100%	N/A	100%	N/A
		Energy Consumed (kWh)	4533947	0	1861443	801978		7197368	1206418	8403786
	Energy Intensity (k	kWh/vol. converted to MG)	2124.6	#DIV/0!	1375.5	216.7	#DIV/0!	N/A	381.3	N/A

	Production Volume (volume units defined above)	Total Utility (kWh/volume)	Net Utility (kWh/volume)		
		Retail Potable Deliveries	22058	326.3	381.0
		Retail Non-Potable Deliveries	0	0.0	0.0
		Wholesale Potable Deliveries	0	0.0	0.0
	V	Vholesale Non-Potable Deliveries	0	0.0	0.0
		Agricultural Deliveries	0	0.0	0.0
		Environmental Deliveries	0	0.0	0.0
		Other	0	0.0	0.0
		All Water Delivery Types	22058	326.3	381.0

O	-4 6-14	Camanatad	Renewable	F
Ouantity	of Self	-Generated	Renewable	Energy

289553 kWh

Data Quality (Estimate, Metered Data, Combination of Estimates and Metered Data)

Metered Data

Data Quality Narrative:

	١	/alidated	meter	data was	provided b	y PWD
--	---	-----------	-------	----------	------------	-------

Narrative:

PWD kept track of energy consumed and volume of water for each source, treatment, or deliver.



Appendix J: 2020 Water Shortage Contingency Plan

Job #: 2044225*00

DRAFT 2020 Water Shortage Contingency Plan Palmdale Water District







2775 North Ventura Road, Suite 202 Oxnard, California 93036 805-973-5700

PUBLIC REVIEW DRAFT

Water Shortage Contingency Plan

14 May 2021

Prepared for

Palmdale Water District

2029 E. Ave Q. Palmdale, CA 93550

KJ Project No. 2044225*00

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List of Acronyms

District Palmdale Water District

DWR California Department of Water Resources

ERP Emergency Response Plan
PWD Palmdale Water District
SWP State Water Project

UWMP Urban Water Management Plan WSCP Water Shortage Contingency Plan

DWR Checklist Table for WSCP

Water Code Section	Summary as Applies to UWMP	2020 WSCP Location					
Subject:	Subject: Water Shortage Contingency Planning 2020 UWMP Guidebook Location: Chapter 8						
10632(a)	Provide a water shortage contingency plan (WSCP) with specified elements below.	Full Document					
10632(a)(2)(A)	Provide the written decision-making process and other methods that the supplier will use each year to determine its water reliability.	Section 2					
10632(a)(2)(B)	Provide data and methodology to evaluate the supplier's water reliability for the current year and one dry year pursuant to factors in the code.	Section 2					
10632(a)(3)(A)	Define six standard water shortage levels of 10, 20, 30, 40, 50 percent shortage and greater than 50 percent shortage. These levels shall be based on supply conditions, including percent reductions in supply, changes in groundwater levels, changes in surface elevation, or other conditions. The shortage levels shall also apply to a catastrophic interruption of supply.	Section 3.1					
10632(a)(3)(B)	Suppliers with an existing water shortage contingency plan that uses different water shortage levels must cross reference their categories with the six standard categories.	Section 3.1					
10632(a)(4)(A)	Suppliers with water shortage contingency plans that align with the defined shortage levels must specify locally appropriate supply augmentation actions.	Section 3.2.1					
10632(a)(4)(B)	Specify locally appropriate demand reduction actions to adequately respond to shortages.	Section 3.2.3					
10632(a)(4)(C)	Specify locally appropriate operational changes.	Section 3.2.2					
10632(a)(4)(D)	Specify additional mandatory prohibitions against specific water use practices that are in addition to state- mandated prohibitions are appropriate to local conditions.	Section 3.3.3.1					
10632(a)(4)(E)	Estimate the extent to which the gap between supplies and demand will be reduced by implementation of the action.	Table 3-4 and 3-7					
10632(a)(5)(A)	Suppliers must describe that they will inform customers, the public and others regarding any current or predicted water shortages.	Section 4.1.1					
10632(a)(5)(B) 10632(a)(5)(C)	Suppliers must describe that they will inform customers, the public and others regarding any shortage response actions triggered or anticipated to be triggered and other relevant communications.	Section 4.1.1					
10632(a)(7)(A)	Describe the legal authority that empowers the supplier to enforce shortage response actions.	Section 2.6					
10632(a)(7)(B)	Provide a statement that the supplier will declare a water shortage emergency Water Code Chapter 3.	Section 3					
10632(a)(7)(C)	Provide a statement that the supplier will coordinate with any city or county within which it provides water for the possible proclamation of a local emergency.	Section 2.6					
10632(a)(8)(A)	Describe the potential revenue reductions and expense increases associated with activated shortage response actions.	Section 7.1.1					
10632(a)(8)(B)	Provide a description of mitigation actions needed to address revenue reductions and expense increases associated with activated shortage response actions.	Section 7.1.2					
10632(a)(8)(C)	Describe the cost of compliance with Water Code Chapter 3.3: Excessive Residential Water Use During Drought.	Table 7-1					
10632(a)(9)	Retail suppliers must describe the monitoring and reporting requirements and procedures that ensure appropriate data is collected, tracked, and analyzed for purposes of monitoring customer compliance.	Section 5.2					
10632(a)(10)	Describe reevaluation and improvement procedures for monitoring and evaluation the water shortage contingency plan to ensure risk tolerance is adequate and appropriate water shortage mitigation strategies are implemented.	Section 1.3					



Section 1: Introduction

1.1 Overview

Water supplies may be interrupted or reduced significantly in a number of ways, such as a drought that limits supplies, an earthquake that damages water delivery or storage facilities, a regional power outage or a toxic spill that affects water quality. This Plan addresses the requirements in the California Water Code Section 10632, which requires that every urban water supplier shall prepare and adopt a Water Shortage Contingency Plan (WSCP) as part of its Urban Water Management Plan (UWMP). This WSCP serves as a guide for the intended actions by Palmdale Water District (PWD, the District) during water shortage conditions to improve preparedness for droughts and other impacts on water supplies by describing the process used to address varying degrees of water shortages.

Since the 1991 drought, PWD has approved and adopted numerous conservation resolutions from establishing a voluntary water conservation program, to implementing a water waste policy, declaring water shortage emergency conditions, identifying stages of action and response requirements, and establishing emergency water conservation regulations. Moreover, due to recent drought conditions and the Governor's emergency declarations that required a reduction in overall potable urban water use statewide, PWD developed ordinances and other planning documents to incentivize individual customer conservation and reduce overall water demands. Budget-based tiered water rates were introduced in May 2009 and updated in October 2019.

This WSCP describes the actions PWD will take to identify and respond to water shortage.

1.2 Plan Preparation, Adoption, Submittal and Availability

PWD began preparation of this WSCP in January 2021. The public hearing for the WSCP Plan was noticed in local newspapers (*TBD*), as prescribed in Government Code 6066, which included the time and place of the hearing (*Date and Place TBD*), as well as the location where the plan was available for public inspection. Interested parties, including other local agencies, were notified of the public hearing.

The final draft of the Plan was adopted by the PWD Board of Directors by Resolution No. 21-0XX (provided in Appendix C) and was submitted to the Department of Water Resources (DWR) within 30 days of approval. Additionally, the plan was made available for public review per the requirements of the Water Code.

1.3 Water Shortage Contingency Plan Refinement Procedures

PWD will convene the following departmental staff as needed to re-evaluate and improve procedures for systematically monitoring and evaluating the functionality of the WSCP to ensure shortage risk tolerance is adequate and appropriate water shortage mitigation strategies are implemented as needed:

- Water Use Efficiency Staff
- Administrative Staff
- Operational Staff

The WSCP will be reviewed, revised, and refined as appropriate and needed following significant changes to PWD supply portfolio, but no less than every 5 years.

1.4 Relationship to the Urban Water Management Plan

Water Code Section 10632(a) requires that every urban water supplier prepare and adopt a water shortage contingency plan as part of its urban water management plan. While the water shortage contingency plan is a stand-alone document it is updated and adopted in concert with the UWMP. Content of the water shortage are informed by the analysis of water supply reliability conducted pursuant to Water Code Section 10635 (contained in the UWMP). The reliability analysis of the UWMP considers "normal", "single-dry", and "5-year drought".

The reliability of PWD supply is highly dependent on the local groundwater sources, imported water availability, and local surface water availability. As shown in Table 1-1 (from Draft UWMP, subject to revision), in the near term (2021 to 2025) the total supplies are greater than demand in years 2022, 2024, and 2025. However, anticipated supplies are less than anticipated water demands in years 2021 and 2023. The WSCP identifies shortage reduction actions to reduce the shortage gap and actions to augment supplies.

Table 1-1 Near Term Water Supply Reliability Assuming 5-Year Drought

Parameter Parameter	2021	2022	2023	2024	2025
Gross Water Use	19,410	19,505	19,620	19,715	20,220
Total Supplies	<u>16,450</u>	<u>26,155</u>	<u>17,475</u>	19,980	24,680
Surplus/Shortfall w/o WSCP Action	-2,960	6,650	-2,145	265	4,460
WSCP - supply augmentation benefit	N/A	N/A	N/A	N/A	N/A
WSCP - use reduction savings benefit	<u>4,270</u>	<u>N/A</u>	<u>4,316</u>	<u>N/A</u>	N/A
Revised Surplus/(shortfall)	1,310	N/A	2,171	N/A	N/A
Resulting % Use Reduction from WSCP action	22%	N/A	22%	N/A	N/A

Note: Reformatted from UWMP Guidebook, Table 7-5 Five-Year Drought Risk Assessment Tables to address Water Code Section 10635(b)



Section 2: Procedures for the Annual Water Supply and Demand Assessment

The California Water Code Division 1, Section 350, states:

"The governing body of a distributor of a public water supply, whether publicly or privately owned and including a mutual water company, shall declare a water shortage emergency condition to prevail within the area served by such distributor whenever it finds and determines that the ordinary demands and requirements of water consumers cannot be satisfied without depleting the water supply of the distributor to the extent that there would be insufficient water for human consumption, sanitation, and fire protection."

New provisions in Water Code Section 10632.1. require that an urban water supplier such as PWD conduct an annual water supply and demand assessment ("Annual Assessment"), on or before July 1 of each year, to be submitted to DWR. An urban water supplier that relies on imported water from the State Water Project or the Bureau of Reclamation shall submit its Annual Assessment within 14 days of receiving its final allocations, or by July 1 of each year, whichever is later. The requirement to perform the Annual Assessment begins in July 2022. The procedures for performing the Annual Assessment are to be detailed in an urban suppliers' Water Shortage Contingency Plan.

This section of the WSCP provides the written procedure for PWD's Annual Assessment.

2.1.1 Timeline for Conducting the Annual Assessment

Table 2-1 provides targets for performing the Annual Assessment and outlines actions for a normal year and one year of drought. By starting to plan in July, PWD will get a snapshot of conditions and can begin to prepare to mitigate supply and start outreach to customers to manage demand. Major actions are proposed in January 2022, when an initial estimate of supply is made and compared to demand. A final annual assessment is proposed in April 2022.

Table 2-1. Timeline for Decision Making Process to Perform Annual Assessment

Target Date	Action
lul Doo	 Monitor supply sources
Jul-Dec	Monitor demand trends
	 Confirm anticipated weather (e.g., National Weather Service Climate Prediction Center, La Niña, US Drought Seasonal Outlook)
	 Confirm State Water Project (SWP initial allocation)
Jan	 Confirm available groundwater
	 Confirm groundwater production capacity
	 Evaluate storage in Littlerock Dam Reservoir available to PWD
	 Prepare initial assessment of Supplies (Supply Table 1)
Feb	Prepare informational item to the Board of Directors
	 Make initial assessment of unconstrained demand (<i>Demand Tables 1, 2, 3</i>)
	Make initial estimate of shortage
	 If shortage anticipated, form Water Shortage Task Force
Mar	Confirm current SWP allocation
	 Confirm groundwater production capacity
	 Estimate supply/storage in Littlerock Dam Reservoir available to PWD
	Start public outreach
April	 Complete Draft Annual Assessment and present to Board of Directors
	 If necessary, prepare notices of public hearing on water shortage
	Continue public outreach
	 Update Annual Water Assessment, present to Board of Directors
	 Finalize Annual Water Assessment and submit to DWR
May-July	 If necessary, declare water shortage and implement supply mitigations and demand reduction actions
	 Monitor customer response to water shortage messaging and other actions

2.2 Factors Affecting Demand and Supply

2.2.1 Weather Outlook

Weather affects PWD supplies in many ways. For many of the supplies, the effects of weather are seen over the long-term and are reflected in reservoir levels and groundwater levels. There are some resources and phenomena that can be considered when looking at the sources of supply:

- Potential for La Niña. ENSO (El Niño Southern Oscillation) is the warming and cooling of the ocean water along the Equator in the Eastern Pacific Ocean near South America. The warm phase is called El Niño and the cold phase is called La Niña. When the Eastern Pacific Ocean is 0.5 degrees Celsius above normal for 5 consecutive 3-month average periods, an El Niño is declared. When the Eastern Pacific Ocean is 0.5 degrees Celsius below normal for 5 consecutive 3-month average periods, a La Niña is declared. The El Niño and La Niña are declared as Weak, Moderate, or Strong depending on how far from normal the water temperature gets. When the temperature is above 1.5 degrees Celsius, it is declared as strong. When the temperature is above 1.0 degrees Celsius, it is declared as Moderate. When the temperature is above 0.5 degrees Celsius, it is declared as Weak. With El Niños, the High Desert tends experience increased precipitation, and decreased precipitation with La Niñas. The National Weather Service Climate Prediction Center provides information on potential for La Niña conditions.
- US Drought Information Seasonal Outlook. The National Weather Service Climate Prediction Center provides information geographically on drought conditions and categorizes geographies as "Drought Persists", "Drought Remains but Improves", "Drought Removal Likely", and "Drought Development Likely".

2.3 Current Year Unconstrained Demand

DWR guidance for the Annual Assessment is to consider the expected water use in the upcoming year, based on recent water use, and before any projected response actions a Supplier may trigger under its Water Shortage Contingency Plan.

2.3.1 Land Use

To evaluate water demand, PWD is required examine current and projected land uses. PWD incorporates City of Palmdale's information on land use in its Master Plan Updates and is part of the City's Development Advisory Board (DAB). The DAB participation will assist with relatively short-term forecasting of upcoming land use development. Using the known built and pending connections, a summarized total of the existing land use within the service area and potential future land use can used to assess total land use development.

2.3.2 Current Demand

PWD will create a table that will summarize the total water consumption (potable, recycled, and untreated) for each consumption category within the water service area for the most recent 5-year average, by month (*Demand Table 1*). Based on anticipated weather, *Demand Table 1*

may be adjusted to assume an increase in current demands. *Demand Table 1* will estimate existing demand in the current calendar year and demand in the subsequent calendar year. For the purposes of the analysis the subsequent year will be assumed to be a drought year.

2.3.3 Potential Demand

PWD will create a table showing anticipated demands from "Under Construction and Approved Projects" (*Demand Table 2*) derived from the Water Service Availability Letters issuance and conditions. In *Demand Table 2* anticipated water use will be forecasted by month. The calculations in *Demand Table 2* will develop or use any recently developed demand factors inclusive of water loss and including a contingency to account for annual demand variations that are likely to occur.

Demand Table 2 will reflect anticipated demands in the current calendar year and demand in the subsequent calendar year. For the purposes of the analysis the subsequent year will be assumed to be a drought year.

2.3.4 Total Near-Term Demands

Near-term water demands (*Demand Table 3*) will be the sum of the demands reflected in *Demand Table 1* plus *Demand Table 2*.

2.4 Assessing Supply in Current Year and One Dry Year

PWD will evaluate the total water sources available, including imported water, local groundwater, local surface water, recycled water, and other sources as they are put into service. Table 2-2 summarizes the factors to be considered.

Using Table 2-2 as a guide, PWD will develop a summary of each water source available in the upcoming year assuming the current and subsequent year will be dry years. *Supply Table 1* will also be developed, in which a quantified summary of each anticipated supply source is provided for the upcoming year assuming the current and subsequent year are dry years. Anticipated water supply will be forecasted by month using past supply patterns.

2.5 Assessing Water Supply Reliability

PWD will compare *Supply Table 1* and *Demand Table 3* and determine if a supply shortage is anticipated, the level of shortage, and prepare if necessary, to implement its water shortage contingency plan.

2.6 Steps Following the Annual Assessment

The District has the power and authority to implement and enforce its shortage response actions including mandatory water conservation measures within its boundaries per Division 11 of the California Water Code as previously exercised by Resolution No. 09-04, which was adopted in March 2009. Shortage response actions are described in Section 3. PWD will declare the appropriate stage of a water shortage emergency in accordance with Chapter 3, commencing with Section 350, of Division 1 of the California Water Code. Should a water shortage be declared, PWD may coordinate with the City of Palmdale and the County of Los Angeles for the possible proclamation of a local emergency, as defined in Section 8558 of the Government Code.

Source	Table 2-2. Annual Assessn Factors to be Evaluated in Current Year	nent of Supply Establishing Supply in Assumed Subsequent Dry Year
Local Groundwater	Regulatory limitations	Regulatory limitations
	Groundwater level	Groundwater level
	Any constraints on supply due to infrastructure or water quality	Any constraints on supply due to infrastructure or water quality
	Consider if supply would be managed differently if it is known subsequent year will be dry year	
Local Surface Water	Regulatory limitations	Regulatory limitations
	Any constraints on supply due to infrastructure or water quality	Any constraints on supply due to infrastructure or water quality
Imported Water (SWP)	Water supply available under contract with DWR and any existing transfers and exchanges	Water supply available under contract with DWR and any existing transfers and exchanges
	Any constraints on supply due to infrastructure or water quality	Any constraints on supply due to infrastructure or water quality
	Consider if supply would be managed differently if it is known subsequent year will be dry year	
Recycled Water	What is current annual recycled water production capability	What is current annual recycled water production capability
	What is current annual demand + new (12 months) demand	What is current annual demand + new (24 months) demand



Section 3: Six Standard Water Shortage Levels

3.1 Stages of Action to Respond to Water Shortages

As required by California Water Code Section 10632(a)(3)(A), this WSCP is framed around six standard water shortage stages, which correspond to progressive ranges of percent supply reductions from zero to more than fifty percent. Table 3-1 presents a description of the six water supply shortage stages, defined as stages I to VI.

Each stage may be triggered by a declaration from federal or state authorities, or PWD to address events that result in a water shortage. The stages and applicable water supply conditions are summarized in Table 3-1 and Table 3-2.

Table 3-1: Rationing and Reduction Goals

Deficiency or State Mandated Reduction	Stage	Demand Reduction Goal	Type of Program	Water Shortage Condition
1-10%	1	10% reduction	Voluntary	Minor Shortage
11-20%	2	20% reduction	Mandatory	Moderate Shortage
21-30%	3	30% reduction	Mandatory	Severe Shortage
31-40%	4	40% reduction	Mandatory	Critical Shortage
41-50%	5	50% reduction	Mandatory	Emergency Shortage
>50%	6	>50% reduction	Mandatory	Catastrophic Failure

DWR Table 8-1

Table 3-2. Stages of PWD Water Shortage Contingency Plan

Stage	Percent Supply Reduction	Triggers
ı	Up to 10%	 Results of the Annual Assessment Federal, state or local disaster declaration that may impact water supplies State declaration due to drought or system maintenance Unplanned PWD water system maintenance
II	Up to 20%	 Results of the Annual Assessment Federal, state or local disaster declaration that may impact water supplies State declaration due to drought or system maintenance Unplanned PWD water system maintenance requiring more time to repair

Stage	Percent Supply Reduction	Triggers
III	Up to 30%	 Results of the Annual Assessment Federal, state or local disaster declaration that may impact water supplies State determination due to drought or significant system failure; and/or Unplanned PWD water system failure or emergency
IV	Up to 40%	 Federal, state or local disaster declaration that may impact water supplies State determination due to drought or significant system failure; and/or Unplanned PWD water system failure or emergency
V	Up to 50%	 Results of the Annual Assessment Federal, state or local disaster declaration that may impact water supplies State determination due to drought or significant system failure; and/or Advanced PWD water system failure or emergency
Stage VI	50% or higher	 Results of the Annual Assessment Federal, state or local disaster declaration that may impact water supplies State determination due to drought or significant system failure Natural or human-caused catastrophe disrupting delivery of water to, or within the service area Severe PWD water system failure

3.1.1 Procedures for Water Shortage Level Determination

The results of the Annual Assessment will be used to determine the water shortage level. In case of emergencies, a special meeting may be called by a majority of the Board on less than twenty-four-hour notice and without an agenda to deal with the disruption of service. If an emergency arises which would ordinarily be brought to the attention of the Board, but insufficient time exists, the General Manager has administrative authority to take action as deemed appropriate and reasonable.

3.2 Water Shortage Response Actions

Once a shortage stage is declared, PWD may implement shortage response actions required by the customer and through operational changes, as listed in Table 3-3. These actions will be supported by communication protocols (discussed in Section 4.1.1), enforcement actions (discussed in Section 3.3.2) and monitoring and reporting efforts (discussed in Section 5.2) activities appropriate at each shortage stage level.

Table 3-3: Customer and PWD Water Shortage Actions

Stage	District Actions	Customer Actions
Stage I	 Initiate public information campaign Increase awareness of conservation measures and water use efficiency programs Conduct focused outreach to large water users Consider coordination of public outreach with the cities and County Publish Water Shortage Event Contingency Plan stages and actions per stage Consider implementation of drought factor for customer bill calculation Consider enforcement of conservation measures 	 Comply with PWD Water Waste Policy (see Table 3-3 and Appendix B) Voluntary water conservation Adhere to conservation measures Consider conversion to more efficient irrigation methods Consider turf removal and conversion to Water Wise Landscape Patronize local carwashes that recycle their water Consider PWD Water Use Efficiency Rebate Programs
Stage II	 Continue previous action Expand public information campaign Commence enforcement of conservation measures Implement of drought factor for customer bill Suspend issuance of potable construction meters. 	 Comply with PWD Water Waste Policy (see Table 3-3and Appendix B) Comply with mandatory conservation regulations Continue previous actions
Stage III	 Continue previous actions Intensify public information campaign Expand enforcement of conservation measures Provide regular media public briefings Activate emergency connections with mutual aid agencies Evaluate size of monetary fines for water waste Begin water waste patrols 	 Comply with PWD Water Waste Policy (see Table 3-3and Appendix B) Continue previous actions Limit washing of sidewalks, driveways, walkways, parking lots, or any other hard-surfaced area by hose or flooding unless otherwise necessary Comply with prohibited outdoor irrigation of ornamental landscape or turf with potable water through an irrigation system between 9:00 am and 6:00 pm and limit system use to two days a week
Stage IV	Continue previous actions	 Comply with PWD Water Waste Policy (see Table 3-3and Appendix B) Continue previous actions Obligation to fix leaks, breaks, or malfunctions within 48 hours
Stage V	 Continue previous actions Enforce mandatory water consumption goals and allocations for all customers and users 	 Comply with PWD Water Waste Policy (see Table 3-3and Appendix B) Continue previous actions
Stage VI	Continue previous actionsImplement crisis communication planActivate Emergency Operations Center	Continue previous actionsTerminate outdoor water use for irrigation, pools and

Stage	District Actions	Customer Actions
	 Coordinate actions with regulatory agencies Coordinate actions with public safety agencies to address enforcement and fire protection issues Recall all temporary meters and activate water fill stations Suspend issuance of new development approvals and new water connections other than those required to be processed by state law 	fountains Water may only be used outdoors for public health and safety purposes Be on alert for Boil Water Orders if they become necessary

3.2.1 Supply Augmentation

Any water shortage event should trigger a review of potential sources for supplemental water supply. Potential sources for supplemental water include increasing allocation of State Water Project water (infrastructure not currently available) or utilizing water from the Palmdale GRRP. Any supplemental water supply project or improvements to existing facilities to allow for entitled flows should be a priority for consideration in immediate capital projects if shortage (e.g., demands exceeding supplies) greater than ten percent is anticipated or when a Stage 3 Water Shortage Event continues for more than 18 months. Additional supply sources for consideration include replacement or rehabilitated wells increased use of reclaimed water, and other alternatives based on the actual circumstances at that time. Supply augmentation in near term is presented in Table 3-4 below.

Table 3-4. Supply Augmentation Actions

Shortage Level	Supply Augmentation Methods and Other Actions by Water Supplier (based on DWR's WUE database categories)	How much is this going to reduce the shortage gap?	Additional Explanation or Reference
3	Groundwater	2,000 AF	Pump Additional Groundwater
4	Groundwater	1,000 AF	Pump Additional Groundwater
5	Groundwater	1,000 AF	Pump Additional Groundwater
6	Groundwater	500 AF	Pump Additional Groundwater

Note: (DWR Table 8-3)

3.2.2 Operational Changes

PWD shall comply with the restrictions similar to those implemented for the public to the extent possible. Hydrant flushing shall be limited except as deemed necessary by the General Manager to enhance water quality or to conduct fire flow and large meter tests. Other actions include efficient water use practices identified in Table 3-5, such as minimizing waste of water in construction, following a modified outdoor landscape watering schedule for PWD facilities depending on shortage stage, and fixing any identified leaks in the distribution system or other related water infrastructure components.

3.2.3 **Demand Reduction Actions**

PWD permanently implements general water conservation measures and irrigation practices aimed at increasing everyday water use efficiency. Those measures, plus those to be enacted in the various stages, are presented in Table 3-5 and are also indicated in the District's Water Waste Policy.

Table 3-5. Prohibitions During Different Shortage Stages

Stage	Prohibition/Requirement
	Water waste is prohibited at all times. Water waste includes but is not limited to: • Application of potable water to outdoor landscapes in a manner that causes runoff.
	 Water leaks shall be repaired in a timely manner and sprinklers shall be adjusted to eliminate over-spray.
	 Hosing of hardscape surfaces, except where health and safety needs dictate, is prohibited.
	 No watering of outdoor landscapes within 48 hours of measurable rainfall.
In Effect at All Times	 Car washing and outside cleaning activities prohibited except when performed with buckets and automatic hose shutoff devices.
	 The serving of drinking water other than upon request in eating or drinking establishments is prohibited.
	 Operators of hotels and motels shall provide guests with the option of choosing not to have towels and linens laundered daily. The hotel or motel shall prominently display notice of this option in each guestroom.
	Other
	 Water for construction purposes, including but not limited to de- brushing of vacant land, compaction of fills and pads, trench backfill, and other construction uses shall be in an efficient manner.
Stage I	Same as In Effect At All Times
	All restrictions/prohibitions/initiatives from Stage I are in effect
	 Landscape watering between the hours of 1000 and 1800 hours is prohibited
Stage II	 Outdoor watering is limited to 3 days per week.
	 Irrigation with potable water outside of newly constructed homes and buildings not delivered by drip or microspray is prohibited.
	Suspend issuance of potable water construction meters.

Stage	Prohibition/Requirement
	 All restrictions/prohibitions/initiatives from Stage I and Stage II are in effect and are mandatory.
Stage	 Irrigation with potable water of ornamental turf on public street medians is prohibited.
III	 Outdoor watering is limited to 2 days per week.
	 Potable water cannot be used to maintain fountains, reflection ponds and decorative water bodies for aesthetic or scenic purposes, except where necessary to support aquatic life.
	 All restrictions/prohibitions/initiatives from Stage I, Stage II, and Stage III are in effect and are mandatory.
	 Outdoor watering is limited to 1 day per week.
Stage IV	 Filling of new swimming pools, spas, hot tubs, or the draining and refilling of existing pools, etc is prohibited. Topping off is allowed to the extent that the designated water allocation is not exceeded.
	 Meters will only be installed for new accounts where the building permit was issued prior to the declaration of the water shortage.
Chara V	Filling of new swimming pools, spas, hot tubs, or the draining and refilling of existing pools, etc is prohibited. Topping off is allowed to the extent that the designated water allocation is not exceeded.
Stage V	 Meters will only be installed for new accounts where the building permit was issued prior to the declaration of the water shortage
	All restrictions/prohibitions/initiatives from previous Shortage Stages are in effect and are mandatory.
Stage	No meters will be installed for new accounts.
VI	 Outdoor irrigation is prohibited, with the exception of drip or hand watering to preserve established trees.

As described in the table above, prohibitions and restrictions on water features that are artificially supplied with water, such as ornamental lakes, ponds and decorative fountains are treated differently from swimming pools and spas, as defined in Section 115921 of the California Health and Safety Code.

3.2.3.1 Emergency Response Plan

In order to prepare for catastrophic events, the PWD has prepared an Emergency Response Plan (ERP) in accordance with other state and federal regulations. The purpose of the ERP is to design actions necessary to minimize the impacts of supply interruptions due to catastrophic events.

The ERP includes PWD's standardized response and recovery procedures to prevent, minimize, and mitigate injury and damage resulting from emergencies or disasters. The ERP includes, or is planned to include incident response procedures for the following incidents:

- Evacuation
- Earthquake
- Fire
- Wildfire
- Flood
- Power Outage
- Drought
- HazMat Release

- Security Incidents
- Bomb Threat
- Single-Employee Security Incident
- Personnel Injury
- Contamination
- Transmission/Main Break
- Distribution Line Break
- Pandemic

The plan considers the various aspects of the potential for malevolent threats or actual terrorism. The information contained in the ERP is intended to guide staff and inform other emergency responding agencies and includes plans, procedures, lists, and identification of equipment, emergency contacts, etc.

3.2.3.2 Seismic Risk Assessment and Mitigation Plan

PWD owns and operates water storage and distribution, treatment, and groundwater pumping facilities. The water distribution system is comprised of two separate systems – one for potable water and the other for recycled water. In 2021 PWD performed the following to understand, plan, for and mitigate seismic risk:

- Evaluated seismic risk zone for the PWD service area
- Identified critical water facilities and seismic and building deficiencies
- Identified mitigation measures to reduce seismic risk at facilities.

This section summarizes the 2020 seismic risk assessment and provides an update of the seismic vulnerability of the drinking water supply, treatment, storage, and distribution facilities and mitigation plan for the water system (Kennedy Jenks 2021). The Seismic Evaluation is included in Appendix C.

3.2.3.2.1 Seismic Evaluation and Mitigation for Steel Tanks

Geotechnical work was conducted for PWD's above-ground potable water reservoirs located on 19 sites in the Palmdale area, to classify sites for repair and retrofit needs. Design level earthquake values were identified for each tank evaluation, corresponding to the appropriate American Society of Civil Engineers design level earthquake.

A seismic evaluation was performed to identify seismic deficiencies and recommend strengthening measures for each of the welded carbon steel tanks. Work included a written description for each tank summarizing the results of the interior and exterior inspections and condition assessments; and the findings of the desktop evaluation.

Several tanks were found to have deficiencies, due to one or more of the following:

- age of the tank
- code which was applicable at the time the tank was designed,
- dimensions of the tank diameter to height ratio,
- lack of anchorage to foundations

The tank structural and seismic evaluation investigated several mitigation concepts in order to bring the tanks within code compliance. These mitigation concepts included arranging for a civil or structural engineer to inspect PWD facilities, consulting with a geotechnical engineering firm to perform site investigations and provide a more detailed analysis, increasing freeboard height to accommodate wave action, and combinations of these.

PWD will prioritize tanks for repairs and replacement based on the likelihood and consequences of various types of damage associated with code compliance issues identified.

3.2.3.2.2 Seismic Evaluation and Mitigation for Pump Stations, Pressure Reducing Valves, Wells or Well Pump Stations

Seismic assessments were performed for the booster pump stations, wells, and booster pump buildings. Work included documentation of facility descriptions, seismic deficiencies, and seismic mitigation measures. Many of these facilities had identified deficiencies associated with anchorage to foundations and walls, inadequate load path to transfer later loads, and thin slabs. Similar to the tank evaluation, additional analysis is recommended.

3.3 Benefit of Shortage Response Actions

As discussed above, supply actions and actions within PWD operations will help reduce water shortage. Closing the "gap" between supplies and demands through customer actions, will include:

- Public Information
- Enforcement
- Restrictions on Non-Essential Water Uses
- Pricing

The water shortage response actions and their anticipated effect are summarized in Table 3-7.

3.3.1 Public Information

Without exception, experience has shown that a well-informed public is generally more willing to heed requests to voluntarily conserve or alter water use patterns and will be more likely to comply if mandatory water use restrictions become necessary. DWR (2008) estimates that public information campaigns have alone reduced demand in the range of **5 to 20** percent, depending on the time, money, and effort spent. Public information supports voluntary and mandatory measures by educating and convincing the public that a critical water shortage exists and provides information on how water is used and how they can help. The DWR Drought Guidebook highlights that when the public perceives a drought to be severe, they change behaviors (such as flushing the toilet less often).

The information provided to the public should include a description of the conditions that will trigger implementation of shortage stages as well as a description of what the plan entails (restrictions, enforcement provisions, etc.). It is also advisable to provide practical "consumer" information that will help water users comply with the plan. For example, information about restrictions on lawn watering might be accompanied with information about proper lawn watering practices.

Based on past experience, with minimal public outreach, a water savings of 5 percent is assumed, with extensive public outreach a water savings of 7 percent is assumed, public information combined with enforcement (see section 3.3.2) is assumed to achieve a savings of up to 22 percent.

3.3.2 Enforcement

A study examining the effectiveness of drought management programs in reducing residential water-use (Virginia Polytechnic Institute 2006) showed considerable variation in the effectiveness of drought management programs and highlighted the importance of public information and enforcement. Results, shown in Table 3-6, indicate that overall reductions in residential water-use ranged from 0-7 percent for voluntary restrictions and from 0-22 percent for mandatory restrictions. The observed differences were statistically attributed to information efforts for voluntary restrictions and both information and enforcement efforts for mandatory restrictions.

Table 3-6. Drought Program Management Variables Effect on Residential Water-Use

	Estimated Change in	Statistically Different than No
Classification	Water-Use	Effect?
Voluntary Restrictions		
Little or no information disseminated	-2%	No
Moderate level of information	-2%	No
Aggressive information dissemination	-7%	Yes
Mandatory Restrictions		
Low information and low enforcement	-5%	No
Moderate information and low enforcement	-6%	Yes
Aggressive information and low enforcement	-12%	Yes
Low information and moderate enforcement	-4%	No
Moderate information and enforcement	-9%	Yes
Aggressive information and moderate enforcement	-15%	Yes
Moderate information and aggressive enforcement	-20%	Yes
Aggressive information and enforcement	-22%	Yes

Source: Virginia Polytechnic Institute 2006

The analysis highlights the key role that public outreach and information plays in the success of drought response actions. Voluntary restriction programs with little to moderate levels of information dissemination had no appreciable effect on water-use. Voluntary restriction programs with active promotional efforts, however, reduced water-use by an estimated 7 percent from what would have otherwise occurred without any restriction program. Thus, for voluntary restrictions, only the most intense programs had even a moderate level of success in reducing water-use.

The analysis highlights the key role that public outreach and information plays in the success of drought response actions. Voluntary restriction programs with little to moderate levels of information dissemination had no appreciable effect on water-use. Voluntary restriction programs with active promotional efforts, however, reduced water-use by an estimated 7 percent from what would have otherwise occurred without any restriction program. Thus for voluntary restrictions, only the most intense programs had even a moderate level of success in reducing water-use.

Mandatory restriction programs without a significant enforcement component broadly mirrored the outcomes achieved by the voluntary programs. Programs with mandatory restrictions that invested minimal effort in information dissemination did not appreciably reduce residential water-use. Programs with no active enforcement efforts but with moderate to high levels of informational dissemination achieved 6 and 12 percent reductions in water-use, respectively. These estimated reductions are similar to those achieved by voluntary programs with aggressive informational campaigns.

The experience the City of Santa Cruz had implementing its Drought Contingency Plan and successfully reaching its reduction goals supports the importance of a strong public information program. Analysis of the implementation program identified the key ingredient to its success was "the public's understanding, awareness, and belief that the City was confronted with a true water shortage problem. Media coverage of water problems across California reinforced the situation. Without that sense of a real and imminent problem, it's likely the level of cooperation and willingness demonstrated by the community in making changes they did might have been considerably reduced." (Santa Cruz 2010)

Delivering accurate and timely information to water users, news media and local governments with updates on conditions, restrictions, and helpful contact information is key.

With aggressive information dissemination and enforcement its assumed PWD could achieve a 22 percent water savings.

3.3.3 Restrictions on Non-Essential Water Uses

PWD's water waste policy focuses on curtailing water waste and non-essential water use. Outdoor water use, including washing sidewalks and watering ornamental landscapes is targeted. These uses are typically considered to be discretionary or nonessential, are highly visible, and therefore relatively easy to monitor, and often are a substantial component of water demand, particularly during the summer months when drought conditions are likely most severe.

Given the significance and visibility of lawn watering as the predominant component of seasonal use, best management practices in drought contingency plans typically prescribe time-of-use and other restrictions on lawn watering. This often involves placing water users on a schedule which allows for staggered lawn watering days, as well as restrictions on the times during the day when lawns can be watered. Additionally, this may include the suspension of potable water construction meters.

The American Waterworks Association estimates that voluntary outdoor water use limits can result in a water savings of **up to 10 percent** and mandatory outdoor water limits can achieve **up to a 56** percent reduction in outdoor water use (AWWA 2008, AWWA 2011). Specifically, case studies found that:

Restricting water use to every third day reduced water use by 22 percent

- Restricting water use to twice a week reduced water use by 33 percent
- Restricting water use to once a week saved 56 percent

PWD performed a detailed review of water use as part of its 2019 Financial Planning Study (PWD 2019). This analysis estimated that for residential customers, approximately 52% of water use was outdoors. Residential water demand makes up approximately 77% of PWD's overall demands Therefore:

- Voluntary outdoor water limits that saved 10% of outdoor residential demands would reduce overall water demand by 4% (0.1*0.52*0.77).
- Restricting water use to twice a week could reduce outdoor water use by 33%, reducing overall water demand by 13% (0.33*0.52*0.77).
- Restricting water use to once a week could reduce outdoor water use by 56%, reducing overall water demand by 22% (0.56*0.52*0.77).

3.3.3.1 Additional Mandatory Restrictions

The State, through the State Water Board, adopted drought emergency conservation regulations in July 2014. The Board expanded, updated, extended, and readopted the emergency regulations several times and in the prohibitions on wasteful water use practices were in place until November 25th, 2017.

As directed by Executive Order B-40-17, the State Water Board is conducting a rulemaking to put in place permanent prohibitions on wasteful water use practices. This rulemaking is part of the broader legislation, *Making Water Conservation a California Way of Life*.

The specific outcome of the permanent prohibitions cannot be known at this time. The emergency conservation regulations in effect through November 2017 included the following prohibitions:

- Application of potable water to outdoor landscapes in a manner that causes runoff such that water flows onto adjacent property, non-irrigated areas, private and public walkways, roadways, parking lots, or structures;
- The use of a hose that dispenses potable water to wash a motor vehicle, except where
 the hose is fitted with a shut-off nozzle or device attached to it that causes it to cease
 dispensing water immediately when not in use
- The application of potable water to driveways and sidewalks
- The use of potable water in a fountain or other decorative water feature except where the water is part of a recirculating system
- The application of potable water to outdoor landscapes during and within 48 hours after measurable rainfall
- The serving of drinking water other than upon request in eating or drinking establishments
- Irrigation with potable water of ornamental turf on public street medians.

The emergency conservation regulations further required that:

- The irrigation with potable water of landscapes outside of newly constructed homes and buildings in a manner inconsistent with regulations or other requirements established by the California Building Standards Commission and the Department of Housing and Community Development
- Commercial, industrial, and institutional properties shall limit outdoor irrigation of ornamental landscapes or turf with potable water to no more than two days per week

PWD's water use restrictions are consistent with the State's prohibitions to prevent water waste. However, dependent on the declared drought stage, PWD may have restrictions and requirements in addition to those of the State such as:

- Limiting outdoor irrigation of ornamental landscape or turf with potable water to certain hours and to certain days of the week (all customer types, not just Commercial, Industrial, or Institutional properties)
- Prohibiting all outdoor irrigation with potable water
- Prohibiting filling of swimming pools, spas, and wading pools

3.3.4 Drought Surcharge Rates

PWD has a drought rate structure to recover costs related to increased effort during drought. While not a specifically meant to reduce water demand, drought surcharge rates are expected to decrease water demands.

Past studies reveal that water use decreases when utilities install water meters and impose commodity charges. AWWA estimates that water use decreases between 15 to 40 percent when customers are charged a commodity rate rather than a flat rate (AWWA 2008). This indicates that customers are price sensitive and will adjust habits to reduce their cost of water. The actual extent that increasing rates during a drought can result in decreased water use is uncertain.

AWWA studies indicate that the effectiveness of pricing to reduce water use is very dependent on the affluence of the water utility customer base. As a rule of thumb, AWWA estimates that marginal price increases in water (up to 10 percent) reduce water use by 1.5 to 7 percent; price increases greater than 10 percent are necessary to achieve water use reductions greater than 10 percent (AWWA 2008).

Based on AWWA data its assumed that water use reductions of 10 to 15 percent will be achieved with drought rates.

Table 3-7. Effectiveness Demand Reduction and Other Actions

Shortage Level	Demand Reduction Actions	Reduction in Shortage Gap	Explanation	Penalty, Charge, or Other Enforcement?
1	Expand Public Information Campaign	7%	Based on AWWA 2008 assumes savings of 7%	No
2	Expand Public Information Campaign	22%	Based on AWWA 2008 assumes savings of 22% with enforcement	Yes
2	Implement or Modify Drought Rate Structure or Surcharge	10%	Based on AWWA 2011 assumes savings of 10%	Yes
3	Expand Public Information Campaign	22%	Based on AWWA 2008 assumes savings of 22% with enforcement	Yes
3	Implement or Modify Drought Rate Structure or Surcharge	10%	Based on AWWA 2011 assumes savings of 10%	Yes
3	Landscape - Other landscape restriction or prohibition	4%	Outdoor water limited to 3 days a week. Based on AWWA 2011.	Yes
4	Expand Public Information Campaign	22%	Based on AWWA 2008 assumes savings of 22% with enforcement	Yes
4	Implement or Modify Drought Rate Structure or Surcharge	15%	Based on AWWA 2011 assumes savings of 15%	Yes
4	Landscape - Other landscape restriction or prohibition	13%	Outdoor water limited to 2 days a week. Based on AWWA 2011.	Yes
5	Expand Public Information Campaign	22%	Based on AWWA 2008 assumes savings of 22% with enforcement	Yes
5	Implement or Modify Drought Rate Structure or Surcharge	15%	Based on AWWA 2011 assumes savings of 15%	Yes
5	Landscape - Other landscape restriction or prohibition	22%	Outdoor water limited to 1 day a week. Based on AWWA 2011.	Yes

Table 3-7. cont.

Shortage Level	Demand Reduction Actions	Reduction in Shortage Gap	Explanation	Penalty, Charge, or Other Enforcement?
6	Expand Public Information Campaign	22%	Based on AWWA 2008 assumes savings of 22% with enforcement	Yes
6	Implement or Modify Drought Rate Structure or Surcharge	15%	Based on AWWA 2011 assumes savings of 15%	Yes
6	Landscape - Other landscape restriction or prohibition	52%	Outdoor water use prohibited	Yes

DWR Table 8-2

Section 4: Communications Protocols

4.1.1 Communications Protocols and Customer Outreach

Customer participation is a key element in responding to a supply shortage, while general media coverage of a drought is likely to increase awareness. Multiple communication channels will continue to be used by PWD staff to communicate water shortage conditions and necessary actions to the PWD Board of Directors, customers, residential homeowners associations, business chambers, inter-governmental bodies, essential facilities (schools, hospitals, fire and police department), and other stakeholders. Communication methods include the following:

- Public water conservation forums hosted at PWD headquarters, off- site locations, or through virtual platforms.
- Attendance and agenda presentation at local city council meetings.
- Attendance and agenda presentations at home-owners association and business chamber meetings.
- Direct mailings and bill inserts to customers and account holders.
- Press releases.
- PWD publications, e.g., "The Pipeline".
- Updated posting of issues and information on PWD website.
- Advertisements in local publications and cable channels.
- Cards, table tents, door hangers and other leave-behind reminders.
- Social media updates and postings



Table 4-1. Communication Protocols and Procedures to Support Shortage Response **Actions**

Shortage Stage	Percent Supply Reduction	Communication Protocols and Procedures (Outreach to customers when each Stage is declared)
I	Up to 10%	 Declaration and notification of water supply shortage I by resolution, and adoption at a public meeting in accordance with state law. Notification of supply shortage in Public Newspaper
II	Up to 20%	 - Declaration and notification of water supply shortage II by resolution, and adoption at a public meeting in accordance with state law. - Notification of supply shortage in Public Newspaper - Advertisement in Local Public Newspaper - Commence social media updates - Notify top 5 water users in each customer class, e.g. residential, and CII
III	Up to 30%	 - Declaration and notification of water supply shortage III by resolution, and adoption at a public meeting in accordance with state law. - Notification of supply shortage in Public Newspaper - Advertisement in Local Public Newspaper and local cable channel - Schedule regular media, city council and County briefings - Continue social media updates - Targeted Messaging to customers - Notify top 10 water users in each customer class, e.g. residential, and CII
IV	Up to 40%	 Declaration and notification of water supply shortage IV by resolution, and adoption at a public meeting in accordance with state law. Notification of supply shortage in Public Newspaper Advertisement in Local Public Newspaper and local cable channel Continue regular media, city council and County briefings Continue social media updates Targeted Messaging to customers Notify top 15 water users in each customer class, e.g. residential, and CII
V	Up to 50%	 Declaration and notification of water supply shortage V by resolution, and adoption at a public meeting in accordance with state law. Notification of supply shortage in Public Newspaper Advertisement in Local Public Newspaper and local cable channel Continue regular media, city council and County briefings Continue social media updates Targeted Messaging to customers Notify top 20 water users in each customer class, e.g. residential, and CII
VI	50% of More	 Declaration and notification of water supply shortage VI by resolution, and adoption at a public meeting in accordance with state law. Notification of supply shortage in Public Newspaper Advertisement in Local Public Newspaper and local cable channel Continue regular media, city council and County briefings Continue social media updates Targeted Messaging to customers Notify top 25 water users in each customer class, e.g. residential, and CII

Section 5: Monitoring and Reporting

Monitoring is essential to ensure that the response actions are achieving their intended water use reduction purposes, or if improvements or new actions need to be considered.

5.1 Mechanism to Determine Reductions in Water Use and to Meet State Reporting Requirements

The PWD has meters on all residential, commercial and landscape service connections in the service area and requires meters on all new connections. These meters record the amount of water consumption at each location. These meters in combination with billing information will be used to monitor actual reductions in water use.

5.2 Monitoring and Reporting

Certain aspects of water conservation can be readily monitored and evaluated, such as metered water use and production quantities. Other aspects such as public education are more difficult to measure in terms of effectiveness. Additionally, weather patterns make it more difficult to compare one year's water demand and conservation results with another year's usage.

When severe shortages occur and some degree of mandatory reduction is required, a program's effectiveness can be judged directly by water billings. In these cases, targeted results must be met, and even reluctant customers will, on the whole, meet the goals. Specific methods to evaluate effectiveness of water conservation programs to be employed by PWD are:

- Monitoring of Metered Water Usage This will determine how much has been used.
 Compiling statistics to track usage of customer groups to determine trends is currently
 being done through the water billing computer system. Meter readings/billings can be
 compared and analyzed to determine the effectiveness of conservation for all customer
 classes.
- Monitoring Production Quantities In normal water supply conditions, production figures
 are recorded daily by the District's automated system. The Water Production Supervisor
 and the Production Lead monitor the accuracy of the monthly production totals. The
 totals are incorporated into the monthly water supply report to the State by the Water
 Treatment Supervisor.

To verify that conservation reduction goals are being met, production and metered usage reports will be provided to General Manager during each stage of the conservation period. Water production figures will be compared to previous year production figures for the same time period to ascertain if conservation goals are being reached. Results will be posted on the Palmdale Water website, as appropriate.

Additional actions available to PWD include:

- 1. Transition of remaining customer water meters to "smart meters" and investment in automated system to improve customer interface to allow more timely monitoring by customer of water use patterns.
- 2. Provide incentives to property owners to install individual meters or sub-meters in multi-family structures to for resident/property owners to track water usage.

Table 5-1 lists specific monitoring and reporting methods for each shortage stage that can be used to measure the effectiveness of reducing the shortage gap. As the stages progress into a greater percent supply reduction needed, the monitoring and reporting will increase in frequency, intensity, and resources.

Table 5-1: Monitoring and Reporting to Support Shortage Response Actions

Shortage Stage (% supply reduction)	Monitoring and Reporting Methods (How to measure effectiveness of reducing the shortage gap)
I	- Water-Use Monitoring Mechanisms
(Up to 10%)	- Prepare and review monthly water use reports
II	All Previous Monitoring and Reporting Methods AND:
(Up to 20%)	- Run and review monthly water use reports
III	All Previous Monitoring and Reporting Methods AND:
(Up to 30%)	- Run and review monthly water use reports
IV	All Previous Monitoring and Reporting Methods AND:
(Up to 40%)	- Run and review monthly water use reports
V	All Previous Monitoring and Reporting Methods AND:
(Up to 50%)	- Run and review monthly water use reports
VI	All Previous Monitoring and Reporting Methods
(Up 50% of More)	- Run and review monthly water use reports

Section 6: Enforcement

The District has the power and authority to implement and enforce its shortage response actions including mandatory water conservation measures within its boundaries per Resolution No. 09-04, which was adopted in March 2009.

Enforcement actions for violations of water conservation measures are summarized in Table 6-1. PWD customers are encouraged to report water conservation violations through use of the PWD hotline.

Table 6-1. Penalties for Customer Violations

Violation Level	Penalties or Charges
1 st Violation	The customer shall be notified in writing. The notice shall include a warning that further violations could result in stricter penalties.
2 nd Violation	A 2 nd violation is punishable by a fine of up to \$50.
3 rd Violation	A 3 rd violation is punishable by a fine of up to \$250.
4 th Violation	A 4 th violation is punishable by a fine of up to \$500.
5 th Violation	A 5 th violation may result in termination of service and a \$1,000 reconnection fee
Violation Assessment Period	Any violations occurring within twelve months of each other will be considered consecutive and result in escalating penalties. The period for assessing. consecutive penalties may be extended beyond 12 months by resolution of the Board.

In accordance with the PWD Water Waste policy, a receipt of notice regarding a claim of water waste or misuse, the Customer shall have five days to file a request for reconsideration with the General Manager, and fifteen days after the General Manager's decision to file a written appeal with the Board. A hearing on the appeal will be conducted in the next Board meeting following the appeal, with the Board's decision from the hearing designated as final and conclusive.

Section 7: Financial Consequences of Actions during Shortages

Water providers face significant financial challenges during droughts. During periods of reduced consumption, revenue from water sales decline while expenses remain relatively constant. A reduction in construction activities can also reduce water service connection fees collected. At the same time, as consumption decreases, some expenditures are expected to increase, including staff costs for community education, enforcement of ordinances, monitoring and evaluation of water use, and drought planning. Operations and maintenance costs may also increase because of the need to identify and quickly repair all water losses.

PWD recognizes the financial impacts of reduced customer deliveries and connections during droughts. The following sections describe potential revenue reductions, expense increases, mitigation actions and the cost of compliance with reducing residential water use during drought.

7.1.1 Revenue Impacts of Reduced Sales and Increased Costs

Currently, about 55 percent of PWD'S O&M costs are covered by fixed revenues. As a result, water conservation efforts can significantly impact revenues and the ability to cover fixed, non-variable costs.

Reductions in potable water use could result in an operating shortfall for the Potable Water Enterprise. While operating expenses are reduced with lower sales, fixed costs cannot be fully recovered when there are significant reductions in sales, thereby resulting in a net operating loss. PWD has planned for this shortfall by creating a reserve fund.

In the case of future water use reductions resulting from the implementation of the PWD WSCP, PWD would likely experience impacts to operating revenue and would draw as necessary and as possible from reserves. In addition, one of the objectives of the budget-based tiered rate structure implemented on January 1, 2020 is to improve revenue stability. Therefore, while revenue would inevitably fluctuate with water use reductions, PWD has established appropriate means to manage these impacts with use of drought surcharge, as indicated in the 2019 Financial Planning report. Future or continued reductions in consumption would ultimately cause a rate structure adjustment that would generate enough revenue to fund operations without drawing from reserves. Table 7-1 presents an amended summary of findings from the 2019 Financial Planning Report with respect to revenue impacts from demand reduction, based on data from 2020.

Table 7-1. Revenue Impacts of Reduced Water Demand

Demand Reduction	Annual Revenue Reduction (\$ million)	State Water Purchase Offset (\$ million)	Ancillary Costs (\$ million) ¹	Net Cost of Compliance (\$ million) ⁴
10%	-\$0.71	+\$0.38	\$0.23	-\$0.10
20%	-\$1.42	+\$0.76	\$0.25	-\$0.41
30%	-\$2.14	+\$1.13	\$0.28	-\$0.73
40%	-\$2.85	+\$1.51	\$0.27	-\$1.07
50%	- \$3.56	+\$1.88	\$0.26	-\$1.42

^{1.} Estimated as a percent of Operations and Maintenance expenses to reflect increased costs for expanded public outreach campaigns, increased meter reading, operational and administrative support during each drought stage to implement demand reduction actions.

7.1.2 Mitigation Actions to Address Revenue Reductions

A reduction in water revenue could be mitigated by use of the established reserve fund, deferral, or avoidance of capital fund expenditures, use of less costly water supplies (if possible), and implementation of drought surcharge rates. This would meet short-term cash flow needs, although it should only be considered on a short-term basis.

A summary of measures to overcome revenue and expenditure impacts is provided in Table 7-2.

Table 7-2. Measures to Overcome Revenue Impacts During Shortage

Measure	Summary of Effects
Use of Reserve Funds	Use of reserves may provide short-term rate stabilization but would require delays in capital expenditures and rebuilding of reserves after the water shortage.
Re-evaluate Capital Expenditure Plans	Delay major construction projects for facilities as well as upgrades and replacements.
Shift Water Sources to Less Costly Supplies if Possible	Reduce costs associated with purchase, treatment, and distribution of water.
Drought Surcharge Rates	Increase revenue.

Drought surcharges are recommended based on the Board Resolution No 09-04 and are summarized in the table below.

^{2.} Calculated sum of annual revenue reduction plus reduced imported water purchased plus ancillary costs.

Table 7-3. Proposed Drought Surcharges

Drought Mandate	CY	2020	CY	2021	CY	2022	CY	2023	CY	2024
20% Surcharge	\$	0.35	\$	0.38	\$	0.40	\$	0.42	\$	0.45
30% Surcharge	\$	0.54	\$	0.58	\$	0.61	\$	0.65	\$	0.69
40% Surcharge	\$	0.79	\$	0.84	\$	0.89	\$	0.94	\$	1.00

Source: PWD Financial Planning, Revenue Requirements, Cost of Service, and Rate Setting Analysis, 2019

7.1.3 Financial Consequences of Limiting Excessive Water Use

Per the California Water Code Section 365 et al., retail water suppliers are required to prohibit or discourage excessive water use. Reporting this is not a required part of the UWMP; however, Water Code Section 10632(a)(8)(C) requires the financial consequences of these actions be reported as part of the UWMP.

Water Code Section 367 states that there are three types of drought emergencies:

- Declared statewide drought emergency
- When a supplier implements its mandatory reductions per their WSCP
- A declared local drought emergency

Water Code Section 366 states that a retail water supplier must prohibit excessive use through one of two strategies:

- Rate structure. Specifically, a rate structure that includes block tiers, water budgets, or rate surcharges over and above base rates for excessive water use by a residential water customer.
- An excessive water use ordinance, Specifically an ordinance that includes a procedure
 to identify and address excessive water use by metered single-family residential
 customers and customers in multiunit housing complexes in which each unit is
 individually metered or submetered and may include a process to issue written warnings
 to a customer and perform a site audit of customer water usage prior to deeming the
 customer in violation.

PWD already has in place budget-based rates that discourage excessive water use. Should a drought emergency occur, PWD would already have the necessary processes in place to discourage excessive use. As discouraging excessive use is already a part of PWD's normal operations, the financial consequences of prohibiting excessive use would be minimal.

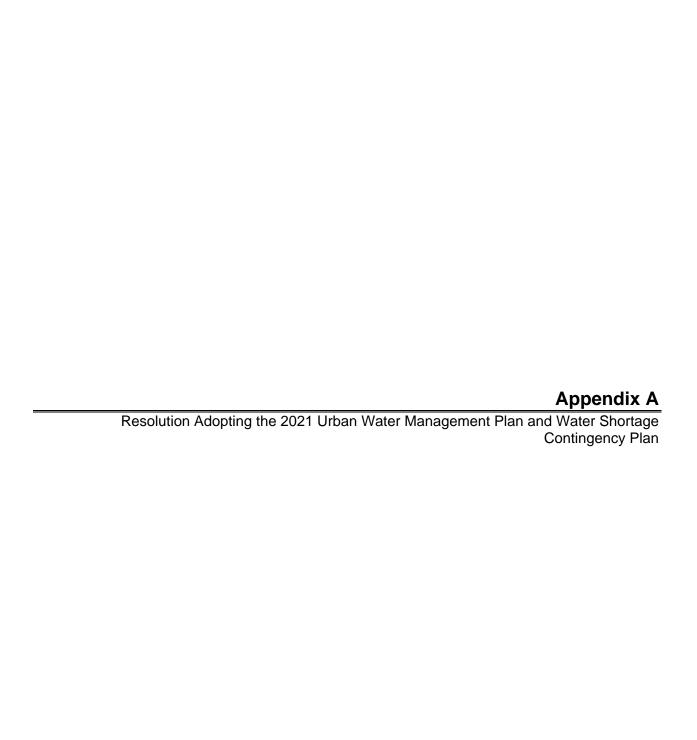
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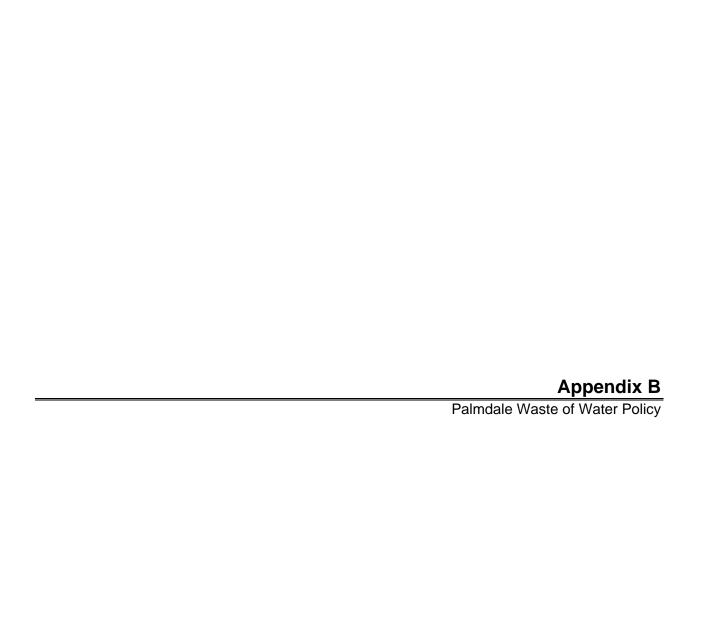
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APPENDIX O

WASTE OF WATER POLICY

Palmdale Water District is engaged in the production, transmission, storage and distribution of water to its Customers in accordance with California law.

California law prohibits the waste or unreasonable use of water and requires that the District take all appropriate actions to prevent such waste and unreasonable use of this finite resource.

Water waste includes but is not limited to:

- Application of potable water to outdoor landscapes in a manner that causes runoff.
- Failure to repair water leaks or to adjust sprinkler overspray in a timely manner.
- Hosing of hardscape surfaces, except where health and safety needs dictate.
- The use of potable water in a fountain or other decorative water feature, except where the water is part of a recirculating system.
- Irrigation with potable water of ornamental turf on public street medians.
- Watering of outdoor landscapes within 48 hours of measurable rainfall.
- Car washing and outside cleaning activities except when performed with buckets and automatic hose shutoff devices.
- The serving of drinking water other than upon request in eating or drinking establishments.
- Failure of operators of hotels and motels to provide guests with the option of choosing not to have towels and linens laundered daily. (The hotel or motel shall prominently display notice of this option in each guestroom.)
- Inefficient use of water for construction purposes.
- Irrigation with potable water outside of newly constructed homes and buildings not delivered by drip or microspray is prohibited.

Categories of Water Waste:

The District recognizes that water waste can vary significantly in severity and for this reason will classify and deal with three levels of water waste.

Level 1 Water Waste:

This is the least severe category of water waste which includes any violation of the Water Waste Policy and any other form of water waste that leads to minor but avoidable water loss. Examples of this would be overspray from improperly adjusted sprinklers or small leaks leading to wetting of the sidewalk.

Penalties for Level 1 Water Waste:

Penalties for Level 1 waste violation will be an initial warning. Failure to repair the violation will result in a \$50 fine. An additional new \$50 fine will be assessed if the follow up inspection shows that the violation is unrepaired. Follow up inspection will occur no more frequently than once every 14 days. If a Level 1 water waste violation continues unrepaired for greater than 60 days, then the District may elevate the penalties to Level 2 fines as described below.

Level 2 Water Waste:

This category includes any form of water waste where water is visibly and measurably flowing off the property. Examples of this would be a sheared off sprinkler or an irrigation system that is stuck on. Follow up inspection will occur no more frequently than once every 7 days.

Penalties for Level 2 Water Waste:

The penalties will mirror the penalties found in the Water Shortage Contingency Plan. These penalties are currently as follows:

1st Notice of Violation- The customer shall be notified in writing. The notice shall include a

warning that further violations could result in stricter penalties.

2nd Notice of Violation- is punishable by a fine of up to \$50.

3rd Notice of Violation- is punishable by a fine of up to \$250.

4th Notice of Violation- is punishable by a fine of up to \$500.

5th Notice of Violation- may result in termination of service.

Level 3 Water Waste:

This category includes any form of water waste where water leaving the property appears uncontrollable or poses a threat to public safety. Examples of this would be a broken water line flowing unrestrained off the property or water leaving the property causing a public safety threat due to icing or flooding.

Penalties for Level 3 Water Waste:

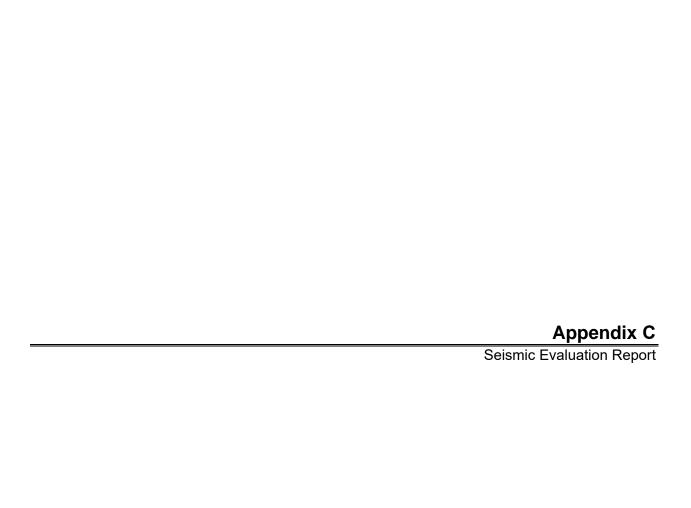
Level 3 water waste will result in the shutdown of service until the repair has been successfully accomplished. Repeat incidences of severe water waste will mirror the penalties found in the Water Shortage Contingency Plan.

District Process:

- 1. Upon notification or observation of waste or misuse of water, the District shall:
 - (a) Make a photographic record of such activity;
 - (b) Provide notice to the Customer in writing or by means of a door tag; and
 - (c) Log the warning on the Customer's service record.
- 2. In the event of a recurring violation, the District shall:
 - (a) Assess the appropriate fine upon the Customer for each notification of violation occurring after the warning has been given;
 - (b) Give notice to the Customer in writing that if such waste or misuse continues, the Customer may be subject to increased penalties up to and including disconnection of service.
- 3. Upon determination that a violation is still unresolved and a final notice needs to be issued, the District shall:
 - (a) Give written notice to the Customer that disconnection of the service will occur within five (5) working days of the date of the notice;
 - (b) Disconnect the Customer's service after the appropriate time has been allotted; and
 - (c) Charge the Customer a disconnection charge for waste or misuse of water as set forth in Appendix D and a turn-on fee as set forth in Appendix D if service is later restored. Service will be restored only when the Customer has provided evidence satisfactory to the District that waste and unreasonable use of water will no longer occur.

The District recognizes that there may be mitigating or intervening circumstances that bear upon a Customer's apparent misuse of water. Upon receipt of any notice regarding purported misuse or waste of water, the Customer shall have five (5) working days within which to file a written request for reconsideration with the General Manager. If the Customer is not satisfied with the General Manager's decision, the Customer shall have fifteen (15) days after the General Manager's decision within which to file a written appeal with the Board. The Board shall conduct a hearing on the appeal at the next Board meeting immediately following the appeal. The Board's decision following such hearing shall be final and conclusive.

ADOPTED BY THE BOARD OF DIRECTORS OF PALMDALE WATER DISTRICT AT A REGULAR MEETING HELD OCTOBER 11, 2017





3200 El Camino Real, 200 Irvine, CA 92602 949-261-1577

Seismic Risk Evaluation and Mitigation Report

14 May 2021

Prepared for

Palmdale Water District

2029 East Avenue Q Palmdale, CA 93550

KJ Project No. 2044225*00

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Section 1: Draft Seismic Risk Analysis

1.1 Overview

The Act requires urban water suppliers to evaluate potential seismic risk to the facilities in their system and produce a mitigation plan. This section describes the review of the of the existing documentation and preliminary evaluation seismic risk the Palmdale Water District's (PWD) existing facilities. This section also provides recommendations for mitigation of the existing risks. Current structural design practice is to design structures for ground motion with a 2.5% probability of exceedance in any 50-year period. This design earthquake is highly dependent on conditions at any given location. Earthquake magnitude is an estimate of the total energy released by a given earthquake and cannot be directly translated into the design earthquake used for structural design. However, The U.S Geological Survey estimates that there is a 99% chance that California will experience a 6.7 magnitude earthquake within 30 years. The Current design earthquake has a lower probability of occurring than an earthquake of similar magnitude to the 1994 Northridge Earthquake, 6.7.

The facilities review as part of this assessment include approximately 29 well sites, 14 booster pump station, and 19 steel water storage tanks, one underground concrete water storage tank, Lake Palmdale, and Little Rock Reservoir. The facilities described in this report were constructed between 1965 and the present day. There are significant gaps in the construction documentation of many of these facilities. Final seismic risk mitigation planning will require site visits by a Structural or Civil Engineer experienced in design of water treatment facilities to evaluate the existing conditions. Where possible an initial determination of the seismic loads at the facilities has been determined in accordance with the 2010 Edition Minimum Design Loads Associate for Buildings and Other Structures (ASCE 7-10) using the web-based Hazard Maps by the Applied Technology Council (ATC). The 2010 edition was used in this stage because ASCE 7-16 as referenced in the current California Building Code (CBC) requires site specific geotechnical investigations for most conditions and structures. When implementing the final mitigation recommendations, a geotechnical investigation will be required for most of the Palmdale Water District's facilities.

1.2 Water Storage Tank Evaluation Summary

The seismic evaluation of SCV Water was conducted by applying the seismic design provision of the 2011 edition of Welded Carbon Steel Tanks for Water Storage by the American Water Works Association (AWWA D100-11). SCV Water currently operates over 90 steel water storage tanks. For our analysis we were provided the diameter, height to the overflow and maximum capacity of the storage tank. Using this information, ASCE 7-10 seismic parameters, and the seismic provision of AWWA D100-11, we determined the seismic loads, sloshing wave height, and anchorage requirements of SCV Water's storage tanks. Final design of welded and bolted steel water storage tanks is typically conducted by specialty contractors and submitted during construction. The construction drawings rarely indicate the final plate thicknesses,

location and size of columns, size and location of anchors or other significant aspects of design beyond size and design criteria. Further field investigations will be required quantify further risk.

Storage tanks build prior to 1984 are unlikely to be compliant with current building standards are unlikely to have been designed for lateral loads due to seismic events. Storage tanks built between 1984 and 2011 were probably designed with seismic loads however they may not be designed to withstand seismic loads determined in accordance with the current building code. Those storage tanks designed after 2011 are likely designed to meet current building code requirements.

Table 1: Tank Design Use Group

AW	/WA D100-11 D	Design Use Group and Seismic Importance Factor
Use	*Importance	
Group	Factor, l _e	Description
I	1	Tanks that provide service to facilities deemed essential for post-earthquake recovery and essential to the life, health, and safety of the public, including post-earthquake recovery
II	1.25	Tanks that provide service to facilities that are deemed important to the welfare of the public.
III	1.5	All Other

^{*}Importance factor is used to amplify loads from earthquakes.

16 of the existing storage tanks require anchorage to the foundations. Neither the PWD standard tank details nor construction documents indicate that these tanks are anchored. The remaining storage tanks will experience uplift due to seismic loads but do not require anchors at the foundation. The sloshing wave height and required freeboard varies between nine and 16 feet in height. In most cases this exceeds the existing freeboard which is typically three feet from the maximum operating height to the roof structure. Record drawings of the underground concrete storage tank were not available for review however, the tank was designed and build in 1994 and built in accordance with ACI 350, Code Requirements for Reinforced Concrete Structures. Investigations should be conducted to determine what the existing conditions of the structure are and determine if any deficiencies may exist.

 Table 2: Anchorage and Freeboard Requirements.

										AW	'WA D100-11 W	elded Carbon Steel	anks Chapter 13 S	Seismic Design ^{1,2}				
		1		Tank Det	ails			Table 28	13.2.1	Table 24	Eqn 13-36		Eqn 13-52	Table 29		Eqn 13-57		
Tank Site	Address	Date Built	Dia	Size	Top of Knuckle	Overflow Height	Freeboard Assumed to be 3 feet unless drawings indicate otherwise	Ri 3 if anchored 2.5 if unanchored	Seismic Use Group	I _E , assume that all tanks are Seismic Use Group III	Overturning Ratio, J	Anchor Requirements	Sloshing Wave Height (d), ft	Minimum Required Freeboard (D), ft	Actual Freeboard (Roof Height- Overflow)	Allowable Lateral Load, V _{allow} (kip)	Total Lateral Seismic Load, Vt (Kip)	Sliding Check
3 MG Tank Site	850 East Avenue S	1960	124	3,000,000	Unknown	34	3	2.5	iii	1.5	2.54	Provide Anchors	16.65	16.65	3	12851	7225.517287	ОК
5 MG Tank	2404 Old Nadeau Road		160	5,000,000	Unknown	20	3	2.5	iii	1.5	0.57	Tank Is Stable	10.08	10.08	3	12338	3533.246096	ОК
6MG	641 East Ave S	1999	206	6,000,000	Unknown	24	3	2.5	iii	1.5	0.64	Tank Is Stable	9.58	9.58	3	24349	6291.49113	ОК
25th Street	26496 Cemetery Road	1976	106	2,000,000	Unknown	30	3	2.5	iii	1.5	2.23	Provide Anchors	15.53	15.53	3	8304	4860.105574	ОК
25111311661	20490 Cemetery Road	1967	154	4,000,000	Unknown	30	3	2.5	iii	1.5	1.51	Uplift but Stable	14.15	14.15	3	17380	7130.096891	ОК
		1988	130	3,000,000	Unknown	30	3	2.5	iii	1.5	1.77	Provide Anchors	14.95	14.95	3	12488	5845.275811	ОК
45th Street	36510 45th St East	1990	150	4,000,000	Unknown	32	3	2.5	iii	1.5	1.74	Provide Anchors	14.33	14.33	3	17687	7540.066766	ОК
		1990	150	4,000,000	Unknown	32	3	2.5	iii	1.5	1.74	Provide Anchors	14.33	14.33	3	17687	7540.066766	ОК
47th Street	35645 47th St East	1967	106	2,000,000	Unknown	30	3	2.5	iii	1.5	2.24	Provide Anchors	15.64	15.64	3	8301	4879.725022	ОК
47111311661	33043 47 th 3t East	1990	132	3,000,000	Unknown	30	3	2.5	iii	1.5	1.87	Provide Anchors	16.32	16.32	3	12801	6303.069693	ОК
50th Street	5001 East Ave. T-8	2007	150	4,000,000	Unknown	30	3	2.5	iii	1.5	1.55	Provide Anchors	14.22	14.22	3	16514	6902.168294	ОК
John Street	Jool Last Ave, 1-6	2007	150	4,000,000	Unknown		3	2.5	iii	1.5	1.55	Provide Anchors	14.22	14.22	3	16514	6902.168294	ОК
Ana Verde	36800 Tovey Avenue	1963	40	300,000	Unknown	32	3	2.5	iii	1.5	5.44	Provide Anchors	9.95	9.95	3	1363	1351.046084	ОК
El Camino Lower	36809 El Camino Dr.	1988	106	2,000,000	Unknown	32	3	2.5	iii	1.5	2.42	Provide Anchors	15.24	15.24	3	8916	5163.807319	ОК
El Camino U.G ⁴	36336 El Camino Road	1994	104	1,500,000	Unknown	26												
El Camino Upper	33030 Ridge Route Rd	1963	40	300,000	Unknown	32	3	2.5	iii	1.5	5.00	Provide Anchors	7.22	7.22	3	1371	1262.693411	ОК
Walt Dahlitz	115 East Avenue S	1993	104	1,500,000	Unknown	31	3	2.5	iii	1.5	1.80	Provide Anchors	9.80	9.80	3	8455	3868.50122	ОК
Well 14	36401 20th ST East		27	100,000	Unknown	22	3	2.5	iii	1.5	4.80	Provide Anchors	6.24	6.24	3	435	399.685968	ОК
Well 18 and 19	4640 Barrel Springs Road	1963	22	41,000	Unknown	30	3	2.5	iii	1.5	11.47	Provide Anchors	8.06	8.06	3	387	488.3004155	Needs Anchors
Well 5	1036 Barrel Spring Road	1963	30	1,463,945	Unknown	22	3	2.5	iii	1.5	5.05	Provide Anchors	9.29	9.29	3	526	561.5710227	Needs Anchors

^{1.} Design spectral response acceleration parameters, S_{D1} and S_{DS}, have been determined using the Applied Technology Council's (ATC) web-based hazard maps in accordance with the American Society of Civil Engineers Standard 7, Minimum Design Loads for Buildings and Other Structures (ASCE 7-10)

^{2.} The Design spectrum for impulsive components, Sai and the Design Spectrum for convective components, Sac have been determined in accordance with Chapter 13 of the AWWA D100-11, Welded Carbon Steel Tanks for Water Storage. These parameters are expressed as a percentage of the acceleration due to gravity, g.

^{3.} Minimum required freeboard is equal to the sloshing wave height for Use Group III and may be reduced for Use Group I and II

^{4.} AWWA D100 calculations do not apply to the El Camino Underground tank. Construction drawings are not available to perform an analysis currently.

To determine if the storage tank walls and roof systems are adequate to resist potential seismic loads, field visits will be required to determine the existing plate thicknesses and structural sections used in construction. Further analysis will then be performed determine the capacity of the storage tank structural system. For those storage tanks that required anchors, greater freeboard, or do not have the structural capacity to meet demand we recommend reducing the operating capacity and overflow height to reduce the seismic demands on the structures. Water storage tanks designed in accordance with AWWA D100 and D103 can be classified in one of three seismic use groups as described in Table 1. The initial analysis has been conducted assuming all of the storage tanks are in Use Group III, essential for post-earthquake recovery and essential to the life, health, and safety of the public, including post-earthquake fire suppression. For those facilities that are not required for post-earthquake recovery, the use group may be designated as Use Group II, tanks that provide direct service to facilities that are teemed important to the welfare of the public. In rare cases they may be assigned to Use Group I, those that are not essential to the health and safety of the public. This will reduce the design seismic load by twenty-five percent and fifty percent.

Field investigation are necessary to determine the structural capacity of the existing storage tanks. Thickness of the tank shells and roofs will be determined using an ultrasonic thickness gauge, the size number and location of columns will be determined. In our experience the most common mode of failure for steel storage tanks is buckling of the lowest shell plate. Due do relatively significant consequences in the event of failure, we recommend that the steel tanks be given high priority for further investigation and mitigation efforts.

1.3 Source Water Supply

The District's source water consists of the Palmdale Lake, Little Rock Reservoir and more than 20 well sites. The Little Rock Lake Reservoir under the jurisdiction of the California Division of Safety of Dams. The Division of Safety of Dams inspects the Little Rock Reservoir Dam on an annual basis and periodically reviews the stability of dams considering improved design approaches. The Little Rock Dam represents minimal risk to the District due to the inspection and review by the Division of Damn Safety. The Little Rock Dam Recreation Areas include several small buildings and structures. These structures pose negligible risk to the public in the event of an earthquake. The facilities at the Little Rock Reservoir and Palmdale Lake are summarized in Table 3 below.

There are several facilities at Palmdale lake including a concrete box culvert, concrete spillway, and drainage channel. These structures consist of relatively minor reinforced concrete at or below grade. The primary risk to these structures is the potential for liquefiable soils in the area. In the event of failure, they pose a relatively minor risk to the public, however geotechnical investigations should eventually be conducted to determine susceptibility to earthquake damage.

The typical well site consists of vertical turbine pumps embedded directly into the soil and represent minimal risk of failure during or after an earthquake. Many of the well sites are colocated with booster pumpstations and tank sites. Site visits by a qualified civil or structural engineer should be conducted to verify the existing conditions at each site. Above ground piping is generally rigid and represents minimal risk of failure during an earthquake. It is typical for the piping systems at older well sites to lack support for lateral loads due to earthquakes. The inspections should take note of any pipe supports that are not anchored into concrete foundation. Where available, record drawings typically indicate that chemical storage tanks. generators and other equipment is anchored to foundations. The current building code requires anchors for steel storage tanks for liquids to fail in a ductile manner. It is unlikely that the anchorage for the existing facilities meet this requirement. The installations of older facilities are unlikely to follow current standard practices. The well sites are summarized in Table 4. Below. Facilities have been assigned a relative risk between one and 10. This assessment is subjective and intended to assist the district in prioritizing further investigation and mitigation. The factors increasing relative risk include the age of structures, lack of necessary record drawings, noted deficiencies.

Table 3: **Miscellaneous Facilities**

		Facilit	ies			
Site	Address	Date Built	Generator	Structural Record Drawings	Structures	Noted Risk/Deficiences
Little Rock Canal	Mulitple	1995	No	1995	Cast-in-Place Concrete Canal	None Noted, subgrade reinforced concrete walls designed and built in 1995.
Little Rock Dam and Reservoir	33883 Cheseboro Road	1992	No	1992	Concrete buttressed earthwork Dam Reinforced Concrete Vault	Under the jurisdiction of the Bureau of Dam Safety, yearly inspection, and periodic review for structural soundness.
Little Rock Dam Recreation Area 1	Adjacent to Little Rock Reservoir	1997	No	1997	Walk-in campsite toilets, wood framed roof over CMU and Gazebo	None Noted.
Little Rock Dam Recreation Area 2	Adjacent to Little Rock Reservoir	1996	No	1996	N/A	None Noted
Little Rock Dam Recreation Area 3	Adjacent to Little Rock Reservoir	1994	No	1994	Cantilever column shelter structures	None noted
Little Rock Dam Recreation Area 4	Adjacent to Little Rock Reservoir	1994	No	1994	None	None Noted
Little Rock Dam Recreation Area 5	Adjacent to Little Rock Reservoir	1994	No	1994	Walk-in campsite toilets, wood framed roof over CMU	None Noted
Little Rock Dam Recreation Area 6	Adjacent to Little Rock Reservoir	1994	No	1994		None Noted
Little Rock Sluice Gate and Siphon	Adjacent to Little Rock Reservoir	Modifications 1998	No	1998	Cast-in-place concrete siphon structure	None Noted
Palmdale Lake Box Culvert	South East of Palmdale Lake	1992	No	1992	Cast-in-place box culvert	None Noted
Palmdale Lake Spillway	North shore of Palmdale Lake	1988	No	1988	Cast-in-place Concrete spillway	Subgrade should be investigated by a Geotechnical Engineer for potential erosion or liquefiable soils.
Palmdale Lake Drainage Channel	Adjacent to Palmdale Lake	1992	No	1992	Concrete lined channel	None noted

Table 4: Well Site Summary

				Fa	cilities							
Well Site	Address	Date Built	Building	Fuel Storage	Chemical Storage	Pump HP	Capacity (GPM)	Structural Record Drawings	Roof Type	Lateral System	Noted Risk/Deficiences	Relative Risk ¹
2A	39400 20th St East	1968	Yes		NaOCl	125	265	1968	Steel deck over steel and wood framing	Solid grouted CMU and wood studs	Potential irregularity due to the mixed resisting System	4
3A	2163 East Ave P-8	1960	Yes	Propane	Salt	500	1,551	1992		Solid Grouted CMU with wood studs	Potential irregularity due to the mixed resisting System	3
4A	2475 East Ave P-8	1970	Yes		Salt/ NaOCI	200	778	Not Available				3
5	1036 Barrel Springs Rd	1965	yes			5	99	Not Available	Steel Deck over steel framing	Steel Braced Frame Steel Moment Frame	Rod Bracing is prone to buckling. Columns are pinned with (2) at shallow embedment	8
6A	39455 10th St East	1983	Yes		NaOCI	125	265	Not Available		Steel moment Frame	Drawings were inadequate to determine specific risks	8
7A	39395 25th St East	1985	Yes		Salt/ NaOCI	500	1,589	Not Available	Steel Deck over steel framing	Pre- engineered metal building	Inspection is required to determine specific vulnerabilities.	8
8A	2200 East Ave P	1987	Yes		NaOCl	600	2,024	Not Available			Drawings were inadequate to determine specific risks	8
10	3701 East Ave P-8	1956	Yes		NaOCI	100	254	1956	Steel Frame	Steel Framed	Drawings were inadequate to determine specific risks. The building is 65 years	8
11A	39501 15th St East	1963	Yes				1,161	1999	Wood deck over 2x wood framing	Wood stud shear wall	None	3
14 ²	39401 20th St East	1965	Yes		Salt	250	1,188				None Noted	3
15	1003 East Ave P	1960	Yes		Salt/ NaOCI	590	998	1999	Wood deck over wood framing	Wood stud shear walls	None Noted	1
16	4125 East Ave S-4	1960	Yes		NaOCl	40	150	Not Available			Drawings were inadequate to determine specific risks	7
17	718 Denise Ave	1966	Yes			20	110	1996	Wood deck over wood framing	Wood stud shear walls	Thin floor slab may provide inadequate anchorage	3
18 and 19 ²	4640 Barrel Springs Rd	1954 1961	Yes		NaOCl	5	96 127					4
20	5680 Pearl Blossom Hwy	1973			NaOCl	60	227	2001	Wood deck over wood framing	Wood stud shear walls	Thin floor slab may provide inadequate anchorage	3
21	36525 52 St East	1973			NaOCI	30	227	1999	Wood deck over wood framing	Wood stud shear walls	Thin floor slab may provide inadequate anchorage	1
22	5401 East Ave S	1974			None	75	347	1999	Wood deck over wood framing	Wood stud shear walls	Thin floor slab may provide inadequate anchorage	1
23A	2202 East Ave P-3	1977	Yes		NaOCI	250	743	1999	Wood deck over wood framing	Wood stud shear walls	Thin floor slab may provide inadequate anchorage	1
25	3750 70th St East	1989	Yes		Salt/ NaOCI	125	514	1992	Wood deck over wood framing Wood deck	Solid CMU	Thin floor slab may provide inadequate anchorage Thin floor slab may	2
26	4701 Katrina Place	1989	Yes			50	304	1992	over wood framing	Wood stud shear walls	provide inadequate anchorage Drawings were	2
29	37700 67th st East	1989	Yes		NaOCl	40	250	1989	Wood deck		inadequate to determine specific risks Thin floor slab may	
30	7392 East Ave R	1989	Yes		Salt/NaOCI	150	498	1990	over wood framing Wood deck	Solid CMU	provide inadequate anchorage Thin floor slab may	3
32	37301 35th St East	1989	Yes		NaOCI	60	293	1992	over wood framing Wood deck	Wood stud shear walls	provide inadequate anchorage Thin floor slab may	2
33	7160 East Ave R	1991	Yes		Salt/ NaOCI	75	418		over wood framing Wood deck	Solid CMU	provide inadequate anchorage Thin floor slab may	2
35	36549 60th St East	1991	Yes		Salt/ NaOCI	75	444		over wood framing	Solid CMU	provide inadequate anchorage	2

^{1.} Relative risk is a subjective measure based on risk to life and post-earthquake operation intended to assist in the District to prioritize further investigation

^{2.} See Table 5 for building structures.

1.4 Booster Pump Stations

Pump stations consist of above grade or below grade structures with multiple pumps wet wells, and additional equipment. Like steel water storage tanks older facilities are less likely to be designed for lateral loads equivalent to modern building standards. Those designed and built later than 2000 are unlikely to pose a substantial risk in the event of an earthquake. Site visits should verify that the existing equipment is anchored to the foundations and walls, and that there is an adequate load path to transfer lateral loads from the roof and walls to the foundations. The booster pump station facilities are summarized in Table 4 below.

1.5 Well and Booster Pump Buildings

Where record drawings are available, they indicate that most of the buildings are relatively small one-story structures. The structural systems include reinforced concrete masonry unit shear walls, wood stud shear walls, and steel framed walls. The roof structures are wood or metal diaphragms over steel or wood framing. The 3 MG Tanks and 5 MG Tank pump stations includes two buildings with a mixed structural system. This may introduce irregularities in performance due lateral earthquake loads. Many buildings have relatively thin slabs. While this is common in earlier designs, the current building code typically requires greater depth of embedment for equipment anchors. The building structure at Well Site 10 appears to be a steel tube framed structure of a type that would no longer be permitted by the building code. The available documentation was not sufficient to fully analyze the system.

1.6 Mitigation Planning

The District should identify which facilities are required to operate immediately following an earthquake, are required for the health and safety of the public, and those that are not either. The highest priority should be given to those facilities that supply fire suppression systems, including water storage tanks and transmission system. The first step in mitigating the risks identified in this report will be to arrange for a civil or structural engineer experienced in design of water treatment and distribution systems to inspect the Districts facilities. Once the District and Kennedy Jenks has identified the most critical and at-risk facilities, the District should consult with a geotechnical engineering firm to perform site investigations of the most crucial facilities to allow a qualified engineer to perform a more accurate and detailed analysis and provide the most appropriate mitigation efforts.

For those storage tanks that require anchorage and or have insufficient freeboard height to accommodate wave action the district may take immediate action to reduce the risk. As shown in Table 2, the District may choose to reduce the operational capacity to prevent instability, increase freeboard, and reduce the sloshing wave height. The District may determine that some of the storage tanks are not required for immediate post-earthquake recovery and do not pose a substantial risk to human life. In those cases, the Seismic Use Group will be reduced to reduce the required freeboard and demands due to seismic loads. This may result in no further

action being required.	Kennedy Jenks re	ecommends providi	ng anchors for all ste	eel water
storage tanks.				

 Table 5:
 Booster Pump Station Summary

					Facilities								
Booster Pump Station Site	Address	Date Built	Building	Fuel Storage	Chemical Storage	Pump HP	Capacity (GPM)	Generator	Structural Record Drawings	Roof Type	Lateral System	Noted Risk/Deficiences	Relative Risk ¹
3 MG Tanks	850 East Ave	1965	(2) CMU (1) Wood Framed		NaOCI	(6) 50 (1) 150	(7) 3500	Yes	1965	(2) Steel deck over steel and wood framing (1) Alumin Sheet over Wood	(2) Partially Grouted CMU (1) Aluminun and Wood Shear Wall	The building is lightly reinforced and partially grouted, it may not be up to current building standards The building slab is 4", equipment is unlikely to have adequate anchorage	4
5 MG Tank	2404 Old Nadeua RD	1960	Yes	Propane	NaOCl	40	_	No	1992		Solid Grouted CMU with wood studs	Potential irregularity do the the mixed resisting System	4
6 MG Tank	700 East Avenue S	1999	Yes		Salt/ NaOCI	(1) 100 (1) 150 (2) 200 (2) 250 (2) 250	(1) 2000 (1) 2800 (2) 7000 (3) 3500	No	1999	(1) Open web steel joists (1) Steel deck over steel framing (1) Subgrade concrete structure for the hydropnuematic tank	Solid Grouted CMU	Relatively Thin Slab may result in inadequate anchorage for some equipment. Single story solid grouted CMU structures are very resistant to earthquake damage.	3
25th Street	26946 Cemetary Rd	1987/ 1996/ 2001	yes		Salt/ NaOCI	50 100	99	315 Kw	Not Available	Wood deck over 2x wood framing	Wood stud shearwall	Wood Stud buildings tend to be resiliant to earthquakes provided adeqate attachments are present. The 3 1/2" may result in inadequate anchorage for equipment. Structural drawings from the orignal construction are not availabe for review.	3
45th Street	36510 45th St E		Yes		NaOCI	(3) 150 (3) 125	(3) 3500 (3) 3500	NO	1998 2004 2001	(1) Wood Deck over Wood Framing (2) Steel deck over steel framing	(1) Wood stud shear wall (2) Solid grouted CMU	Both wood stud and Solid Grouted CMU shear wall structures are resistent to earthquake loads. All three buildings appear to have complete load paths. The generator building floor slab is only 4" thick and may not provide adequate anchorage to any floor mounted equipment.	8
Avenue T-8	4250 E. Ave. T-8	1995	Yes		Salt/NaOCI	(2) 15 (1) 50	(3) 3250	No	Addition 1998	Wood deck over 2x wood framing	Wood stud shearwall	Construction drawings for the original building are not available for review, wood framed structures are generally resistent to earthquake.	8
El Camino Lower El Camino Under Ground	36336 El Camino Dr	2000	Yes		NaOCI NaOCI	(1) 40 (1) 75	Not recorded on Drawings	No	2000	Wood deck over wood framing	Solid grouted CMU	Wood diaphrams with solid grouted CMU wall are generally resistent to earthquakes loads.	8
Well 14	36401 20th St E	1997	Yes		Salt	250	1,188		1997	Wood deck over 2x wood framing	Solid grouted CMU and wood stud shear walls	Potential irregularity do the the mixed resisting System. Construction drawings from the original building were not avaible for review.	8
Well 5	39401 20th St East	1663	Yes		Salt	250	1,188		Not avaiable				3
Alta Valley Well 18 and 19	4640 Barrel Springs Road	1976 1997	Yes		NaOCI	5	96 127		1976 1997	Wood deck over wood framing	Wood stud shearwall	Relatively thin slab may result in inadequate anchorage for some equipment. Single story solid grouted CMU structures are very resistant to earthquake damage.	3
3600 ft boosters	601 Lakeview Dr	1966	Yes			20	110		Not availalable			Record drawings were not avaible for the existing building, field investigations are required.	1
3900	36200 El Camino Dr	1954	Yes		NaOCl	5	96						7
boosters		1961					127					Donald day, time and a time la beautiful and the state of the base	3
Hilltop	35609 Cheseboro Rd	Multiple	Yes		NaOCl	60	227		Not Available			Record drawings are not aviable, howerver the small size of the buiding represents minimal risk.	2



												Ĭ																AWWA	D100-11 Welded O	Carbon Steel Tan	s Chapter 13 Seism	nic Design															
		Coord	dinates				T:	ank Details						Table 28	13.2.1	Table 24 AT	1 Eqn 13	9 ^{1,2} Eqn 1	3-22 E	qn 13-12/13 ²			13	3-27 1	3-25/26 Eqn 13-	28/29 Estimat	ate Estima	ate Estimate	Eqn 13-16		Eqn 13-24/25	Eqn 13-3)		Eqn 13-26	Eqn 13-31	Eqn 13-23	Eqn 13-37	Eqn 13-41	Eqn 13-36		Eqn 13-53/54	Eqn 13-52	Table 29	Equ	qn 13-57	
Tank Site	Address	Latitude	Longitude Tar	ık Type Co	Piping Foot nnection	ing	Anchorage	Date Built	Dia	Size Botton Knu		Overflow e Height	Freeboard Assumed to be 3 feet unless drawings indicate otherwise	Ri 3 if anchored 5 if unanchored		, assume that all Sels anks are ismic Use Ma Group III	nic Based on S	ts from		Sac, g ed on Sd1 from ASCE 7-10	D/H 3.67	7*D/H Vol =	olume ft ² : π*(Dia^2)/4	Total Weight, Ibf W = V Vol*62.4pcf	Impulsive latera	Sloshing Roof (ht of the Weig (Wr), lbf Shell	ght of the Weight of t (Ws), lbf Floor (Wf),	Implusive he Design lbf Acceleration (Al)	Impulsive Lateral Force (VI), kip	Overturning Moment due to Impulsive Lateral 1 Force(Mi), ft- kip	Convective Weight (Wc), lbf mass (X ft	al Convective to Design we Acceleration	Convective Lateral Force (Vc), kip	Overturning Moment due to Convective Lateral Force(Mc), ft- kip	Design Latera Force at the top of the foundation (Vf), kip		Maximum Resting Weigh of the Tank Contents (wt.) Ibf/ft	Weight of the Tank Shell and Roof Resisting Overturning (wt), lbf/ft		Anchor equirements	Convective Design Accelaration, Af	Sloshing Wave Height (d), ft	Required F Freeboard (D), (I	ctual Ai reeboard Roof Height- Lo lverflow)	Allowable Late Lateral Seis Load, Valow Load	otal teral ismic Sliding id, Vt (ip)
3 MG Tank Site	850 East Avenue S		-118.11 W	elded				1960	124 3,	000,000	Unknov	m 34	3	2.5	ш	1.5 1.3	15 1.80		-	0.27	3.647 1.	.006	410594	25621040	8082906	13	92459	138480 924	159 0.774	4 650	82912	16424329	18 0.192	3150	57649	722	100984	2185 539	474	4 2.54 Provi	ide Anchors	0.27 0.29	1.27 16.65	16.65	3	12851 7225.	.51729 OK
5 MG Tank	2404 Old Nadeau Road	ad 34.53	-118.08						160 5,	000,000	Unknov	vn 20	3	2.5	III .	1.5 1.3	02 1.76	11.1	13	0.13	8.000 0.	459	402124	25092529	3621894	8	153938	104550 153	938 0.756	6 305	22875	19810034	10 0.090	1784	18144	353	29197	1676 409	36:	1 0.57 Tank	k Is Stable	0.18 0.13	10.08	10.08	3	12338 35?	13.2461 OK
6MG	641 East Ave S		-118.15					1999	206 6,	000,000		vn 24	3	2.5		1.5 1.3	16 1.80	13.0	03	0.09	8.583 0.	.428	799900	49913745	6714999	9	255176	160865 255	176 0.77	3 571	51395	39739497	12 0.066	2640	32159	629	60628	1836 632	441	6 0.64 Tank		0.15 0.09	1.09 9.58	9.58	3	24349 6291.	
25th Street	26496 Cemetary Road	d 34.55	-118.09					1976	106 2,	000,000	Unknow	vn 30	3	2.5		1.5 1.3	16 1.80	6.7	4	0.29	3.533 1.	.039	264742	16519902	5375203	11	67564	104870 67	564 0.77	3 434	48840	10436273	16 0.209	2185	35431	486		2052 407	410	6 2.23 Provi		0.29 0.35		3 15.53	3	8304 4860.	.10557 OK
25til Street	20490 Cellietal y Road			elded No	t Flexible Ring	wall with Sand Interio	or	1967	154 4,	000,000	Unknow	vn 30	3	2.5		1.5 1.2	78 1.77	9.1	.3	0.18	5.133 0.	715	558795	34868813	7841520	11	142609	151052 142	509 0.762	2 631	71001	25267634	16 0.131	3318	51781	713	87878	2052 591	461	0 1.51 Uplift	ift but Stable	0.21 0.18	14.15	5 14.15	3	17380 7130.	
		34.54	-118.05					1988	200 0	000,000	Unknow		3	2.5		1.5 1.2	14 1.72						398197	24847485	6614006	11	101623	127961 101	523 0.731	8 512	57696	17074207	16 0.164	2809	44414	584	72811	2052 499	431	8 1.77 Provi	ide Anchors	0.23 0.23	1.23 14.95	14.95	3	12488 5845.	
45th Street	36510 45th St East							1990		000,000		m 32	3	2.5	III	1.5 1.2	1.72		_				565487	35286369	8687384	12	135297	157017 135		8 673	80769	24894926	17 0.137	3398	56992	754	98852	2120 614	47	7 1.74 Provi	ide Anchors	0.21 0.19	1.19 14.33	3 14.33	3	17687 7540.	
								1990		000,000	Unknov		3	2.5	III	1.5 1.2			_				565487	35286369	8687384	12	135297	157017 135	297 0.731	8 673	80769	24894926	17 0.137	3398	56992	754	98852	2120 614	47	7 1.74 Provi	ide Anchors	0.21 0.19	1.19 14.33	3 14.33	3	17687 7540.	
47th Street	35645 47th St East	34.53	-118.05					1967		000,000	Unknov		3	2.5	III	1.5 1.3	1.0.			0.00			264742	16519902	5375203	11	67564	104870 679	564 0.776	6 435	49003	10436273	16 0.211	2200	35674	488	60613	2052 407	416	6 2.24 Provi	ide Anchors	0.30 0.35	1.30 15.64	15.64	3	8301 4879.	
	***************************************							1990		000,000		vn 30	3	2.5	III	1.5 1.3							410543	25617904	6716566		104774	129885 104		6 547	61576	17698347	16 0.177	3126	49427	630	78960	2052 506	441	0 1.87 Provi		0.25 0.25	1.25 16.32	2 16.32	3	12801 6303.	
50th Street	5001 East Ave. T-8	34.54	-118.04							000,000		vn 30	3	2.5	III	1.5 1.3			_				530144	33080971	7637298			147203 135		8 610			16 0.135		50405			2052 576	450	6 1.55 Provi		0.21 0.19		2 14.22	3	16514 6902.	
	,			elded?		crete Ring Wall	None Shown	2007	150 4,	seejeee	Unknov		3	2.5	III	1.5 1.3			_				530144	33080971	7637298	11	135297	147203 135	297 0.751	8 610	68664	23796213	16 0.135	3223	50405	690	85178	2052 576	450	6 1.55 Provi	ide Anchors	0.21 0.19	1.19 14.22	2 14.22	3	16514 6902.	
Ana Verde	36800 Tovey Aveneu			elded No	t Flexible Con	crete Rink wall	Not Shown	1963		00,000	Unknov		3	2.5	III	1.5 1.2							40212	2509253	1825481	12	9621	44129 9	521 0.70	2 132	16240	717357	22 0.355	255	5658	135	17197	2120 163	385	9 5.44 Provi	ide Anchors	0.50 1.09	1.50 9.95	9.95	3		.04608 OK
El Camino Lower	36809 El Camino Dr.	34.55	-118.13					1988		000,000		vn 32	3	2.5	III	1.5 1.3	7 1.71	6.6	i3	0.29	3.313 1.	.108	282391	17621228	6103267	12	67564	111862 67	564 0.73	5 466	55977	10784811	17 0.205	2215	38666	516	68033	2120 434	43	7 2.42 Provi	ide Anchors	0.29 0.35	1.29 15.24	15.24	3	8916 5163.	.80732 OK
El Camino U.G ⁴	36336 El Camino Road	d						1994	104 1,	500,000	Unknov	vn 26																																			
El Camino Upper	33030 Ridge Route Rd	d 34.54	-118.13 W	elded I	Flexible Ring	wall with Sand Inte	None Shown	1963	40 3	00,000	Unknow	m 32	3	2.5	Ш	1.5 0.8	81 1.54	3.6	i6	0.36	1.250 2.	.936	40212	2509253	1825481	12	9621	44129 9	521 0.66	1 124	15289	717357	22 0.258	185	4106	126		2120 163	385	9 5.00 Provi	ide Anchors	0.36 0.79	1.36 7.22	7.22	3	1371 1262.	.69341 OK
Walt Dahlitz	115 East Avenue S		W	elded I	Flexible Con-	rete Ringwall, oil s	None Shown	1993	104 1,	500,000	Unknow	vn 31	3	2.5	Ш	1.5 0.8	27 1.44	6.5	i8	0.19	3.355 1.	.094	263341	16432470	5622265	12	65039	106378 658	0.61	8 362	42091	10122208	17 0.135	1362	22997	386		2086 412	42	5 1.80 Provi	ide Anchors	0.19 0.23	1.19 9.80	9.80	3	8455 3868.	
Well 14	36401 20th ST East		W	leled? No	t Flexible Con	crete Ringwall, grav	3/4" 5' OC 8" embed		27 1	00,000	Unknow	m 22	3	2.5	Ш	1.5 0.9	27 1.51	3.0	11	0.46	1.227 2.	.990	12596	786004	575712	8	4384	21166 4	384 0.649	9 39	3325	220749	15 0.330	73	1119	40		1758 76	27	5 4.80 Provi	ide Anchors	0.46 1.23	1.46 6.24	6.24	3	435 399.6	85968 OK
Well 18 and 19	4640 Barrel Springs Roa	ad						1963	22	1,000	Unknow	vn 30	3	2.5	Ш	1.5 1.3	23 1.8	2.7	1	0.73	0.733 5.	.005	11404	711608	597846	13	2910	24053 25	910 0.77	1 48	6262	120014	24 0.524	63	1513	48	6442	2052 84	36	9 11.47 Provi	ide Anchors	0.73 2.17	1.73 8.06	8.06	3		300415 Needs And
Well 5	1036 Barrel Spring Roa	ad						1963	30 1,	463,945	Unknow	m 22	3	2.5	Ш	1.5 1.3	11 1.78	3.1	.8	0.62	1.364 2.	.691	15551	970375	680168	8	5412	23283 54	112 0.76	4 54	4500	301560	15 0.442	133	1982	56	4918	1758 84	27	6 5.05 Provi	ide Anchors	0.62 1.56	1.62 9.29	9.29	3	526 561.	571023 Needs And
	response acceleration par trum for impulsive compo						,													ravity, g.																											

Facility list indicates that these facilities conatain 0 gallons and does not provide the overflow height, therefore we were not apple to determine the seismic demands on these structures.
 A.WWA D100 calculations do not apply to the El Camino Underground tank. Construction drawings are not available to perform an analysis at this time.
 Minimum required freeboard is equal to the sloshing wave height for Use Group III and may be reduced for Use Group I and III.



Search Information

Coordinates: 34.557353817153206, -118.11224470422972

Elevation: 2750 ft

Timestamp: 2021-04-09T16:22:17.704Z

Hazard Type: Seismic

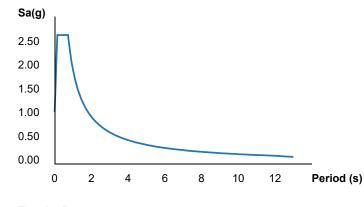
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

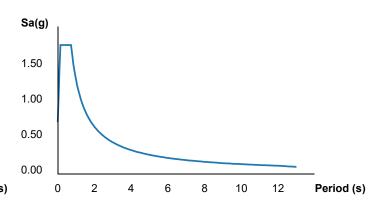
MCER Horizontal Response Spectrum





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Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.707	MCE _R ground motion (period=0.2s)
S ₁	1.315	MCE _R ground motion (period=1.0s)
S _{MS}	2.707	Site-modified spectral acceleration value
S _{M1}	1.973	Site-modified spectral acceleration value
S _{DS}	1.805	Numeric seismic design value at 0.2s SA
S _{D1}	1.315	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.919	Coefficient of risk (0.2s)
CR ₁	0.903	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:22 AM

PGA	1.045	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.045	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.418	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.719	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.707	Factored deterministic acceleration value (0.2s)
S1RT	1.605	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.778	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.315	Factored deterministic acceleration value (1.0s)
PGAd	1.045	Factored deterministic acceleration value (PGA)

Disclaimer

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Search Information

34.53471326457233, -118.08343773439331 Coordinates:

Elevation: 2968 ft

Timestamp: 2021-04-09T16:35:02.162Z

Hazard Type: Seismic

Reference ASCE7-10

Document:

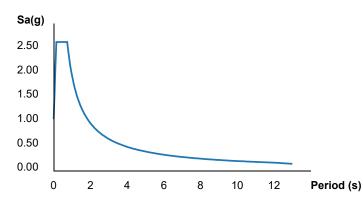
Risk Category: IV

Site Class: D

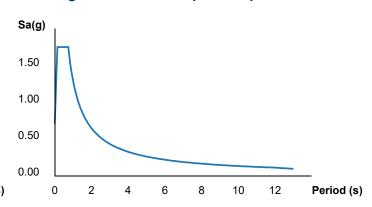
2968 ft Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S.

Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.646	MCE _R ground motion (period=0.2s)
S ₁	1.302	MCE _R ground motion (period=1.0s)
S _{MS}	2.646	Site-modified spectral acceleration value
S _{M1}	1.953	Site-modified spectral acceleration value
S _{DS}	1.764	Numeric seismic design value at 0.2s SA
S _{D1}	1.302	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.924	Coefficient of risk (0.2s)
CR ₁	0.904	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:35 AM

PGA	1.018	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.018	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.282	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.552	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.646	Factored deterministic acceleration value (0.2s)
S1RT	1.53	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.694	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.302	Factored deterministic acceleration value (1.0s)
PGAd	1.018	Factored deterministic acceleration value (PGA)

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Search Information

34547 Address:

Coordinates: 34.5497, -118.132821

Elevation: 2923 ft

2021-04-08T21:00:34.329Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

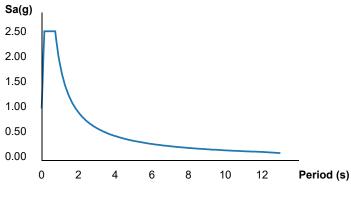
Document:

Risk Category: Ш

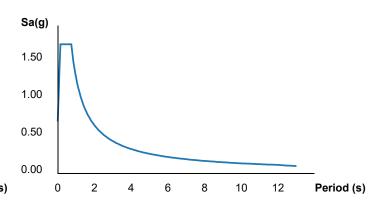
Site Class:

wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.573	MCE _R ground motion (period=0.2s)
S ₁	1.271	MCE _R ground motion (period=1.0s)
S _{MS}	2.573	Site-modified spectral acceleration value
S _{M1}	1.906	Site-modified spectral acceleration value
S _{DS}	1.715	Numeric seismic design value at 0.2s SA
S _{D1}	1.271	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.916	Coefficient of risk (0.2s)

4/8/2021, 3:01 PM 1 of 2

CR ₁	0.904	Coefficient of risk (1.0s)
PGA	0.987	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.987	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.429	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.743	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.573	Factored deterministic acceleration value (0.2s)
S1RT	1.614	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.785	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.271	Factored deterministic acceleration value (1.0s)
PGAd	0.987	Factored deterministic acceleration value (PGA)

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2 of 2 4/8/2021, 3:01 PM

ATC Hazards by Location

Search Information

Coordinates: 34.559419345037064, -118.11618400870667

Elevation: 2750 ft

Timestamp: 2021-04-09T16:36:57.402Z

Hazard Type: Seismic

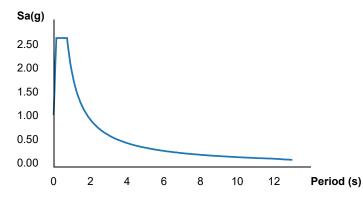
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

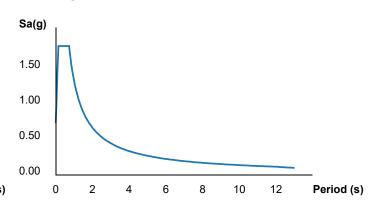
MCER Horizontal Response Spectrum





ivan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.706	MCE _R ground motion (period=0.2s)
S ₁	1.316	MCE _R ground motion (period=1.0s)
S _{MS}	2.706	Site-modified spectral acceleration value
S _{M1}	1.975	Site-modified spectral acceleration value
S _{DS}	1.804	Numeric seismic design value at 0.2s SA
S _{D1}	1.316	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.92	Coefficient of risk (0.2s)
CR ₁	0.903	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:37 AM

PGA	1.046	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.046	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.37	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.665	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.706	Factored deterministic acceleration value (0.2s)
S1RT	1.58	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.749	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.316	Factored deterministic acceleration value (1.0s)
PGAd	1.046	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.55371, -118.087856

Elevation: 2752 ft

Timestamp: 2021-04-09T16:19:01.173Z

Hazard Type: Seismic

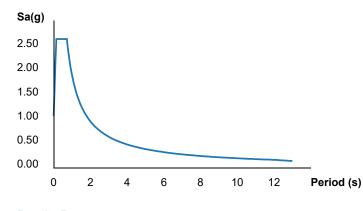
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

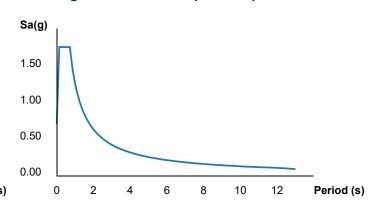
MCER Horizontal Response Spectrum



Ave 2752 ft 27

Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.668	MCE _R ground motion (period=0.2s)
S ₁	1.278	MCE _R ground motion (period=1.0s)
S _{MS}	2.668	Site-modified spectral acceleration value
S _{M1}	1.917	Site-modified spectral acceleration value
S _{DS}	1.779	Numeric seismic design value at 0.2s SA
S _{D1}	1.278	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.919	Coefficient of risk (0.2s)
CR ₁	0.902	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:19 AM

PGA	1.031	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.031	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.432	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.737	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.668	Factored deterministic acceleration value (0.2s)
S1RT	1.613	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.788	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.278	Factored deterministic acceleration value (1.0s)
PGAd	1.031	Factored deterministic acceleration value (PGA)

Disclaimer

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Search Information

Coordinates: 34.55371, -118.087856

Elevation: 2752 ft

Timestamp: 2021-04-09T16:17:53.781Z

Hazard Type: Seismic

Reference ASCE7-16

Document:

Risk Category: IV

Site Class: D-default



Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Basic Parameters

Name	Value	Description
S _S	2.404	MCE _R ground motion (period=0.2s)
S ₁	1.025	MCE _R ground motion (period=1.0s)
S _{MS}	2.885	Site-modified spectral acceleration value
S _{M1}	* null	Site-modified spectral acceleration value
S _{DS}	1.923	Numeric seismic design value at 0.2s SA
S _{D1}	* null	Numeric seismic design value at 1.0s SA

^{*} See Section 11.4.8

▼Additional Information

Name	Value	Description
SDC	* null	Seismic design category
Fa	1.2	Site amplification factor at 0.2s
F _v	* null	Site amplification factor at 1.0s
CRS	0.874	Coefficient of risk (0.2s)
CR ₁	0.869	Coefficient of risk (1.0s)
PGA	1.033	MCE _G peak ground acceleration
F _{PGA}	1.2	Site amplification factor at PGA
PGA _M	1.24	Site modified peak ground acceleration

1 of 2 4/9/2021, 10:18 AM

TL	12	Long-period transition period (s)
SsRT	3.008	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.441	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.404	Factored deterministic acceleration value (0.2s)
S1RT	1.294	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.489	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.025	Factored deterministic acceleration value (1.0s)
PGAd	1.033	Factored deterministic acceleration value (PGA)

^{*} See Section 11.4.8

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ATC Hazards by Location

Search Information

Coordinates: 34.544961034712664, -118.04877924893493

Elevation: 2740 ft

Timestamp: 2021-04-09T16:27:34.922Z

Hazard Type: Seismic

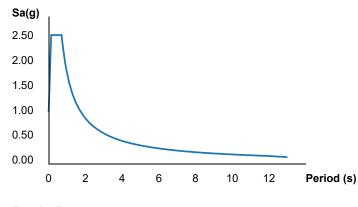
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

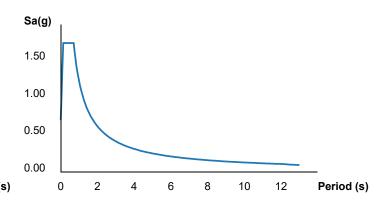
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.584	MCE _R ground motion (period=0.2s)
S ₁	1.214	MCE _R ground motion (period=1.0s)
S _{MS}	2.584	Site-modified spectral acceleration value
S _{M1}	1.821	Site-modified spectral acceleration value
S _{DS}	1.723	Numeric seismic design value at 0.2s SA
S _{D1}	1.214	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.921	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:27 AM

PGA	0.996	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.996	Site modified peak ground acceleration
T_L	12	Long-period transition period (s)
SsRT	3.159	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.432	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.584	Factored deterministic acceleration value (0.2s)
S1RT	1.47	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.624	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.214	Factored deterministic acceleration value (1.0s)
PGAd	0.996	Factored deterministic acceleration value (PGA)

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ATC Hazards by Location

Search Information

Coordinates: 34.52903336279662, -118.04584351481934

Elevation: 2971 ft

Timestamp: 2021-04-09T16:31:06.633Z

Hazard Type: Seismic

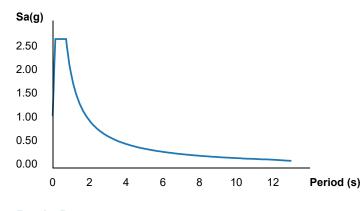
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

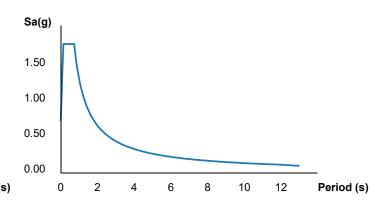
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.714	MCE _R ground motion (period=0.2s)
S ₁	1.325	MCE _R ground motion (period=1.0s)
S _{MS}	2.714	Site-modified spectral acceleration value
S _{M1}	1.987	Site-modified spectral acceleration value
S _{DS}	1.81	Numeric seismic design value at 0.2s SA
S _{D1}	1.325	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.923	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:31 AM

PGA	1.048	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.048	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.142	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.404	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.714	Factored deterministic acceleration value (0.2s)
S1RT	1.461	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.614	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.325	Factored deterministic acceleration value (1.0s)
PGAd	1.048	Factored deterministic acceleration value (PGA)

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8

10

12

Period (s)

Geological Survey, USDA Farm Service Agency

ATC Hazards by Location

Search Information

Coordinates: 34.536316858195896, -118.04017088147585

8

10

Elevation: 2825 ft

Timestamp: 2021-04-09T16:33:04.897Z

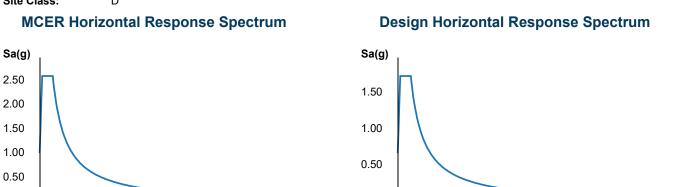
Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D



0.00

0

2

Period (s)

Basic Parameters

0.00

0

Name	Value	Description
S _S	2.652	MCE _R ground motion (period=0.2s)
S ₁	1.26	MCE _R ground motion (period=1.0s)
S _{MS}	2.652	Site-modified spectral acceleration value
S _{M1}	1.889	Site-modified spectral acceleration value
S _{DS}	1.768	Numeric seismic design value at 0.2s SA
S _{D1}	1.26	Numeric seismic design value at 1.0s SA

12

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.923	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:33 AM

PGA	1.024	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.024	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.121	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.381	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.652	Factored deterministic acceleration value (0.2s)
S1RT	1.449	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.602	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.26	Factored deterministic acceleration value (1.0s)
PGAd	1.024	Factored deterministic acceleration value (PGA)

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ATC Hazards by Location

Search Information

Coordinates: 34.54972773620536, -118.1502535834671

Elevation: 3116 ft

Timestamp: 2021-04-09T16:41:41.594Z

Hazard Type: Seismic

Reference ASCE7-10

Document:

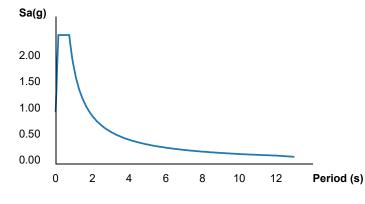
Risk Category: IV

Site Class: D

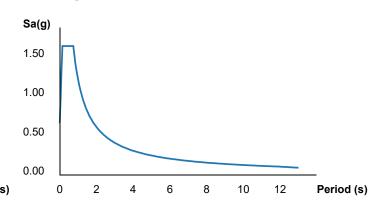
3116 ft & Accienda Dr. Wan data @2021 Imagery @2021 Maxar Technologies, U.S. Geological Surve

wan data ©2021 Imagery ©2021 , Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



MCER Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.458	MCE _R ground motion (period=0.2s)
S ₁	1.214	MCE _R ground motion (period=1.0s)
S _{MS}	2.458	Site-modified spectral acceleration value
S _{M1}	1.82	Site-modified spectral acceleration value
S _{DS}	1.639	Numeric seismic design value at 0.2s SA
S _{D1}	1.214	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.916	Coefficient of risk (0.2s)
CR ₁	0.906	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:41 AM

PGA	0.945	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.945	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.335	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.642	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.458	Factored deterministic acceleration value (0.2s)
S1RT	1.566	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.728	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.214	Factored deterministic acceleration value (1.0s)
PGAd	0.945	Factored deterministic acceleration value (PGA)

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Search Information

36809 El Camino Dr, Palmdale, CA 93551, USA Address:

34.54952240000001, -118.1326806 Coordinates:

Elevation: 2925 ft

2021-04-09T16:20:57.078Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: IV

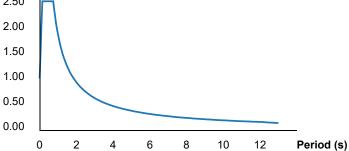
Site Class:

2925 ft

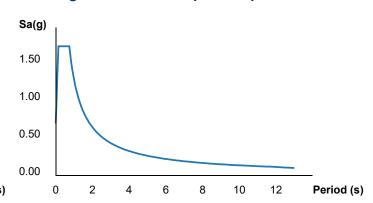
wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum

Sa(g) 2.50



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.571	MCE _R ground motion (period=0.2s)
S ₁	1.27	MCE _R ground motion (period=1.0s)
S _{MS}	2.571	Site-modified spectral acceleration value
S _{M1}	1.905	Site-modified spectral acceleration value
S _{DS}	1.714	Numeric seismic design value at 0.2s SA
S _{D1}	1.27	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.916	Coefficient of risk (0.2s)

1 of 2 4/9/2021, 10:21 AM

CR ₁	0.904	Coefficient of risk (1.0s)
PGA	0.986	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.986	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.426	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.74	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.571	Factored deterministic acceleration value (0.2s)
S1RT	1.613	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.783	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.27	Factored deterministic acceleration value (1.0s)
PGAd	0.986	Factored deterministic acceleration value (PGA)

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Coordinates: 34.53840630847815, -118.13288506137695

Elevation: 3359 ft

Timestamp: 2021-04-09T20:04:43.993Z

Hazard Type: Seismic

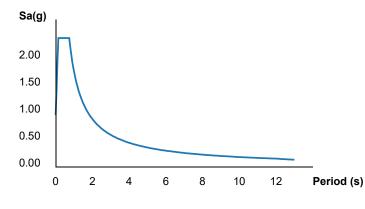
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

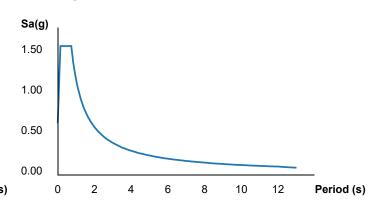
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.375	MCE _R ground motion (period=0.2s)
S ₁	1.171	MCE _R ground motion (period=1.0s)
S _{MS}	2.375	Site-modified spectral acceleration value
S _{M1}	1.756	Site-modified spectral acceleration value
S _{DS}	1.583	Numeric seismic design value at 0.2s SA
S _{D1}	1.171	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.925	Coefficient of risk (0.2s)
CR ₁	0.908	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 2:04 PM

PGA	0.917	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.917	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.236	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.499	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.375	Factored deterministic acceleration value (0.2s)
S1RT	1.505	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.657	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.171	Factored deterministic acceleration value (1.0s)
PGAd	0.917	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:04 PM



34.56128566737895, -118.12898168848265 Coordinates:

Elevation: 2924 ft

Timestamp: 2021-04-09T20:40:24.218Z

Hazard Type: Seismic

ASCE7-10 Reference

Document:

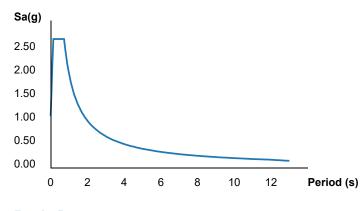
Risk Category: IV

Site Class: D

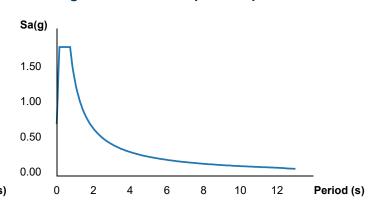
2924 ft Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S.

Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.733	MCE _R ground motion (period=0.2s)
S ₁	1.331	MCE _R ground motion (period=1.0s)
S _{MS}	2.733	Site-modified spectral acceleration value
S _{M1}	1.997	Site-modified spectral acceleration value
S _{DS}	1.822	Numeric seismic design value at 0.2s SA
S _{D1}	1.331	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.92	Coefficient of risk (0.2s)
CR ₁	0.904	Coefficient of risk (1.0s)

4/9/2021, 2:40 PM 1 of 2

PGA	1.055	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.055	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.306	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.594	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.733	Factored deterministic acceleration value (0.2s)
S1RT	1.547	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.71	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.331	Factored deterministic acceleration value (1.0s)
PGAd	1.055	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:40 PM

Search Information

34547 Address:

34.538438, -118.132863 Coordinates:

Elevation: 3360 ft

2021-04-08T22:06:10.243Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: Ш

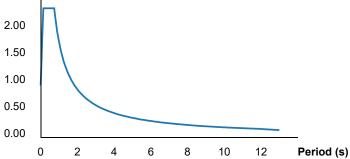
Site Class:

3360 ft

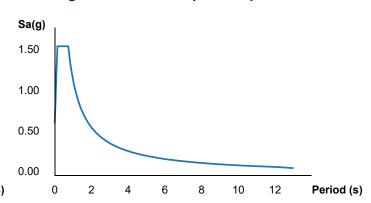
wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum

Sa(g)



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.376	MCE _R ground motion (period=0.2s)
S ₁	1.171	MCE _R ground motion (period=1.0s)
S _{MS}	2.376	Site-modified spectral acceleration value
S _{M1}	1.757	Site-modified spectral acceleration value
S _{DS}	1.584	Numeric seismic design value at 0.2s SA
S _{D1}	1.171	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.925	Coefficient of risk (0.2s)

4/8/2021, 4:06 PM 1 of 2

CR ₁	0.908	Coefficient of risk (1.0s)
PGA	0.917	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.917	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.236	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.5	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.376	Factored deterministic acceleration value (0.2s)
S1RT	1.505	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.657	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.171	Factored deterministic acceleration value (1.0s)
PGAd	0.917	Factored deterministic acceleration value (PGA)

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2 of 2 4/8/2021, 4:06 PM

Search Information

Coordinates: 34.598759799594845, -118.09844223112182

Elevation: 2583 ft

Timestamp: 2021-04-09T20:48:48.917Z

Hazard Type: Seismic

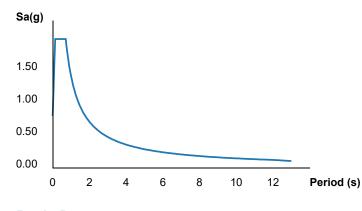
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

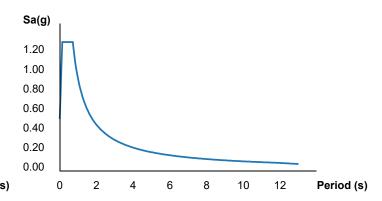
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	1.971	MCE _R ground motion (period=0.2s)
S ₁	0.937	MCE _R ground motion (period=1.0s)
S _{MS}	1.971	Site-modified spectral acceleration value
S _{M1}	1.406	Site-modified spectral acceleration value
S _{DS}	1.314	Numeric seismic design value at 0.2s SA
S _{D1}	0.937	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.937	Coefficient of risk (0.2s)
CR ₁	0.911	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 2:48 PM

PGA	0.77	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.77	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	2.602	Probabilistic risk-targeted ground motion (0.2s)
SsUH	2.776	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	1.971	Factored deterministic acceleration value (0.2s)
S1RT	1.168	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.282	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	0.937	Factored deterministic acceleration value (1.0s)
PGAd	0.77	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:48 PM

Search Information

Address: 1036 Barrel Spring Road palmdale, ca

Coordinates: 34.5457226, -118.1085956

Elevation: 2817 ft

Timestamp: 2021-05-04T20:11:47.998Z

Hazard Type: Seismic

Reference

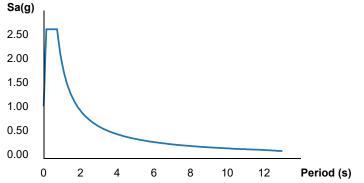
ASCE7-10

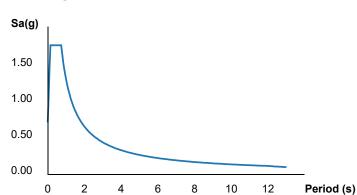
Document:

Risk Category:

Site Class: D

MCER Horizontal Response Spectrum Design Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

E Barrel Springs Rd

Basic Parameters

Name	Value	Description
S _S	2.674	MCE _R ground motion (period=0.2s)
S ₁	1.311	MCE _R ground motion (period=1.0s)
S _{MS}	2.674	Site-modified spectral acceleration value
S _{M1}	1.967	Site-modified spectral acceleration value
S _{DS}	1.782	Numeric seismic design value at 0.2s SA
S _{D1}	1.311	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.919	Coefficient of risk (0.2s)

1 of 2 5/4/2021, 2:13 PM

CR ₁	0.902	Coefficient of risk (1.0s)
PGA	1.029	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.029	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.49	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.799	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.674	Factored deterministic acceleration value (0.2s)
S1RT	1.643	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.821	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.311	Factored deterministic acceleration value (1.0s)
PGAd	1.029	Factored deterministic acceleration value (PGA)

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2 of 2 5/4/2021, 2:13 PM

Search Information

Address: 15 4640 Barrel Spring Road palmdale, ca

Coordinates: 34.5268275, -118.0540864

Elevation: 3036 ft

Timestamp: 2021-05-04T20:14:23.952Z

Hazard Type: Seismic

Reference ASCE7-10

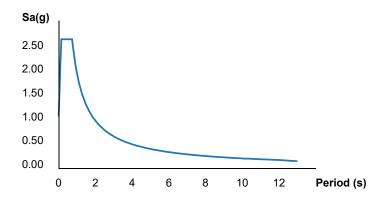
Document:

Risk Category:

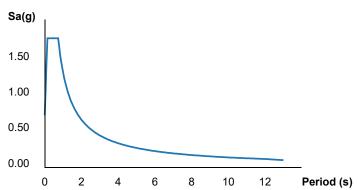
Site Class: D

3036 ft 3036 ft Religion Religion Ballely Common data © 2021 Imagery © 2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



MCER Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.7	MCE _R ground motion (period=0.2s)
S ₁	1.323	MCE _R ground motion (period=1.0s)
S _{MS}	2.7	Site-modified spectral acceleration value
S _{M1}	1.984	Site-modified spectral acceleration value
S _{DS}	1.8	Numeric seismic design value at 0.2s SA
S _{D1}	1.323	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.924	Coefficient of risk (0.2s)

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CR ₁	0.905	Coefficient of risk (1.0s)
PGA	1.04	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.04	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.149	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.409	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.7	Factored deterministic acceleration value (0.2s)
S1RT	1.464	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.617	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.323	Factored deterministic acceleration value (1.0s)
PGAd	1.04	Factored deterministic acceleration value (PGA)

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2 of 2 5/4/2021, 2:14 PM

												Ĭ																AWWA	D100-11 Welded O	Carbon Steel Tan	s Chapter 13 Seism	nic Design															
		Coord	dinates				T:	ank Details						Table 28	13.2.1	Table 24 AT	1 Eqn 13	9 ^{1,2} Eqn 1	3-22 E	qn 13-12/13 ²			13	3-27 1	3-25/26 Eqn 13-	28/29 Estimat	ate Estima	ate Estimate	Eqn 13-16		Eqn 13-24/25	Eqn 13-3)		Eqn 13-26	Eqn 13-31	Eqn 13-23	Eqn 13-37	Eqn 13-41	Eqn 13-36		Eqn 13-53/54	Eqn 13-52	Table 29	Equ	qn 13-57	
Tank Site	Address	Latitude	Longitude Tar	ık Type Co	Piping Foot nnection	ing	Anchorage	Date Built	Dia	Size Botton Knu		Overflow e Height	Freeboard Assumed to be 3 feet unless drawings indicate otherwise	Ri 3 if anchored 5 if unanchored		, assume that all Sels anks are ismic Use Ma Group III	nic Based on S	ts from		Sac, g ed on Sd1 from ASCE 7-10	D/H 3.67	7*D/H Vol =	olume ft ² : π*(Dia^2)/4	Total Weight, Ibf W = V Vol*62.4pcf	Impulsive latera	Sloshing Roof (ht of the Weig (Wr), lbf Shell	ght of the Weight of t (Ws), lbf Floor (Wf),	Implusive he Design lbf Acceleration (Al)	Impulsive Lateral Force (VI), kip	Overturning Moment due to Impulsive Lateral 1 Force(Mi), ft- kip	Convective Weight (Wc), lbf mass (X ft	al Convective to Design we Acceleration	Convective Lateral Force (Vc), kip	Overturning Moment due to Convective Lateral Force(Mc), ft- kip	Design Latera Force at the top of the foundation (Vf), kip		Maximum Resting Weigh of the Tank Contents (wt.) Ibf/ft	Weight of the Tank Shell and Roof Resisting Overturning (wt), lbf/ft		Anchor equirements	Convective Design Accelaration, Af	Sloshing Wave Height (d), ft	Required F Freeboard (D), (I	ctual Ai reeboard Roof Height- Lo lverflow)	Allowable Late Lateral Seis Load, Valow Load	otal teral ismic Sliding id, Vt (ip)
3 MG Tank Site	850 East Avenue S		-118.11 W	elded				1960	124 3,	000,000	Unknov	m 34	3	2.5	ш	1.5 1.3	15 1.80		-	0.27	3.647 1.	.006	410594	25621040	8082906	13	92459	138480 924	159 0.774	4 650	82912	16424329	18 0.192	3150	57649	722	100984	2185 539	474	4 2.54 Provi	ide Anchors	0.27 0.29	1.27 16.65	16.65	3	12851 7225.	.51729 OK
5 MG Tank	2404 Old Nadeau Road	ad 34.53	-118.08						160 5,	000,000	Unknov	vn 20	3	2.5	III .	1.5 1.3	02 1.76	11.1	13	0.13	8.000 0.	459	402124	25092529	3621894	8	153938	104550 153	938 0.756	6 305	22875	19810034	10 0.090	1784	18144	353	29197	1676 409	36:	1 0.57 Tank	k Is Stable	0.18 0.13	10.08	10.08	3	12338 35?	13.2461 OK
6MG	641 East Ave S		-118.15					1999	206 6,	000,000		vn 24	3	2.5		1.5 1.3	16 1.80	13.0	03	0.09	8.583 0.	.428	799900	49913745	6714999	9	255176	160865 255	176 0.77	3 571	51395	39739497	12 0.066	2640	32159	629	60628	1836 632	441	6 0.64 Tank		0.15 0.09	1.09 9.58	9.58	3	24349 6291.	
25th Street	26496 Cemetary Road	d 34.55	-118.09					1976	106 2,	000,000	Unknow	vn 30	3	2.5		1.5 1.3	16 1.80	6.7	4	0.29	3.533 1.	.039	264742	16519902	5375203	11	67564	104870 67	564 0.77	3 434	48840	10436273	16 0.209	2185	35431	486		2052 407	410	6 2.23 Provi		0.29 0.35		3 15.53	3	8304 4860.	.10557 OK
25til Street	20490 Cellietal y Road			elded No	t Flexible Ring	wall with Sand Interio	or	1967	154 4,	000,000	Unknow	vn 30	3	2.5		1.5 1.2	78 1.77	9.1	.3	0.18	5.133 0.	715	558795	34868813	7841520	11	142609	151052 142	509 0.762	2 631	71001	25267634	16 0.131	3318	51781	713	87878	2052 591	461	0 1.51 Uplift	ift but Stable	0.21 0.18	14.15	5 14.15	3	17380 7130.	
		34.54	-118.05					1988	200 0	000,000	Unknow		3	2.5		1.5 1.2	14 1.72						398197	24847485	6614006	11	101623	127961 101	523 0.731	8 512	57696	17074207	16 0.164	2809	44414	584	72811	2052 499	431	8 1.77 Provi	ide Anchors	0.23 0.23	1.23 14.95	14.95	3	12488 5845.	
45th Street	36510 45th St East							1990		000,000		m 32	3	2.5	III	1.5 1.2	1.72		_				565487	35286369	8687384	12	135297	157017 135		8 673	80769	24894926	17 0.137	3398	56992	754	98852	2120 614	47	7 1.74 Provi	ide Anchors	0.21 0.19	1.19 14.33	3 14.33	3	17687 7540.	
								1990		000,000	Unknov		3	2.5	III	1.5 1.2			_				565487	35286369	8687384	12	135297	157017 135	297 0.731	8 673	80769	24894926	17 0.137	3398	56992	754	98852	2120 614	47	7 1.74 Provi	ide Anchors	0.21 0.19	1.19 14.33	3 14.33	3	17687 7540.	
47th Street	35645 47th St East	34.53	-118.05					1967		000,000	Unknov		3	2.5	III	1.5 1.3	1.0.			0.00			264742	16519902	5375203	11	67564	104870 67	564 0.776	6 435	49003	10436273	16 0.211	2200	35674	488	60613	2052 407	416	6 2.24 Provi	ide Anchors	0.30 0.35	1.30 15.64	15.64	3	8301 4879.	
	***************************************							1990		000,000		vn 30	3	2.5	III	1.5 1.3							410543	25617904	6716566		104774	129885 104		6 547	61576	17698347	16 0.177	3126	49427	630	78960	2052 506	441	0 1.87 Provi		0.25 0.25	1.25 16.32	2 16.32	3	12801 6303.	
50th Street	5001 East Ave. T-8	34.54	-118.04							000,000		vn 30	3	2.5	III	1.5 1.3			_				530144	33080971	7637298			147203 135		8 610			16 0.135		50405			2052 576	450	6 1.55 Provi		0.21 0.19		2 14.22	3	16514 6902.	
	,			elded?		crete Ring Wall	None Shown	2007	150 4,	seejeee	Unknov		3	2.5	III	1.5 1.3			_				530144	33080971	7637298	11	135297	147203 135	297 0.751	8 610	68664	23796213	16 0.135	3223	50405	690	85178	2052 576	450	6 1.55 Provi	ide Anchors	0.21 0.19	1.19 14.22	2 14.22	3	16514 6902.	
Ana Verde	36800 Tovey Aveneu			elded No	t Flexible Con	crete Rink wall	Not Shown	1963		00,000	Unknov		3	2.5	III	1.5 1.2							40212	2509253	1825481	12	9621	44129 9	521 0.70	2 132	16240	717357	22 0.355	255	5658	135	17197	2120 163	385	9 5.44 Provi	ide Anchors	0.50 1.09	1.50 9.95	9.95	3		.04608 OK
El Camino Lower	36809 El Camino Dr.	34.55	-118.13					1988		000,000		vn 32	3	2.5	III	1.5 1.3	7 1.71	6.6	i3	0.29	3.313 1.	.108	282391	17621228	6103267	12	67564	111862 67	564 0.73	5 466	55977	10784811	17 0.205	2215	38666	516	68033	2120 434	43	7 2.42 Provi	ide Anchors	0.29 0.35	1.29 15.24	15.24	3	8916 5163.	.80732 OK
El Camino U.G ⁴	36336 El Camino Road	d						1994	104 1,	500,000	Unknov	vn 26																																			
El Camino Upper	33030 Ridge Route Rd	d 34.54	-118.13 W	elded I	Flexible Ring	wall with Sand Inte	None Shown	1963	40 3	00,000	Unknow	m 32	3	2.5	Ш	1.5 0.8	81 1.54	3.6	i6	0.36	1.250 2.	.936	40212	2509253	1825481	12	9621	44129 9	521 0.66	1 124	15289	717357	22 0.258	185	4106	126		2120 163	385	9 5.00 Provi	ide Anchors	0.36 0.79	1.36 7.22	7.22	3	1371 1262.	.69341 OK
Walt Dahlitz	115 East Avenue S		W	elded I	Flexible Con-	rete Ringwall, oil s	None Shown	1993	104 1,	500,000	Unknow	vn 31	3	2.5	Ш	1.5 0.8	27 1.44	6.5	i8	0.19	3.355 1.	.094	263341	16432470	5622265	12	65039	106378 658	0.61	8 362	42091	10122208	17 0.135	1362	22997	386		2086 412	42	5 1.80 Provi	ide Anchors	0.19 0.23	9.80	9.80	3	8455 3868.	
Well 14	36401 20th ST East		W	leled? No	t Flexible Con	crete Ringwall, grav	3/4" 5' OC 8" embed		27 1	00,000	Unknow	m 22	3	2.5	Ш	1.5 0.9	27 1.51	3.0	11	0.46	1.227 2.	.990	12596	786004	575712	8	4384	21166 4	384 0.649	9 39	3325	220749	15 0.330	73	1119	40		1758 76	27	5 4.80 Provi	ide Anchors	0.46 1.23	1.46 6.24	6.24	3	435 399.6	85968 OK
Well 18 and 19	4640 Barrel Springs Roa	ad						1963	22	1,000	Unknow	vn 30	3	2.5	Ш	1.5 1.3	23 1.8	2.7	1	0.73	0.733 5.	.005	11404	711608	597846	13	2910	24053 25	910 0.77	1 48	6262	120014	24 0.524	63	1513	48	6442	2052 84	36	9 11.47 Provi	ide Anchors	0.73 2.17	1.73 8.06	8.06	3		300415 Needs And
Well 5	1036 Barrel Spring Roa	ad						1963	30 1,	463,945	Unknow	m 22	3	2.5	Ш	1.5 1.3	11 1.78	3.1	.8	0.62	1.364 2.	.691	15551	970375	680168	8	5412	23283 54	112 0.76	4 54	4500	301560	15 0.442	133	1982	56	4918	1758 84	27	6 5.05 Provi	ide Anchors	0.62 1.56	1.62 9.29	9.29	3	526 561.	571023 Needs And
	gn spectral response acceleration parameters, S_{cs} and S_{tr} , have been determined using the Applied Technology Council's (ATC) web based hazard maps in accordance with the American Society of Civil Engineers Standard 7, Minimum Design Loads for Buildings and Other Structures (ASCE 7-10) Design spectrum for impulsive components, Sai and the Design Spectrum for convective components, Sai chave been determined in accordance with Chapter 13 of the AWWA D100-11, Welded Carbon Steel Trails for Water Storage. These parameters are expressed as a percentage of the acceleration due to gravity, g.																																														

Facility list indicates that these facilities conatain 0 gallons and does not provide the overflow height, therefore we were not apple to determine the seismic demands on these structures.
 A.WWA D100 calculations do not apply to the El Camino Underground tank. Construction drawings are not available to perform an analysis at this time.
 Minimum required freeboard is equal to the sloshing wave height for Use Group III and may be reduced for Use Group I and III.



Coordinates: 34.557353817153206, -118.11224470422972

Elevation: 2750 ft

Timestamp: 2021-04-09T16:22:17.704Z

Hazard Type: Seismic

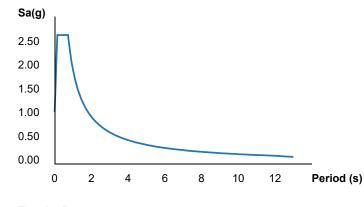
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

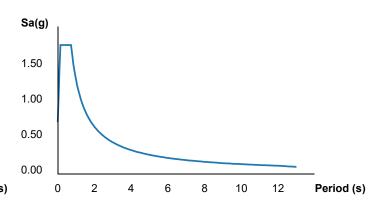
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.707	MCE _R ground motion (period=0.2s)
S ₁	1.315	MCE _R ground motion (period=1.0s)
S _{MS}	2.707	Site-modified spectral acceleration value
S _{M1}	1.973	Site-modified spectral acceleration value
S _{DS}	1.805	Numeric seismic design value at 0.2s SA
S _{D1}	1.315	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description							
SDC	F	Seismic design category							
Fa	1	Site amplification factor at 0.2s							
F _v	1.5	Site amplification factor at 1.0s							
CRS	0.919	Coefficient of risk (0.2s)							
CR ₁	0.903	Coefficient of risk (1.0s)							

1 of 2 4/9/2021, 10:22 AM

PGA	1.045	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.045	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.418	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.719	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.707	Factored deterministic acceleration value (0.2s)
S1RT	1.605	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.778	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.315	Factored deterministic acceleration value (1.0s)
PGAd	1.045	Factored deterministic acceleration value (PGA)

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34.53471326457233, -118.08343773439331 Coordinates:

Elevation: 2968 ft

Timestamp: 2021-04-09T16:35:02.162Z

Hazard Type: Seismic

Reference ASCE7-10

Document:

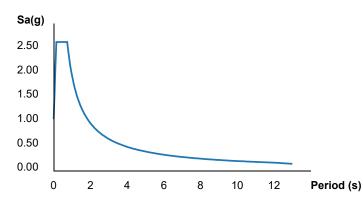
Risk Category: IV

Site Class: D

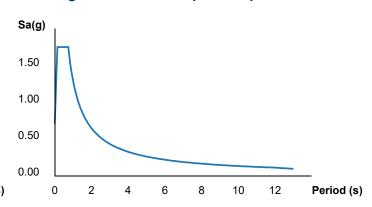
2968 ft Map data @2021 Imagery @2021, CNES / Airbus, Maxar Technologies, U.S.

Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.646	MCE _R ground motion (period=0.2s)
S ₁	1.302	MCE _R ground motion (period=1.0s)
S _{MS}	2.646	Site-modified spectral acceleration value
S _{M1}	1.953	Site-modified spectral acceleration value
S _{DS}	1.764	Numeric seismic design value at 0.2s SA
S _{D1}	1.302	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.924	Coefficient of risk (0.2s)
CR ₁	0.904	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:35 AM

PGA	1.018	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.018	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.282	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.552	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.646	Factored deterministic acceleration value (0.2s)
S1RT	1.53	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.694	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.302	Factored deterministic acceleration value (1.0s)
PGAd	1.018	Factored deterministic acceleration value (PGA)

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34547 Address:

Coordinates: 34.5497, -118.132821

Elevation: 2923 ft

2021-04-08T21:00:34.329Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

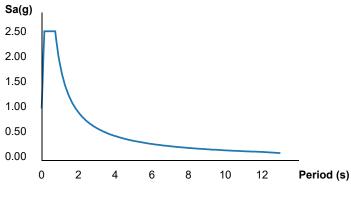
Document:

Risk Category: Ш

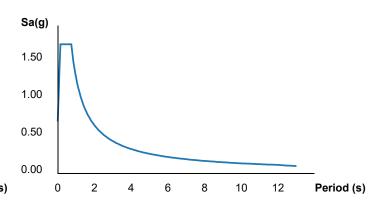
Site Class:

wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.573	MCE _R ground motion (period=0.2s)
S ₁	1.271	MCE _R ground motion (period=1.0s)
S _{MS}	2.573	Site-modified spectral acceleration value
S _{M1}	1.906	Site-modified spectral acceleration value
S _{DS}	1.715	Numeric seismic design value at 0.2s SA
S _{D1}	1.271	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.916	Coefficient of risk (0.2s)

4/8/2021, 3:01 PM 1 of 2

CR ₁	0.904	Coefficient of risk (1.0s)
PGA	0.987	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.987	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.429	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.743	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.573	Factored deterministic acceleration value (0.2s)
S1RT	1.614	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.785	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.271	Factored deterministic acceleration value (1.0s)
PGAd	0.987	Factored deterministic acceleration value (PGA)

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2 of 2 4/8/2021, 3:01 PM

Search Information

Coordinates: 34.559419345037064, -118.11618400870667

Elevation: 2750 ft

Timestamp: 2021-04-09T16:36:57.402Z

Hazard Type: Seismic

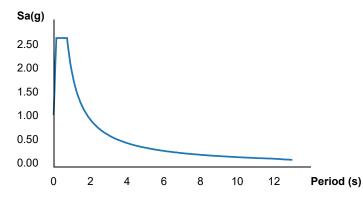
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

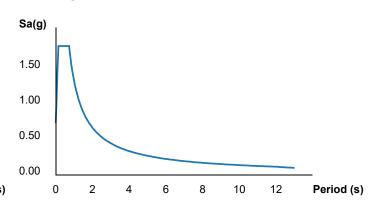
MCER Horizontal Response Spectrum





ivan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.706	MCE _R ground motion (period=0.2s)
S ₁	1.316	MCE _R ground motion (period=1.0s)
S _{MS}	2.706	Site-modified spectral acceleration value
S _{M1}	1.975	Site-modified spectral acceleration value
S _{DS}	1.804	Numeric seismic design value at 0.2s SA
S _{D1}	1.316	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.92	Coefficient of risk (0.2s)
CR ₁	0.903	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:37 AM

PGA	1.046	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.046	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.37	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.665	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.706	Factored deterministic acceleration value (0.2s)
S1RT	1.58	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.749	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.316	Factored deterministic acceleration value (1.0s)
PGAd	1.046	Factored deterministic acceleration value (PGA)

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Coordinates: 34.55371, -118.087856

Elevation: 2752 ft

Timestamp: 2021-04-09T16:19:01.173Z

Hazard Type: Seismic

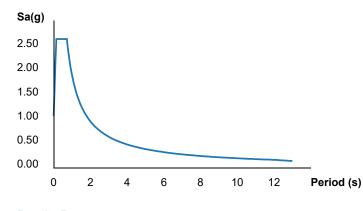
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

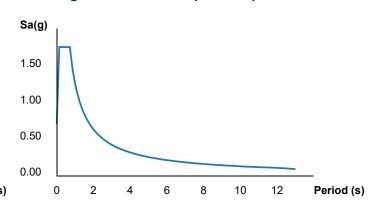
MCER Horizontal Response Spectrum



Ave 2752 ft 27

Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.668	MCE _R ground motion (period=0.2s)
S ₁	1.278	MCE _R ground motion (period=1.0s)
S _{MS}	2.668	Site-modified spectral acceleration value
S _{M1}	1.917	Site-modified spectral acceleration value
S _{DS}	1.779	Numeric seismic design value at 0.2s SA
S _{D1}	1.278	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.919	Coefficient of risk (0.2s)
CR ₁	0.902	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:19 AM

PGA	1.031	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.031	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.432	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.737	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.668	Factored deterministic acceleration value (0.2s)
S1RT	1.613	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.788	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.278	Factored deterministic acceleration value (1.0s)
PGAd	1.031	Factored deterministic acceleration value (PGA)

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Coordinates: 34.55371, -118.087856

Elevation: 2752 ft

Timestamp: 2021-04-09T16:17:53.781Z

Hazard Type: Seismic

Reference ASCE7-16

Document:

Risk Category: IV

Site Class: D-default



Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Basic Parameters

Name	Value	Description
S _S	2.404	MCE _R ground motion (period=0.2s)
S ₁	1.025	MCE _R ground motion (period=1.0s)
S _{MS}	2.885	Site-modified spectral acceleration value
S _{M1}	* null	Site-modified spectral acceleration value
S _{DS}	1.923	Numeric seismic design value at 0.2s SA
S _{D1}	* null	Numeric seismic design value at 1.0s SA

^{*} See Section 11.4.8

▼Additional Information

Name	Value	Description
SDC	* null	Seismic design category
Fa	1.2	Site amplification factor at 0.2s
F _v	* null	Site amplification factor at 1.0s
CRS	0.874	Coefficient of risk (0.2s)
CR ₁	0.869	Coefficient of risk (1.0s)
PGA	1.033	MCE _G peak ground acceleration
F _{PGA}	1.2	Site amplification factor at PGA
PGA _M	1.24	Site modified peak ground acceleration

1 of 2 4/9/2021, 10:18 AM

TL	12	Long-period transition period (s)
SsRT	3.008	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.441	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.404	Factored deterministic acceleration value (0.2s)
S1RT	1.294	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.489	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.025	Factored deterministic acceleration value (1.0s)
PGAd	1.033	Factored deterministic acceleration value (PGA)

^{*} See Section 11.4.8

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Search Information

Coordinates: 34.544961034712664, -118.04877924893493

Elevation: 2740 ft

Timestamp: 2021-04-09T16:27:34.922Z

Hazard Type: Seismic

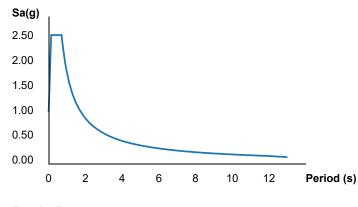
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

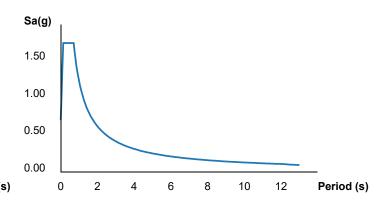
MCER Horizontal Response Spectrum





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Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.584	MCE _R ground motion (period=0.2s)
S ₁	1.214	MCE _R ground motion (period=1.0s)
S _{MS}	2.584	Site-modified spectral acceleration value
S _{M1}	1.821	Site-modified spectral acceleration value
S _{DS}	1.723	Numeric seismic design value at 0.2s SA
S _{D1}	1.214	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.921	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:27 AM

PGA	0.996	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.996	Site modified peak ground acceleration
T_L	12	Long-period transition period (s)
SsRT	3.159	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.432	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.584	Factored deterministic acceleration value (0.2s)
S1RT	1.47	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.624	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.214	Factored deterministic acceleration value (1.0s)
PGAd	0.996	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.52903336279662, -118.04584351481934

Elevation: 2971 ft

Timestamp: 2021-04-09T16:31:06.633Z

Hazard Type: Seismic

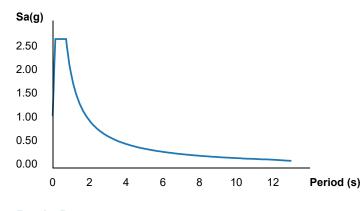
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

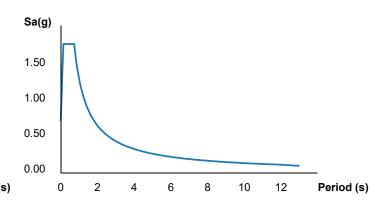
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.714	MCE _R ground motion (period=0.2s)
S ₁	1.325	MCE _R ground motion (period=1.0s)
S _{MS}	2.714	Site-modified spectral acceleration value
S _{M1}	1.987	Site-modified spectral acceleration value
S _{DS}	1.81	Numeric seismic design value at 0.2s SA
S _{D1}	1.325	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.923	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:31 AM

PGA	1.048	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.048	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.142	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.404	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.714	Factored deterministic acceleration value (0.2s)
S1RT	1.461	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.614	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.325	Factored deterministic acceleration value (1.0s)
PGAd	1.048	Factored deterministic acceleration value (PGA)

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8

10

12

Period (s)

Geological Survey, USDA Farm Service Agency

ATC Hazards by Location

Search Information

Coordinates: 34.536316858195896, -118.04017088147585

8

10

Elevation: 2825 ft

Timestamp: 2021-04-09T16:33:04.897Z

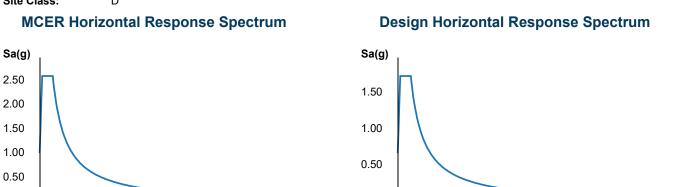
Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D



0.00

0

2

Period (s)

Basic Parameters

0.00

0

Name	Value	Description
S _S	2.652	MCE _R ground motion (period=0.2s)
S ₁	1.26	MCE _R ground motion (period=1.0s)
S _{MS}	2.652	Site-modified spectral acceleration value
S _{M1}	1.889	Site-modified spectral acceleration value
S _{DS}	1.768	Numeric seismic design value at 0.2s SA
S _{D1}	1.26	Numeric seismic design value at 1.0s SA

12

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.923	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:33 AM

PGA	1.024	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.024	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.121	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.381	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.652	Factored deterministic acceleration value (0.2s)
S1RT	1.449	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.602	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.26	Factored deterministic acceleration value (1.0s)
PGAd	1.024	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.54972773620536, -118.1502535834671

Elevation: 3116 ft

Timestamp: 2021-04-09T16:41:41.594Z

Hazard Type: Seismic

Reference ASCE7-10

Document:

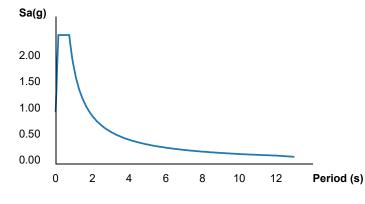
Risk Category: IV

Site Class: D

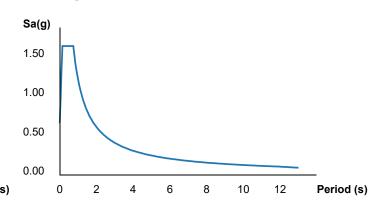
3116 ft & Accienda Dr. Wan data @2021 Imagery @2021 Maxar Technologies, U.S. Geological Surve

wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



MCER Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.458	MCE _R ground motion (period=0.2s)
S ₁	1.214	MCE _R ground motion (period=1.0s)
S _{MS}	2.458	Site-modified spectral acceleration value
S _{M1}	1.82	Site-modified spectral acceleration value
S _{DS}	1.639	Numeric seismic design value at 0.2s SA
S _{D1}	1.214	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.916	Coefficient of risk (0.2s)
CR ₁	0.906	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:41 AM

PGA	0.945	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.945	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.335	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.642	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.458	Factored deterministic acceleration value (0.2s)
S1RT	1.566	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.728	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.214	Factored deterministic acceleration value (1.0s)
PGAd	0.945	Factored deterministic acceleration value (PGA)

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Search Information

36809 El Camino Dr, Palmdale, CA 93551, USA Address:

34.54952240000001, -118.1326806 Coordinates:

Elevation: 2925 ft

2021-04-09T16:20:57.078Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: IV

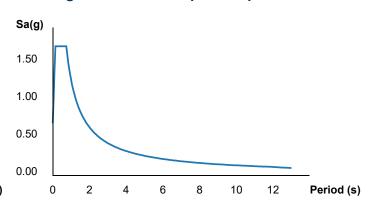
Site Class:

2925 ft wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum

Sa(g) 2.50 2.00 1.50 1.00 0.50 0.00 0 10 12 Period (s)

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.571	MCE _R ground motion (period=0.2s)
S ₁	1.27	MCE _R ground motion (period=1.0s)
S _{MS}	2.571	Site-modified spectral acceleration value
S _{M1}	1.905	Site-modified spectral acceleration value
S _{DS}	1.714	Numeric seismic design value at 0.2s SA
S _{D1}	1.27	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.916	Coefficient of risk (0.2s)

1 of 2 4/9/2021, 10:21 AM

CR ₁	0.904	Coefficient of risk (1.0s)
PGA	0.986	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.986	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.426	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.74	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.571	Factored deterministic acceleration value (0.2s)
S1RT	1.613	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.783	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.27	Factored deterministic acceleration value (1.0s)
PGAd	0.986	Factored deterministic acceleration value (PGA)

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Coordinates: 34.53840630847815, -118.13288506137695

Elevation: 3359 ft

Timestamp: 2021-04-09T20:04:43.993Z

Hazard Type: Seismic

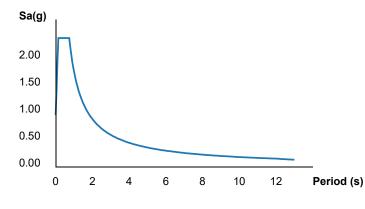
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

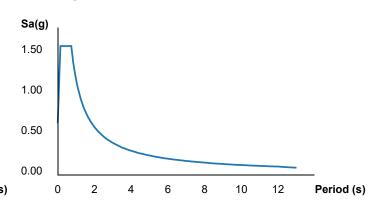
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.375	MCE _R ground motion (period=0.2s)
S ₁	1.171	MCE _R ground motion (period=1.0s)
S _{MS}	2.375	Site-modified spectral acceleration value
S _{M1}	1.756	Site-modified spectral acceleration value
S _{DS}	1.583	Numeric seismic design value at 0.2s SA
S _{D1}	1.171	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.925	Coefficient of risk (0.2s)
CR ₁	0.908	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 2:04 PM

PGA	0.917	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.917	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.236	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.499	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.375	Factored deterministic acceleration value (0.2s)
S1RT	1.505	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.657	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.171	Factored deterministic acceleration value (1.0s)
PGAd	0.917	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:04 PM



34.56128566737895, -118.12898168848265 Coordinates:

Elevation: 2924 ft

Timestamp: 2021-04-09T20:40:24.218Z

Hazard Type: Seismic

ASCE7-10 Reference

Document:

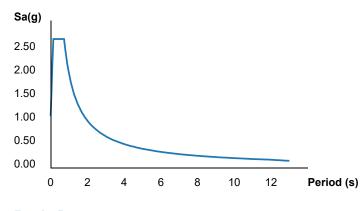
Risk Category: IV

Site Class: D

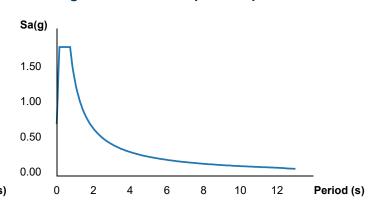
2924 ft Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S.

Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.733	MCE _R ground motion (period=0.2s)
S ₁	1.331	MCE _R ground motion (period=1.0s)
S _{MS}	2.733	Site-modified spectral acceleration value
S _{M1}	1.997	Site-modified spectral acceleration value
S _{DS}	1.822	Numeric seismic design value at 0.2s SA
S _{D1}	1.331	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.92	Coefficient of risk (0.2s)
CR ₁	0.904	Coefficient of risk (1.0s)

4/9/2021, 2:40 PM 1 of 2

PGA	1.055	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.055	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.306	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.594	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.733	Factored deterministic acceleration value (0.2s)
S1RT	1.547	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.71	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.331	Factored deterministic acceleration value (1.0s)
PGAd	1.055	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:40 PM

Search Information

34547 Address:

34.538438, -118.132863 Coordinates:

Elevation: 3360 ft

2021-04-08T22:06:10.243Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: Ш

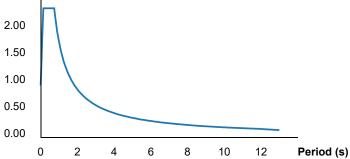
Site Class:

3360 ft

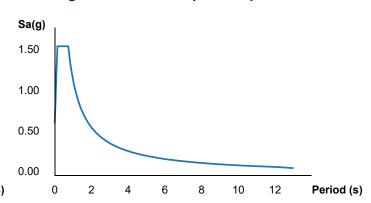
wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum

Sa(g)



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.376	MCE _R ground motion (period=0.2s)
S ₁	1.171	MCE _R ground motion (period=1.0s)
S _{MS}	2.376	Site-modified spectral acceleration value
S _{M1}	1.757	Site-modified spectral acceleration value
S _{DS}	1.584	Numeric seismic design value at 0.2s SA
S _{D1}	1.171	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.925	Coefficient of risk (0.2s)

4/8/2021, 4:06 PM 1 of 2

CR ₁	0.908	Coefficient of risk (1.0s)
PGA	0.917	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.917	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.236	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.5	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.376	Factored deterministic acceleration value (0.2s)
S1RT	1.505	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.657	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.171	Factored deterministic acceleration value (1.0s)
PGAd	0.917	Factored deterministic acceleration value (PGA)

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2 of 2 4/8/2021, 4:06 PM

Search Information

Coordinates: 34.598759799594845, -118.09844223112182

Elevation: 2583 ft

Timestamp: 2021-04-09T20:48:48.917Z

Hazard Type: Seismic

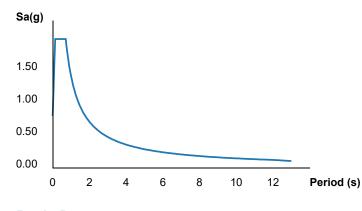
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

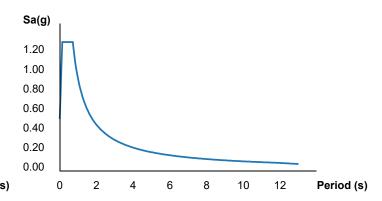
MCER Horizontal Response Spectrum





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Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	1.971	MCE _R ground motion (period=0.2s)
S ₁	0.937	MCE _R ground motion (period=1.0s)
S _{MS}	1.971	Site-modified spectral acceleration value
S _{M1}	1.406	Site-modified spectral acceleration value
S _{DS}	1.314	Numeric seismic design value at 0.2s SA
S _{D1}	0.937	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.937	Coefficient of risk (0.2s)
CR ₁	0.911	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 2:48 PM

PGA	0.77	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.77	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	2.602	Probabilistic risk-targeted ground motion (0.2s)
SsUH	2.776	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	1.971	Factored deterministic acceleration value (0.2s)
S1RT	1.168	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.282	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	0.937	Factored deterministic acceleration value (1.0s)
PGAd	0.77	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:48 PM

Search Information

Address: 1036 Barrel Spring Road palmdale, ca

Coordinates: 34.5457226, -118.1085956

Elevation: 2817 ft

Timestamp: 2021-05-04T20:11:47.998Z

Hazard Type: Seismic

Reference

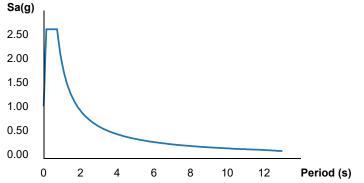
ASCE7-10

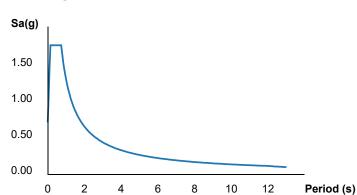
Document:

Risk Category:

Site Class: D

MCER Horizontal Response Spectrum Design Horizontal Response Spectrum





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E Barrel Springs Rd

Basic Parameters

Name	Value	Description
S _S	2.674	MCE _R ground motion (period=0.2s)
S ₁	1.311	MCE _R ground motion (period=1.0s)
S _{MS}	2.674	Site-modified spectral acceleration value
S _{M1}	1.967	Site-modified spectral acceleration value
S _{DS}	1.782	Numeric seismic design value at 0.2s SA
S _{D1}	1.311	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.919	Coefficient of risk (0.2s)

1 of 2 5/4/2021, 2:13 PM

CR ₁	0.902	Coefficient of risk (1.0s)
PGA	1.029	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.029	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.49	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.799	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.674	Factored deterministic acceleration value (0.2s)
S1RT	1.643	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.821	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.311	Factored deterministic acceleration value (1.0s)
PGAd	1.029	Factored deterministic acceleration value (PGA)

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2 of 2 5/4/2021, 2:13 PM

Search Information

Address: 15 4640 Barrel Spring Road palmdale, ca

Coordinates: 34.5268275, -118.0540864

Elevation: 3036 ft

Timestamp: 2021-05-04T20:14:23.952Z

Hazard Type: Seismic

Reference ASCE7-10

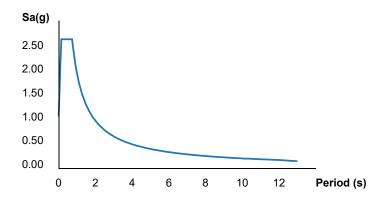
Document:

Risk Category:

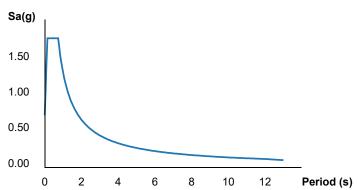
Site Class: D

3036 ft 3036 ft Religion Religion Ballely Common data © 2021 Imagery © 2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



MCER Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.7	MCE _R ground motion (period=0.2s)
S ₁	1.323	MCE _R ground motion (period=1.0s)
S _{MS}	2.7	Site-modified spectral acceleration value
S _{M1}	1.984	Site-modified spectral acceleration value
S _{DS}	1.8	Numeric seismic design value at 0.2s SA
S _{D1}	1.323	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.924	Coefficient of risk (0.2s)

1 of 2 5/4/2021, 2:14 PM

CR ₁	0.905	Coefficient of risk (1.0s)
PGA	1.04	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.04	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.149	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.409	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.7	Factored deterministic acceleration value (0.2s)
S1RT	1.464	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.617	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.323	Factored deterministic acceleration value (1.0s)
PGAd	1.04	Factored deterministic acceleration value (PGA)

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2 of 2 5/4/2021, 2:14 PM

												Ĭ																AWWA	D100-11 Welded O	Carbon Steel Tan	s Chapter 13 Seism	nic Design															
		Coord	dinates				T:	ank Details						Table 28	13.2.1	Table 24 AT	1 Eqn 13	9 ^{1,2} Eqn 1	3-22 E	qn 13-12/13 ²			13	3-27 1	3-25/26 Eqn 13-	28/29 Estimat	ate Estima	ate Estimate	Eqn 13-16		Eqn 13-24/25	Eqn 13-3)		Eqn 13-26	Eqn 13-31	Eqn 13-23	Eqn 13-37	Eqn 13-41	Eqn 13-36		Eqn 13-53/54	Eqn 13-52	Table 29	Equ	qn 13-57	
Tank Site	Address	Latitude	Longitude Tar	ık Type Co	Piping Foot nnection	ing	Anchorage	Date Built	Dia	Size Botton Knu		Overflow e Height	Freeboard Assumed to be 3 feet unless drawings indicate otherwise	Ri 3 if anchored 5 if unanchored		, assume that all Sels anks are ismic Use Ma Group III	nic Based on S	ts from		Sac, g ed on Sd1 from ASCE 7-10	D/H 3.67	7*D/H Vol =	olume ft ² : π*(Dia^2)/4	Total Weight, Ibf W = V Vol*62.4pcf	Impulsive latera	Sloshing Roof (ht of the Weig (Wr), lbf Shell	ght of the Weight of t (Ws), lbf Floor (Wf),	Implusive he Design lbf Acceleration (Al)	Impulsive Lateral Force (VI), kip	Overturning Moment due to Impulsive Lateral 1 Force(Mi), ft- kip	Convective Weight (Wc), lbf mass (X ft	al Convective to Design we Acceleration	Convective Lateral Force (Vc), kip	Overturning Moment due to Convective Lateral Force(Mc), ft- kip	Design Latera Force at the top of the foundation (Vf), kip		Maximum Resting Weigh of the Tank Contents (wt.) Ibf/ft	Weight of the Tank Shell and Roof Resisting Overturning (wt), lbf/ft		Anchor equirements	Convective Design Accelaration, Af	Sloshing Wave Height (d), ft	Required F Freeboard (D), (I	ctual Ai reeboard Roof Height- Lo lverflow)	Allowable Late Lateral Seis Load, Valow Load	otal teral ismic Sliding id, Vt (ip)
3 MG Tank Site	850 East Avenue S		-118.11 W	elded				1960	124 3,	000,000	Unknov	m 34	3	2.5	ш	1.5 1.3	15 1.80		-	0.27	3.647 1.	.006	410594	25621040	8082906	13	92459	138480 924	159 0.774	4 650	82912	16424329	18 0.192	3150	57649	722	100984	2185 539	474	4 2.54 Provi	ide Anchors	0.27 0.29	1.27 16.65	16.65	3	12851 7225.	.51729 OK
5 MG Tank	2404 Old Nadeau Road	ad 34.53	-118.08						160 5,	000,000	Unknov	vn 20	3	2.5	III .	1.5 1.3	02 1.76	11.1	13	0.13	8.000 0.	459	402124	25092529	3621894	8	153938	104550 153	938 0.756	6 305	22875	19810034	10 0.090	1784	18144	353	29197	1676 409	36:	1 0.57 Tank	k Is Stable	0.18 0.13	10.08	10.08	3	12338 35?	13.2461 OK
6MG	641 East Ave S		-118.15					1999	206 6,	000,000		vn 24	3	2.5		1.5 1.3	16 1.80	13.0	03	0.09	8.583 0.	.428	799900	49913745	6714999	9	255176	160865 255	176 0.77	3 571	51395	39739497	12 0.066	2640	32159	629	60628	1836 632	441	6 0.64 Tank		0.15 0.09	1.09 9.58	9.58	3	24349 6291.	
25th Street	26496 Cemetary Road	d 34.55	-118.09					1976	106 2,	000,000	Unknow	vn 30	3	2.5		1.5 1.3	16 1.80	6.7	4	0.29	3.533 1.	.039	264742	16519902	5375203	11	67564	104870 67	564 0.77	3 434	48840	10436273	16 0.209	2185	35431	486		2052 407	410	6 2.23 Provi		0.29 0.35		3 15.53	3	8304 4860.	.10557 OK
25til Street	20490 Cellietal y Road			elded No	t Flexible Ring	wall with Sand Interio	or	1967	154 4,	000,000	Unknow	vn 30	3	2.5		1.5 1.2	78 1.77	9.1	.3	0.18	5.133 0.	715	558795	34868813	7841520	11	142609	151052 142	509 0.762	2 631	71001	25267634	16 0.131	3318	51781	713	87878	2052 591	461	0 1.51 Uplift	ift but Stable	0.21 0.18	14.15	5 14.15	3	17380 7130.	
		34.54	-118.05					1988	200 0	000,000	Unknow		3	2.5		1.5 1.2	14 1.72						398197	24847485	6614006	11	101623	127961 101	523 0.731	8 512	57696	17074207	16 0.164	2809	44414	584	72811	2052 499	431	8 1.77 Provi	ide Anchors	0.23 0.23	1.23 14.95	14.95	3	12488 5845.	
45th Street	36510 45th St East							1990		000,000		m 32	3	2.5	III	1.5 1.2	1.72		_				565487	35286369	8687384	12	135297	157017 135		8 673	80769	24894926	17 0.137	3398	56992	754	98852	2120 614	47	7 1.74 Provi	ide Anchors	0.21 0.19	1.19 14.33	3 14.33	3	17687 7540.	
								1990		000,000	Unknov		3	2.5	III	1.5 1.2			_				565487	35286369	8687384	12	135297	157017 135	297 0.731	8 673	80769	24894926	17 0.137	3398	56992	754	98852	2120 614	47	7 1.74 Provi	ide Anchors	0.21 0.19	1.19 14.33	3 14.33	3	17687 7540.	
47th Street	35645 47th St East	34.53	-118.05					1967		000,000	Unknov		3	2.5	III	1.5 1.3	1.0.			0.00			264742	16519902	5375203	11	67564	104870 67	564 0.776	6 435	49003	10436273	16 0.211	2200	35674	488	60613	2052 407	416	6 2.24 Provi	ide Anchors	0.30 0.35	1.30 15.64	15.64	3	8301 4879.	
	***************************************							1990		000,000		vn 30	3	2.5	III	1.5 1.3			_				410543	25617904	6716566		104774	129885 104		6 547	61576	17698347	16 0.177	3126	49427	630	78960	2052 506	441	0 1.87 Provi		0.25 0.25	1.25 16.32	2 16.32	3	12801 6303.	
50th Street	5001 East Ave. T-8	34.54	-118.04							000,000		vn 30	3	2.5	III	1.5 1.3			_				530144	33080971	7637298			147203 135		8 610			16 0.135		50405			2052 576	450	6 1.55 Provi		0.21 0.19		2 14.22	3	16514 6902.	
	,			elded?		crete Ring Wall	None Shown	2007	150 4,	seejeee	Unknov		3	2.5	III	1.5 1.3			_				530144	33080971	7637298	11	135297	147203 135	297 0.751	8 610	68664	23796213	16 0.135	3223	50405	690	85178	2052 576	450	6 1.55 Provi	ide Anchors	0.21 0.19	1.19 14.22	2 14.22	3	16514 6902.	
Ana Verde	36800 Tovey Aveneu			elded No	t Flexible Con	crete Rink wall	Not Shown	1963		00,000	Unknov		3	2.5	III	1.5 1.2							40212	2509253	1825481	12	9621	44129 9	521 0.70	2 132	16240	717357	22 0.355	255	5658	135	17197	2120 163	385	9 5.44 Provi	ide Anchors	0.50 1.09	1.50 9.95	9.95	3		.04608 OK
El Camino Lower	36809 El Camino Dr.	34.55	-118.13					1988		000,000		vn 32	3	2.5	III	1.5 1.3	7 1.71	6.6	i3	0.29	3.313 1.	.108	282391	17621228	6103267	12	67564	111862 67	564 0.73	5 466	55977	10784811	17 0.205	2215	38666	516	68033	2120 434	43	7 2.42 Provi	ide Anchors	0.29 0.35	1.29 15.24	15.24	3	8916 5163.	.80732 OK
El Camino U.G ⁴	36336 El Camino Road	d						1994	104 1,	500,000	Unknov	vn 26																																			
El Camino Upper	33030 Ridge Route Rd	d 34.54	-118.13 W	elded I	Flexible Ring	wall with Sand Inte	None Shown	1963	40 3	00,000	Unknow	m 32	3	2.5	Ш	1.5 0.8	81 1.54	3.6	i6	0.36	1.250 2.	.936	40212	2509253	1825481	12	9621	44129 9	521 0.66	1 124	15289	717357	22 0.258	185	4106	126		2120 163	385	9 5.00 Provi	ide Anchors	0.36 0.79	1.36 7.22	7.22	3	1371 1262.	.69341 OK
Walt Dahlitz	115 East Avenue S		W	elded I	Flexible Con-	rete Ringwall, oil s	None Shown	1993	104 1,	500,000	Unknow	vn 31	3	2.5	Ш	1.5 0.8	27 1.44	6.5	i8	0.19	3.355 1.	.094	263341	16432470	5622265	12	65039	106378 658	0.61	8 362	42091	10122208	17 0.135	1362	22997	386		2086 412	42	5 1.80 Provi	ide Anchors	0.19 0.23	9.80	9.80	3	8455 3868.	
Well 14	36401 20th ST East		W	leled? No	t Flexible Con	crete Ringwall, grav	3/4" 5' OC 8" embed		27 1	00,000	Unknow	m 22	3	2.5	Ш	1.5 0.9	27 1.51	3.0	11	0.46	1.227 2.	.990	12596	786004	575712	8	4384	21166 4	384 0.649	9 39	3325	220749	15 0.330	73	1119	40		1758 76	27	5 4.80 Provi	ide Anchors	0.46 1.23	1.46 6.24	6.24	3	435 399.6	85968 OK
Well 18 and 19	4640 Barrel Springs Roa	ad						1963	22	1,000	Unknow	vn 30	3	2.5	Ш	1.5 1.3	23 1.8	2.7	1	0.73	0.733 5.	.005	11404	711608	597846	13	2910	24053 25	910 0.77	1 48	6262	120014	24 0.524	63	1513	48	6442	2052 84	36	9 11.47 Provi	ide Anchors	0.73 2.17	1.73 8.06	8.06	3		300415 Needs And
Well 5	1036 Barrel Spring Roa	ad						1963	30 1,	463,945	Unknow	m 22	3	2.5	Ш	1.5 1.3	11 1.78	3.1	.8	0.62	1.364 2.	.691	15551	970375	680168	8	5412	23283 54	112 0.76	4 54	4500	301560	15 0.442	133	1982	56	4918	1758 84	27	6 5.05 Provi	ide Anchors	0.62 1.56	1.62 9.29	9.29	3	526 561.	571023 Needs And
	response acceleration par trum for impulsive compo						,					,								ravity, g.																											

Facility list indicates that these facilities conatain 0 gallons and does not provide the overflow height, therefore we were not apple to determine the seismic demands on these structures.
 A.WWA D100 calculations do not apply to the El Camino Underground tank. Construction drawings are not available to perform an analysis at this time.
 Minimum required freeboard is equal to the sloshing wave height for Use Group III and may be reduced for Use Group I and III.



Coordinates: 34.557353817153206, -118.11224470422972

Elevation: 2750 ft

Timestamp: 2021-04-09T16:22:17.704Z

Hazard Type: Seismic

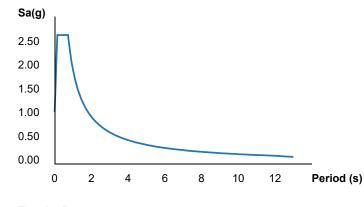
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

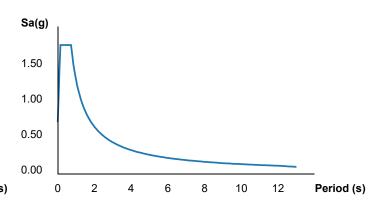
MCER Horizontal Response Spectrum





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Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.707	MCE _R ground motion (period=0.2s)
S ₁	1.315	MCE _R ground motion (period=1.0s)
S _{MS}	2.707	Site-modified spectral acceleration value
S _{M1}	1.973	Site-modified spectral acceleration value
S _{DS}	1.805	Numeric seismic design value at 0.2s SA
S _{D1}	1.315	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.919	Coefficient of risk (0.2s)
CR ₁	0.903	Coefficient of risk (1.0s)

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PGA	1.045	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.045	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.418	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.719	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.707	Factored deterministic acceleration value (0.2s)
S1RT	1.605	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.778	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.315	Factored deterministic acceleration value (1.0s)
PGAd	1.045	Factored deterministic acceleration value (PGA)

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34.53471326457233, -118.08343773439331 Coordinates:

Elevation: 2968 ft

Timestamp: 2021-04-09T16:35:02.162Z

Hazard Type: Seismic

Reference ASCE7-10

Document:

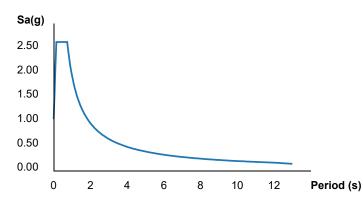
Risk Category: IV

Site Class: D

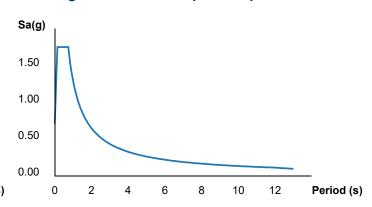
2968 ft Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S.

Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.646	MCE _R ground motion (period=0.2s)
S ₁	1.302	MCE _R ground motion (period=1.0s)
S _{MS}	2.646	Site-modified spectral acceleration value
S _{M1}	1.953	Site-modified spectral acceleration value
S _{DS}	1.764	Numeric seismic design value at 0.2s SA
S _{D1}	1.302	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.924	Coefficient of risk (0.2s)
CR ₁	0.904	Coefficient of risk (1.0s)

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PGA	1.018	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.018	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.282	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.552	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.646	Factored deterministic acceleration value (0.2s)
S1RT	1.53	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.694	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.302	Factored deterministic acceleration value (1.0s)
PGAd	1.018	Factored deterministic acceleration value (PGA)

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34547 Address:

Coordinates: 34.5497, -118.132821

Elevation: 2923 ft

2021-04-08T21:00:34.329Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

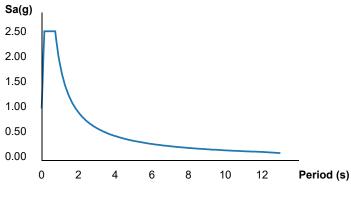
Document:

Risk Category: Ш

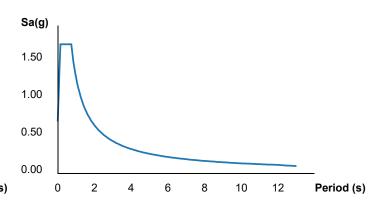
Site Class:

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MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.573	MCE _R ground motion (period=0.2s)
S ₁	1.271	MCE _R ground motion (period=1.0s)
S _{MS}	2.573	Site-modified spectral acceleration value
S _{M1}	1.906	Site-modified spectral acceleration value
S _{DS}	1.715	Numeric seismic design value at 0.2s SA
S _{D1}	1.271	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.916	Coefficient of risk (0.2s)

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CR ₁	0.904	Coefficient of risk (1.0s)
PGA	0.987	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.987	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.429	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.743	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.573	Factored deterministic acceleration value (0.2s)
S1RT	1.614	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.785	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.271	Factored deterministic acceleration value (1.0s)
PGAd	0.987	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.559419345037064, -118.11618400870667

Elevation: 2750 ft

Timestamp: 2021-04-09T16:36:57.402Z

Hazard Type: Seismic

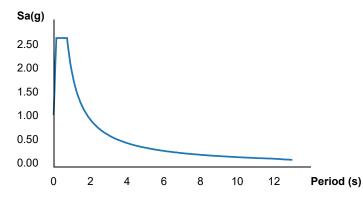
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

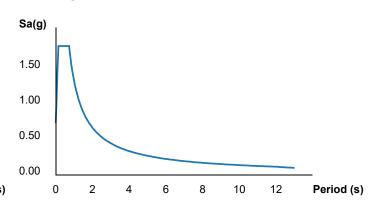
MCER Horizontal Response Spectrum





ivan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.706	MCE _R ground motion (period=0.2s)
S ₁	1.316	MCE _R ground motion (period=1.0s)
S _{MS}	2.706	Site-modified spectral acceleration value
S _{M1}	1.975	Site-modified spectral acceleration value
S _{DS}	1.804	Numeric seismic design value at 0.2s SA
S _{D1}	1.316	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.92	Coefficient of risk (0.2s)
CR ₁	0.903	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:37 AM

PGA	1.046	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.046	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.37	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.665	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.706	Factored deterministic acceleration value (0.2s)
S1RT	1.58	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.749	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.316	Factored deterministic acceleration value (1.0s)
PGAd	1.046	Factored deterministic acceleration value (PGA)

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Coordinates: 34.55371, -118.087856

Elevation: 2752 ft

Timestamp: 2021-04-09T16:19:01.173Z

Hazard Type: Seismic

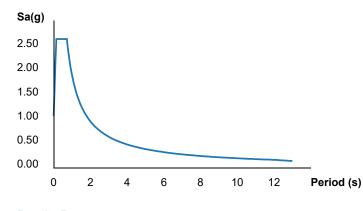
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

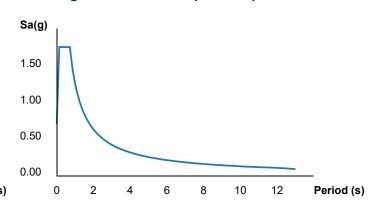
MCER Horizontal Response Spectrum



Ave 2752 ft 27

Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.668	MCE _R ground motion (period=0.2s)
S ₁	1.278	MCE _R ground motion (period=1.0s)
S _{MS}	2.668	Site-modified spectral acceleration value
S _{M1}	1.917	Site-modified spectral acceleration value
S _{DS}	1.779	Numeric seismic design value at 0.2s SA
S _{D1}	1.278	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.919	Coefficient of risk (0.2s)
CR ₁	0.902	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:19 AM

PGA	1.031	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.031	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.432	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.737	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.668	Factored deterministic acceleration value (0.2s)
S1RT	1.613	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.788	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.278	Factored deterministic acceleration value (1.0s)
PGAd	1.031	Factored deterministic acceleration value (PGA)

Disclaimer

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Coordinates: 34.55371, -118.087856

Elevation: 2752 ft

Timestamp: 2021-04-09T16:17:53.781Z

Hazard Type: Seismic

Reference ASCE7-16

Document:

Risk Category: IV

Site Class: D-default



Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Basic Parameters

Name	Value	Description
S _S	2.404	MCE _R ground motion (period=0.2s)
S ₁	1.025	MCE _R ground motion (period=1.0s)
S _{MS}	2.885	Site-modified spectral acceleration value
S _{M1}	* null	Site-modified spectral acceleration value
S _{DS}	1.923	Numeric seismic design value at 0.2s SA
S _{D1}	* null	Numeric seismic design value at 1.0s SA

^{*} See Section 11.4.8

▼Additional Information

Name	Value	Description
SDC	* null	Seismic design category
Fa	1.2	Site amplification factor at 0.2s
F _v	* null	Site amplification factor at 1.0s
CRS	0.874	Coefficient of risk (0.2s)
CR ₁	0.869	Coefficient of risk (1.0s)
PGA	1.033	MCE _G peak ground acceleration
F _{PGA}	1.2	Site amplification factor at PGA
PGA _M	1.24	Site modified peak ground acceleration

1 of 2 4/9/2021, 10:18 AM

TL	12	Long-period transition period (s)
SsRT	3.008	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.441	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.404	Factored deterministic acceleration value (0.2s)
S1RT	1.294	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.489	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.025	Factored deterministic acceleration value (1.0s)
PGAd	1.033	Factored deterministic acceleration value (PGA)

^{*} See Section 11.4.8

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Search Information

Coordinates: 34.544961034712664, -118.04877924893493

Elevation: 2740 ft

Timestamp: 2021-04-09T16:27:34.922Z

Hazard Type: Seismic

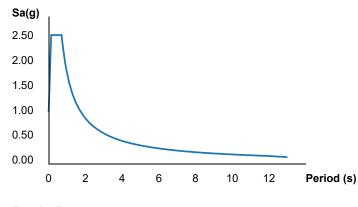
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

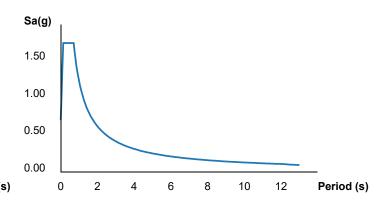
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.584	MCE _R ground motion (period=0.2s)
S ₁	1.214	MCE _R ground motion (period=1.0s)
S _{MS}	2.584	Site-modified spectral acceleration value
S _{M1}	1.821	Site-modified spectral acceleration value
S _{DS}	1.723	Numeric seismic design value at 0.2s SA
S _{D1}	1.214	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.921	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:27 AM

PGA	0.996	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.996	Site modified peak ground acceleration
T_L	12	Long-period transition period (s)
SsRT	3.159	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.432	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.584	Factored deterministic acceleration value (0.2s)
S1RT	1.47	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.624	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.214	Factored deterministic acceleration value (1.0s)
PGAd	0.996	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.52903336279662, -118.04584351481934

Elevation: 2971 ft

Timestamp: 2021-04-09T16:31:06.633Z

Hazard Type: Seismic

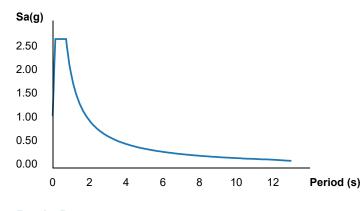
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

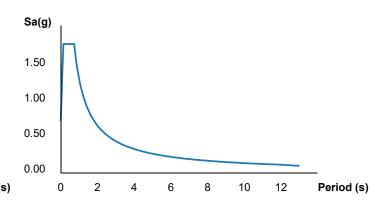
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.714	MCE _R ground motion (period=0.2s)
S ₁	1.325	MCE _R ground motion (period=1.0s)
S _{MS}	2.714	Site-modified spectral acceleration value
S _{M1}	1.987	Site-modified spectral acceleration value
S _{DS}	1.81	Numeric seismic design value at 0.2s SA
S _{D1}	1.325	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.923	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:31 AM

PGA	1.048	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.048	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.142	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.404	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.714	Factored deterministic acceleration value (0.2s)
S1RT	1.461	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.614	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.325	Factored deterministic acceleration value (1.0s)
PGAd	1.048	Factored deterministic acceleration value (PGA)

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Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S.

8

10

12

Period (s)

Geological Survey, USDA Farm Service Agency

ATC Hazards by Location

Search Information

Coordinates: 34.536316858195896, -118.04017088147585

8

10

Elevation: 2825 ft

Timestamp: 2021-04-09T16:33:04.897Z

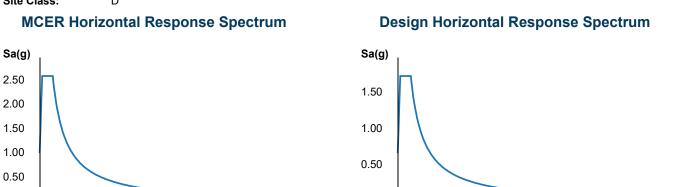
Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D



0.00

0

2

Period (s)

Basic Parameters

0.00

0

Name	Value	Description
S _S	2.652	MCE _R ground motion (period=0.2s)
S ₁	1.26	MCE _R ground motion (period=1.0s)
S _{MS}	2.652	Site-modified spectral acceleration value
S _{M1}	1.889	Site-modified spectral acceleration value
S _{DS}	1.768	Numeric seismic design value at 0.2s SA
S _{D1}	1.26	Numeric seismic design value at 1.0s SA

12

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.923	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:33 AM

PGA	1.024	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.024	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.121	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.381	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.652	Factored deterministic acceleration value (0.2s)
S1RT	1.449	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.602	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.26	Factored deterministic acceleration value (1.0s)
PGAd	1.024	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.54972773620536, -118.1502535834671

Elevation: 3116 ft

Timestamp: 2021-04-09T16:41:41.594Z

Hazard Type: Seismic

Reference ASCE7-10

Document:

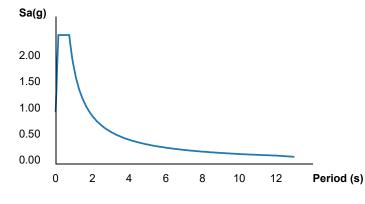
Risk Category: IV

Site Class: D

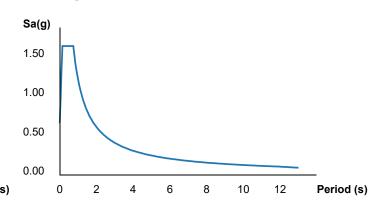
3116 ft & Accienda Dr. Wan data @2021 Imagery @2021 Maxar Technologies, U.S. Geological Surve

wan data ©2021 Imagery ©2021 , Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



MCER Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.458	MCE _R ground motion (period=0.2s)
S ₁	1.214	MCE _R ground motion (period=1.0s)
S _{MS}	2.458	Site-modified spectral acceleration value
S _{M1}	1.82	Site-modified spectral acceleration value
S _{DS}	1.639	Numeric seismic design value at 0.2s SA
S _{D1}	1.214	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.916	Coefficient of risk (0.2s)
CR ₁	0.906	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:41 AM

PGA	0.945	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.945	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.335	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.642	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.458	Factored deterministic acceleration value (0.2s)
S1RT	1.566	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.728	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.214	Factored deterministic acceleration value (1.0s)
PGAd	0.945	Factored deterministic acceleration value (PGA)

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Search Information

36809 El Camino Dr, Palmdale, CA 93551, USA Address:

34.54952240000001, -118.1326806 Coordinates:

Elevation: 2925 ft

2021-04-09T16:20:57.078Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: IV

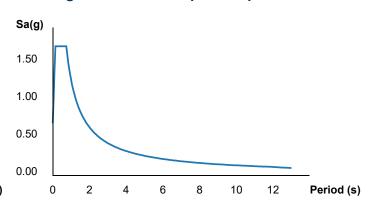
Site Class:

2925 ft wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum

Sa(g) 2.50 2.00 1.50 1.00 0.50 0.00 0 10 12 Period (s)

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.571	MCE _R ground motion (period=0.2s)
S ₁	1.27	MCE _R ground motion (period=1.0s)
S _{MS}	2.571	Site-modified spectral acceleration value
S _{M1}	1.905	Site-modified spectral acceleration value
S _{DS}	1.714	Numeric seismic design value at 0.2s SA
S _{D1}	1.27	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.916	Coefficient of risk (0.2s)

1 of 2 4/9/2021, 10:21 AM

CR ₁	0.904	Coefficient of risk (1.0s)
PGA	0.986	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.986	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.426	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.74	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.571	Factored deterministic acceleration value (0.2s)
S1RT	1.613	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.783	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.27	Factored deterministic acceleration value (1.0s)
PGAd	0.986	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.53840630847815, -118.13288506137695

Elevation: 3359 ft

Timestamp: 2021-04-09T20:04:43.993Z

Hazard Type: Seismic

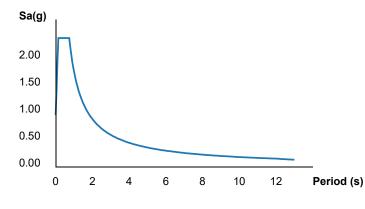
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

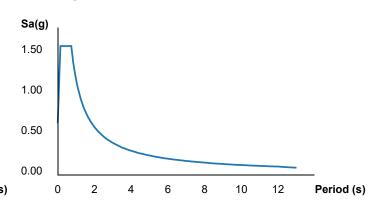
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.375	MCE _R ground motion (period=0.2s)
S ₁	1.171	MCE _R ground motion (period=1.0s)
S _{MS}	2.375	Site-modified spectral acceleration value
S _{M1}	1.756	Site-modified spectral acceleration value
S _{DS}	1.583	Numeric seismic design value at 0.2s SA
S _{D1}	1.171	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.925	Coefficient of risk (0.2s)
CR ₁	0.908	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 2:04 PM

PGA	0.917	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.917	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.236	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.499	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.375	Factored deterministic acceleration value (0.2s)
S1RT	1.505	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.657	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.171	Factored deterministic acceleration value (1.0s)
PGAd	0.917	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:04 PM



Search Information

34.56128566737895, -118.12898168848265 Coordinates:

Elevation: 2924 ft

Timestamp: 2021-04-09T20:40:24.218Z

Hazard Type: Seismic

ASCE7-10 Reference

Document:

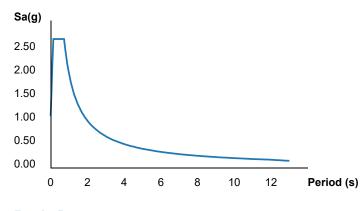
Risk Category: IV

Site Class: D

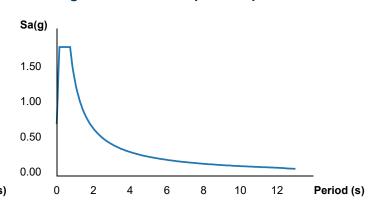
2924 ft Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S.

Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.733	MCE _R ground motion (period=0.2s)
S ₁	1.331	MCE _R ground motion (period=1.0s)
S _{MS}	2.733	Site-modified spectral acceleration value
S _{M1}	1.997	Site-modified spectral acceleration value
S _{DS}	1.822	Numeric seismic design value at 0.2s SA
S _{D1}	1.331	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.92	Coefficient of risk (0.2s)
CR ₁	0.904	Coefficient of risk (1.0s)

4/9/2021, 2:40 PM 1 of 2

PGA	1.055	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.055	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.306	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.594	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.733	Factored deterministic acceleration value (0.2s)
S1RT	1.547	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.71	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.331	Factored deterministic acceleration value (1.0s)
PGAd	1.055	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:40 PM

Search Information

34547 Address:

34.538438, -118.132863 Coordinates:

Elevation: 3360 ft

2021-04-08T22:06:10.243Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: Ш

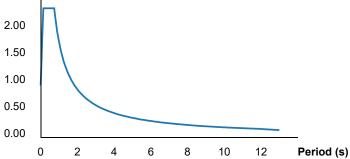
Site Class:

3360 ft

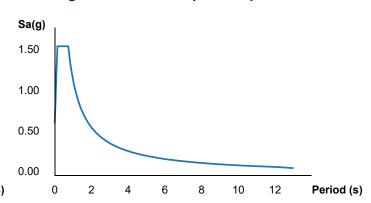
wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum

Sa(g)



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.376	MCE _R ground motion (period=0.2s)
S ₁	1.171	MCE _R ground motion (period=1.0s)
S _{MS}	2.376	Site-modified spectral acceleration value
S _{M1}	1.757	Site-modified spectral acceleration value
S _{DS}	1.584	Numeric seismic design value at 0.2s SA
S _{D1}	1.171	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.925	Coefficient of risk (0.2s)

4/8/2021, 4:06 PM 1 of 2

CR ₁	0.908	Coefficient of risk (1.0s)
PGA	0.917	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.917	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.236	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.5	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.376	Factored deterministic acceleration value (0.2s)
S1RT	1.505	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.657	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.171	Factored deterministic acceleration value (1.0s)
PGAd	0.917	Factored deterministic acceleration value (PGA)

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2 of 2 4/8/2021, 4:06 PM

Search Information

Coordinates: 34.598759799594845, -118.09844223112182

Elevation: 2583 ft

Timestamp: 2021-04-09T20:48:48.917Z

Hazard Type: Seismic

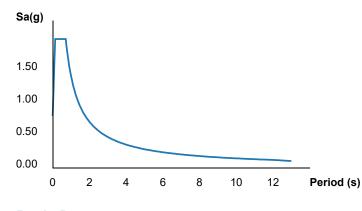
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

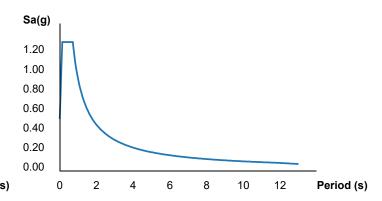
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	1.971	MCE _R ground motion (period=0.2s)
S ₁	0.937	MCE _R ground motion (period=1.0s)
S _{MS}	1.971	Site-modified spectral acceleration value
S _{M1}	1.406	Site-modified spectral acceleration value
S _{DS}	1.314	Numeric seismic design value at 0.2s SA
S _{D1}	0.937	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.937	Coefficient of risk (0.2s)
CR ₁	0.911	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 2:48 PM

PGA	0.77	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.77	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	2.602	Probabilistic risk-targeted ground motion (0.2s)
SsUH	2.776	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	1.971	Factored deterministic acceleration value (0.2s)
S1RT	1.168	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.282	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	0.937	Factored deterministic acceleration value (1.0s)
PGAd	0.77	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:48 PM

Search Information

Address: 1036 Barrel Spring Road palmdale, ca

Coordinates: 34.5457226, -118.1085956

Elevation: 2817 ft

Timestamp: 2021-05-04T20:11:47.998Z

Hazard Type: Seismic

Reference

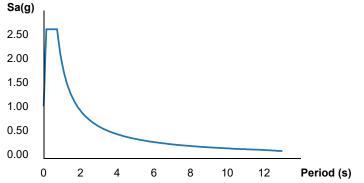
ASCE7-10

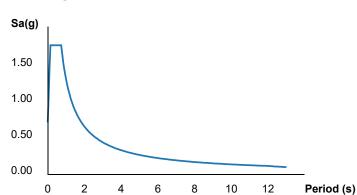
Document:

Risk Category:

Site Class: D

MCER Horizontal Response Spectrum Design Horizontal Response Spectrum





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E Barrel Springs Rd

Basic Parameters

Name	Value	Description
S _S	2.674	MCE _R ground motion (period=0.2s)
S ₁	1.311	MCE _R ground motion (period=1.0s)
S _{MS}	2.674	Site-modified spectral acceleration value
S _{M1}	1.967	Site-modified spectral acceleration value
S _{DS}	1.782	Numeric seismic design value at 0.2s SA
S _{D1}	1.311	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.919	Coefficient of risk (0.2s)

1 of 2 5/4/2021, 2:13 PM

CR ₁	0.902	Coefficient of risk (1.0s)
PGA	1.029	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.029	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.49	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.799	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.674	Factored deterministic acceleration value (0.2s)
S1RT	1.643	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.821	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.311	Factored deterministic acceleration value (1.0s)
PGAd	1.029	Factored deterministic acceleration value (PGA)

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2 of 2 5/4/2021, 2:13 PM

Search Information

Address: 15 4640 Barrel Spring Road palmdale, ca

Coordinates: 34.5268275, -118.0540864

Elevation: 3036 ft

Timestamp: 2021-05-04T20:14:23.952Z

Hazard Type: Seismic

Reference ASCE7-10

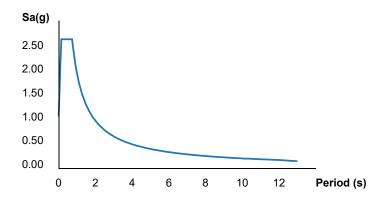
Document:

Risk Category:

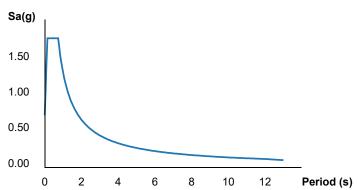
Site Class: D

3036 ft 3036 ft Religion Religion Ballely Common data © 2021 Imagery © 2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



MCER Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.7	MCE _R ground motion (period=0.2s)
S ₁	1.323	MCE _R ground motion (period=1.0s)
S _{MS}	2.7	Site-modified spectral acceleration value
S _{M1}	1.984	Site-modified spectral acceleration value
S _{DS}	1.8	Numeric seismic design value at 0.2s SA
S _{D1}	1.323	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.924	Coefficient of risk (0.2s)

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CR ₁	0.905	Coefficient of risk (1.0s)
PGA	1.04	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.04	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.149	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.409	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.7	Factored deterministic acceleration value (0.2s)
S1RT	1.464	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.617	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.323	Factored deterministic acceleration value (1.0s)
PGAd	1.04	Factored deterministic acceleration value (PGA)

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2 of 2 5/4/2021, 2:14 PM

												Ĭ																AWWA	D100-11 Welded O	Carbon Steel Tan	s Chapter 13 Seism	nic Design															
		Coord	dinates				T:	ank Details						Table 28	13.2.1	Table 24 AT	1 Eqn 13	9 ^{1,2} Eqn 1	3-22 E	qn 13-12/13 ²			13	3-27 1	3-25/26 Eqn 13-	28/29 Estimat	ate Estima	ate Estimate	Eqn 13-16		Eqn 13-24/25	Eqn 13-3)		Eqn 13-26	Eqn 13-31	Eqn 13-23	Eqn 13-37	Eqn 13-41	Eqn 13-36		Eqn 13-53/54	Eqn 13-52	Table 29	Equ	qn 13-57	
Tank Site	Address	Latitude	Longitude Tar	ık Type Co	Piping Foot nnection	ing	Anchorage	Date Built	Dia	Size Botton Knu		Overflow e Height	Freeboard Assumed to be 3 feet unless drawings indicate otherwise	Ri 3 if anchored 5 if unanchored		, assume that all Sels anks are ismic Use Ma Group III	nic Based on S	ts from		Sac, g ed on Sd1 from ASCE 7-10	D/H 3.67	7*D/H Vol =	olume ft ² : π*(Dia^2)/4	Total Weight, Ibf W = V Vol*62.4pcf	Impulsive latera	Sloshing Roof (ht of the Weig (Wr), lbf Shell	ght of the Weight of t (Ws), lbf Floor (Wf),	Implusive he Design lbf Acceleration (Al)	Impulsive Lateral Force (VI), kip	Overturning Moment due to Impulsive Lateral 1 Force(Mi), ft- kip	Convective Weight (Wc), lbf mass (X ft	al Convective to Design we Acceleration	Convective Lateral Force (Vc), kip	Overturning Moment due to Convective Lateral Force(Mc), ft- kip	Design Latera Force at the top of the foundation (Vf), kip		Maximum Resting Weigh of the Tank Contents (wt.) Ibf/ft	Weight of the Tank Shell and Roof Resisting Overturning (wt), lbf/ft		Anchor equirements	Convective Design Accelaration, Af	Sloshing Wave Height (d), ft	Required F Freeboard (D), (I	ctual Ai reeboard Roof Height- Lo lverflow)	Allowable Late Lateral Seis Load, Valow Load	otal teral ismic Sliding id, Vt (ip)
3 MG Tank Site	850 East Avenue S		-118.11 W	elded				1960	124 3,	000,000	Unknov	m 34	3	2.5	ш	1.5 1.3	15 1.80		-	0.27	3.647 1.	.006	410594	25621040	8082906	13	92459	138480 924	159 0.774	4 650	82912	16424329	18 0.192	3150	57649	722	100984	2185 539	474	4 2.54 Provi	ide Anchors	0.27 0.29	1.27 16.65	16.65	3	12851 7225.	.51729 OK
5 MG Tank	2404 Old Nadeau Road	ad 34.53	-118.08						160 5,	000,000	Unknov	vn 20	3	2.5	III .	1.5 1.3	02 1.76	11.1	13	0.13	8.000 0.	459	402124	25092529	3621894	8	153938	104550 153	938 0.756	6 305	22875	19810034	10 0.090	1784	18144	353	29197	1676 409	36:	1 0.57 Tank	k Is Stable	0.18 0.13	10.08	10.08	3	12338 35?	13.2461 OK
6MG	641 East Ave S		-118.15					1999	206 6,	000,000		vn 24	3	2.5		1.5 1.3	16 1.80	13.0	03	0.09	8.583 0.	.428	799900	49913745	6714999	9	255176	160865 255	176 0.77	3 571	51395	39739497	12 0.066	2640	32159	629	60628	1836 632	441	6 0.64 Tank		0.15 0.09	1.09 9.58	9.58	3	24349 6291.	
25th Street	26496 Cemetary Road	d 34.55	-118.09					1976	106 2,	000,000	Unknow	vn 30	3	2.5		1.5 1.3	16 1.80	6.7	4	0.29	3.533 1.	.039	264742	16519902	5375203	11	67564	104870 67	564 0.77	3 434	48840	10436273	16 0.209	2185	35431	486		2052 407	410	6 2.23 Provi		0.29 0.35		3 15.53	3	8304 4860.	.10557 OK
25til Street	20490 Cellietal y Road			elded No	t Flexible Ring	wall with Sand Interio	or	1967	154 4,	000,000	Unknow	vn 30	3	2.5		1.5 1.2	78 1.77	9.1	.3	0.18	5.133 0.	715	558795	34868813	7841520	11	142609	151052 142	509 0.762	2 631	71001	25267634	16 0.131	3318	51781	713	87878	2052 591	461	0 1.51 Uplift	ift but Stable	0.21 0.18	14.15	5 14.15	3	17380 7130.	
		34.54	-118.05					1988	200 0	000,000	Unknow		3	2.5		1.5 1.2	14 1.72						398197	24847485	6614006	11	101623	127961 101	523 0.731	8 512	57696	17074207	16 0.164	2809	44414	584	72811	2052 499	431	8 1.77 Provi	ide Anchors	0.23 0.23	1.23 14.95	14.95	3	12488 5845.	
45th Street	36510 45th St East							1990		000,000		m 32	3	2.5	III	1.5 1.2	1.72		_				565487	35286369	8687384	12	135297	157017 135		8 673	80769	24894926	17 0.137	3398	56992	754	98852	2120 614	47	7 1.74 Provi	ide Anchors	0.21 0.19	1.19 14.33	3 14.33	3	17687 7540.	
								1990		000,000	Unknov		3	2.5	III	1.5 1.2			_				565487	35286369	8687384	12	135297	157017 135	297 0.731	8 673	80769	24894926	17 0.137	3398	56992	754	98852	2120 614	47	7 1.74 Provi	ide Anchors	0.21 0.19	1.19 14.33	3 14.33	3	17687 7540.	
47th Street	35645 47th St East	34.53	-118.05					1967		000,000	Unknov		3	2.5	III	1.5 1.3	1.0.			0.00			264742	16519902	5375203	11	67564	104870 67	564 0.776	6 435	49003	10436273	16 0.211	2200	35674	488	60613	2052 407	416	6 2.24 Provi	ide Anchors	0.30 0.35	1.30 15.64	15.64	3	8301 4879.	
	***************************************							1990		000,000		vn 30	3	2.5	III	1.5 1.3							410543	25617904	6716566		104774	129885 104		6 547	61576	17698347	16 0.177	3126	49427	630	78960	2052 506	441	0 1.87 Provi		0.25 0.25	1.25 16.32	2 16.32	3	12801 6303.	
50th Street	5001 East Ave. T-8	34.54	-118.04							000,000		vn 30	3	2.5	III	1.5 1.3			_				530144	33080971	7637298			147203 135		8 610			16 0.135		50405			2052 576	450	6 1.55 Provi		0.21 0.19		2 14.22	3	16514 6902.	
	,			elded?		crete Ring Wall	None Shown	2007	150 4,	seejeee	Unknov		3	2.5	III	1.5 1.3			_				530144	33080971	7637298	11	135297	147203 135	297 0.751	8 610	68664	23796213	16 0.135	3223	50405	690	85178	2052 576	450	6 1.55 Provi	ide Anchors	0.21 0.19	1.19 14.22	2 14.22	3	16514 6902.	
Ana Verde	36800 Tovey Aveneu			elded No	t Flexible Con	crete Rink wall	Not Shown	1963		00,000	Unknov		3	2.5	III	1.5 1.2							40212	2509253	1825481	12	9621	44129 9	521 0.70	2 132	16240	717357	22 0.355	255	5658	135	17197	2120 163	385	9 5.44 Provi	ide Anchors	0.50 1.09	1.50 9.95	9.95	3		.04608 OK
El Camino Lower	36809 El Camino Dr.	34.55	-118.13					1988		000,000		vn 32	3	2.5	III	1.5 1.3	7 1.71	6.6	i3	0.29	3.313 1.	.108	282391	17621228	6103267	12	67564	111862 67	564 0.73	5 466	55977	10784811	17 0.205	2215	38666	516	68033	2120 434	43	7 2.42 Provi	ide Anchors	0.29 0.35	1.29 15.24	15.24	3	8916 5163.	.80732 OK
El Camino U.G ⁴	36336 El Camino Road	d						1994	104 1,	500,000	Unknov	vn 26																																			
El Camino Upper	33030 Ridge Route Rd	d 34.54	-118.13 W	elded I	Flexible Ring	wall with Sand Inte	None Shown	1963	40 3	00,000	Unknow	m 32	3	2.5	Ш	1.5 0.8	81 1.54	3.6	i6	0.36	1.250 2.	.936	40212	2509253	1825481	12	9621	44129 9	521 0.66	1 124	15289	717357	22 0.258	185	4106	126		2120 163	385	9 5.00 Provi	ide Anchors	0.36 0.79	1.36 7.22	7.22	3	1371 1262.	.69341 OK
Walt Dahlitz	115 East Avenue S		W	elded I	Flexible Con-	rete Ringwall, oil s	None Shown	1993	104 1,	500,000	Unknow	vn 31	3	2.5	Ш	1.5 0.8	27 1.44	6.5	i8	0.19	3.355 1.	.094	263341	16432470	5622265	12	65039	106378 658	0.61	8 362	42091	10122208	17 0.135	1362	22997	386		2086 412	42	5 1.80 Provi	ide Anchors	0.19 0.23	1.19 9.80	9.80	3	8455 3868.	
Well 14	36401 20th ST East		W	leled? No	t Flexible Con	crete Ringwall, grav	3/4" 5' OC 8" embed		27 1	00,000	Unknow	m 22	3	2.5	Ш	1.5 0.9	27 1.51	3.0	11	0.46	1.227 2.	.990	12596	786004	575712	8	4384	21166 4	384 0.649	9 39	3325	220749	15 0.330	73	1119	40		1758 76	27	5 4.80 Provi	ide Anchors	0.46 1.23	1.46 6.24	6.24	3	435 399.6	85968 OK
Well 18 and 19	4640 Barrel Springs Roa	ad						1963	22	1,000	Unknow	vn 30	3	2.5	Ш	1.5 1.3	23 1.8	2.7	1	0.73	0.733 5.	.005	11404	711608	597846	13	2910	24053 25	910 0.77	1 48	6262	120014	24 0.524	63	1513	48	6442	2052 84	36	9 11.47 Provi	ide Anchors	0.73 2.17	1.73 8.06	8.06	3		300415 Needs And
Well 5	1036 Barrel Spring Roa	ad						1963	30 1,	463,945	Unknow	m 22	3	2.5	Ш	1.5 1.3	11 1.78	3.1	.8	0.62	1.364 2.	.691	15551	970375	680168	8	5412	23283 54	112 0.76	4 54	4500	301560	15 0.442	133	1982	56	4918	1758 84	27	6 5.05 Provi	ide Anchors	0.62 1.56	1.62 9.29	9.29	3	526 561.	571023 Needs And
	response acceleration par trum for impulsive compo						,					,								ravity, g.																											

Facility list indicates that these facilities conatain 0 gallons and does not provide the overflow height, therefore we were not apple to determine the seismic demands on these structures.
 A.WWA D100 calculations do not apply to the El Camino Underground tank. Construction drawings are not available to perform an analysis at this time.
 Minimum required freeboard is equal to the sloshing wave height for Use Group III and may be reduced for Use Group I and III.



Search Information

Coordinates: 34.557353817153206, -118.11224470422972

Elevation: 2750 ft

Timestamp: 2021-04-09T16:22:17.704Z

Hazard Type: Seismic

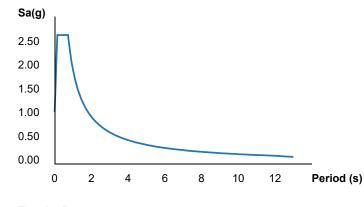
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

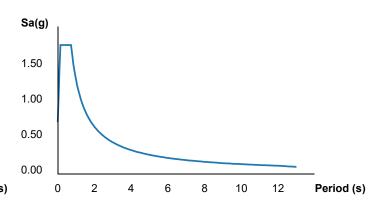
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.707	MCE _R ground motion (period=0.2s)
S ₁	1.315	MCE _R ground motion (period=1.0s)
S _{MS}	2.707	Site-modified spectral acceleration value
S _{M1}	1.973	Site-modified spectral acceleration value
S _{DS}	1.805	Numeric seismic design value at 0.2s SA
S _{D1}	1.315	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.919	Coefficient of risk (0.2s)
CR ₁	0.903	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:22 AM

PGA	1.045	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.045	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.418	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.719	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.707	Factored deterministic acceleration value (0.2s)
S1RT	1.605	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.778	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.315	Factored deterministic acceleration value (1.0s)
PGAd	1.045	Factored deterministic acceleration value (PGA)

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Search Information

34.53471326457233, -118.08343773439331 Coordinates:

Elevation: 2968 ft

Timestamp: 2021-04-09T16:35:02.162Z

Hazard Type: Seismic

Reference ASCE7-10

Document:

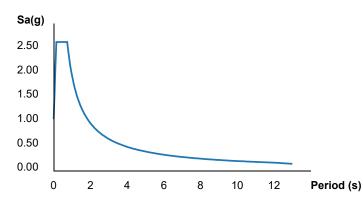
Risk Category: IV

Site Class: D

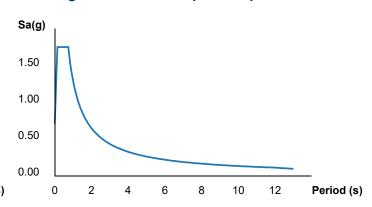
2968 ft Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S.

Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.646	MCE _R ground motion (period=0.2s)
S ₁	1.302	MCE _R ground motion (period=1.0s)
S _{MS}	2.646	Site-modified spectral acceleration value
S _{M1}	1.953	Site-modified spectral acceleration value
S _{DS}	1.764	Numeric seismic design value at 0.2s SA
S _{D1}	1.302	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.924	Coefficient of risk (0.2s)
CR ₁	0.904	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:35 AM

PGA	1.018	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.018	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.282	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.552	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.646	Factored deterministic acceleration value (0.2s)
S1RT	1.53	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.694	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.302	Factored deterministic acceleration value (1.0s)
PGAd	1.018	Factored deterministic acceleration value (PGA)

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Search Information

34547 Address:

Coordinates: 34.5497, -118.132821

Elevation: 2923 ft

2021-04-08T21:00:34.329Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

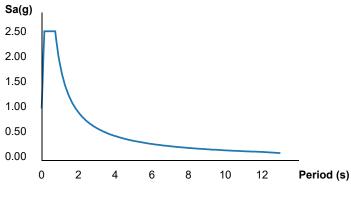
Document:

Risk Category: Ш

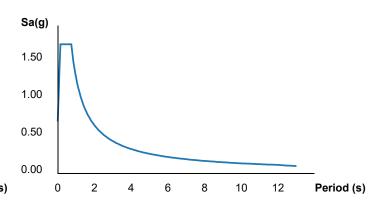
Site Class:

wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.573	MCE _R ground motion (period=0.2s)
S ₁	1.271	MCE _R ground motion (period=1.0s)
S _{MS}	2.573	Site-modified spectral acceleration value
S _{M1}	1.906	Site-modified spectral acceleration value
S _{DS}	1.715	Numeric seismic design value at 0.2s SA
S _{D1}	1.271	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.916	Coefficient of risk (0.2s)

4/8/2021, 3:01 PM 1 of 2

CR ₁	0.904	Coefficient of risk (1.0s)
PGA	0.987	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.987	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.429	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.743	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.573	Factored deterministic acceleration value (0.2s)
S1RT	1.614	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.785	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.271	Factored deterministic acceleration value (1.0s)
PGAd	0.987	Factored deterministic acceleration value (PGA)

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2 of 2 4/8/2021, 3:01 PM

Search Information

Coordinates: 34.559419345037064, -118.11618400870667

Elevation: 2750 ft

Timestamp: 2021-04-09T16:36:57.402Z

Hazard Type: Seismic

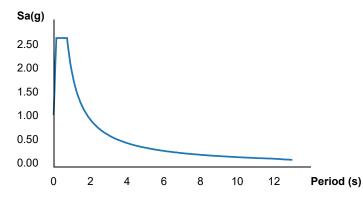
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

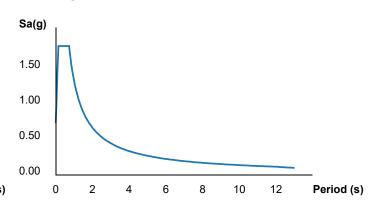
MCER Horizontal Response Spectrum





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Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.706	MCE _R ground motion (period=0.2s)
S ₁	1.316	MCE _R ground motion (period=1.0s)
S _{MS}	2.706	Site-modified spectral acceleration value
S _{M1}	1.975	Site-modified spectral acceleration value
S _{DS}	1.804	Numeric seismic design value at 0.2s SA
S _{D1}	1.316	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.92	Coefficient of risk (0.2s)
CR ₁	0.903	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:37 AM

PGA	1.046	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.046	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.37	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.665	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.706	Factored deterministic acceleration value (0.2s)
S1RT	1.58	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.749	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.316	Factored deterministic acceleration value (1.0s)
PGAd	1.046	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.55371, -118.087856

Elevation: 2752 ft

Timestamp: 2021-04-09T16:19:01.173Z

Hazard Type: Seismic

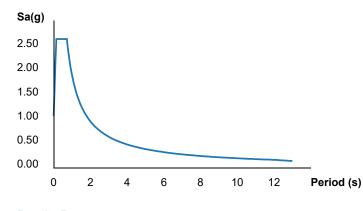
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

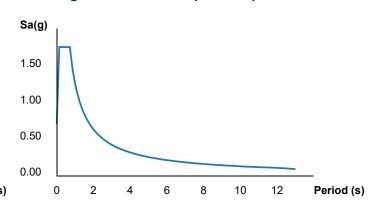
MCER Horizontal Response Spectrum



Ave 2752 ft 27

Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.668	MCE _R ground motion (period=0.2s)
S ₁	1.278	MCE _R ground motion (period=1.0s)
S _{MS}	2.668	Site-modified spectral acceleration value
S _{M1}	1.917	Site-modified spectral acceleration value
S _{DS}	1.779	Numeric seismic design value at 0.2s SA
S _{D1}	1.278	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.919	Coefficient of risk (0.2s)
CR ₁	0.902	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:19 AM

PGA	1.031	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.031	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.432	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.737	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.668	Factored deterministic acceleration value (0.2s)
S1RT	1.613	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.788	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.278	Factored deterministic acceleration value (1.0s)
PGAd	1.031	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.55371, -118.087856

Elevation: 2752 ft

Timestamp: 2021-04-09T16:17:53.781Z

Hazard Type: Seismic

Reference ASCE7-16

Document:

Risk Category: IV

Site Class: D-default



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Basic Parameters

Name	Value	Description
S _S	2.404	MCE _R ground motion (period=0.2s)
S ₁	1.025	MCE _R ground motion (period=1.0s)
S _{MS}	2.885	Site-modified spectral acceleration value
S _{M1}	* null	Site-modified spectral acceleration value
S _{DS}	1.923	Numeric seismic design value at 0.2s SA
S _{D1}	* null	Numeric seismic design value at 1.0s SA

^{*} See Section 11.4.8

▼Additional Information

Name	Value	Description
SDC	* null	Seismic design category
Fa	1.2	Site amplification factor at 0.2s
F _v	* null	Site amplification factor at 1.0s
CRS	0.874	Coefficient of risk (0.2s)
CR ₁	0.869	Coefficient of risk (1.0s)
PGA	1.033	MCE _G peak ground acceleration
F _{PGA}	1.2	Site amplification factor at PGA
PGA _M	1.24	Site modified peak ground acceleration

1 of 2 4/9/2021, 10:18 AM

TL	12	Long-period transition period (s)
SsRT	3.008	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.441	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.404	Factored deterministic acceleration value (0.2s)
S1RT	1.294	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.489	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.025	Factored deterministic acceleration value (1.0s)
PGAd	1.033	Factored deterministic acceleration value (PGA)

^{*} See Section 11.4.8

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Search Information

Coordinates: 34.544961034712664, -118.04877924893493

Elevation: 2740 ft

Timestamp: 2021-04-09T16:27:34.922Z

Hazard Type: Seismic

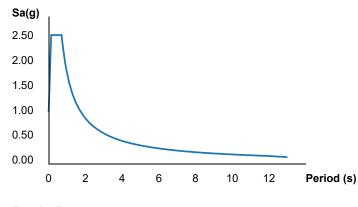
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

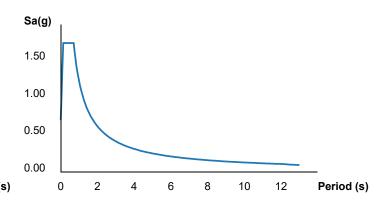
MCER Horizontal Response Spectrum





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Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.584	MCE _R ground motion (period=0.2s)
S ₁	1.214	MCE _R ground motion (period=1.0s)
S _{MS}	2.584	Site-modified spectral acceleration value
S _{M1}	1.821	Site-modified spectral acceleration value
S _{DS}	1.723	Numeric seismic design value at 0.2s SA
S _{D1}	1.214	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.921	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:27 AM

PGA	0.996	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.996	Site modified peak ground acceleration
T_L	12	Long-period transition period (s)
SsRT	3.159	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.432	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.584	Factored deterministic acceleration value (0.2s)
S1RT	1.47	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.624	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.214	Factored deterministic acceleration value (1.0s)
PGAd	0.996	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.52903336279662, -118.04584351481934

Elevation: 2971 ft

Timestamp: 2021-04-09T16:31:06.633Z

Hazard Type: Seismic

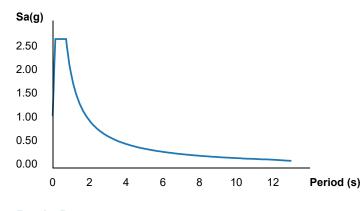
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

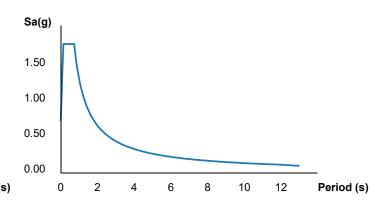
MCER Horizontal Response Spectrum





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Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.714	MCE _R ground motion (period=0.2s)
S ₁	1.325	MCE _R ground motion (period=1.0s)
S _{MS}	2.714	Site-modified spectral acceleration value
S _{M1}	1.987	Site-modified spectral acceleration value
S _{DS}	1.81	Numeric seismic design value at 0.2s SA
S _{D1}	1.325	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.923	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:31 AM

PGA	1.048	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.048	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.142	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.404	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.714	Factored deterministic acceleration value (0.2s)
S1RT	1.461	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.614	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.325	Factored deterministic acceleration value (1.0s)
PGAd	1.048	Factored deterministic acceleration value (PGA)

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8

10

12

Period (s)

Geological Survey, USDA Farm Service Agency

ATC Hazards by Location

Search Information

Coordinates: 34.536316858195896, -118.04017088147585

8

10

Elevation: 2825 ft

Timestamp: 2021-04-09T16:33:04.897Z

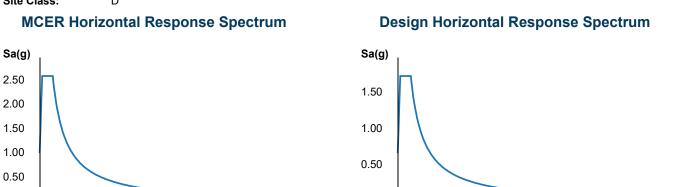
Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D



0.00

0

2

Period (s)

Basic Parameters

0.00

0

Name	Value	Description
S _S	2.652	MCE _R ground motion (period=0.2s)
S ₁	1.26	MCE _R ground motion (period=1.0s)
S _{MS}	2.652	Site-modified spectral acceleration value
S _{M1}	1.889	Site-modified spectral acceleration value
S _{DS}	1.768	Numeric seismic design value at 0.2s SA
S _{D1}	1.26	Numeric seismic design value at 1.0s SA

12

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.923	Coefficient of risk (0.2s)
CR ₁	0.905	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:33 AM

PGA	1.024	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.024	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.121	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.381	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.652	Factored deterministic acceleration value (0.2s)
S1RT	1.449	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.602	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.26	Factored deterministic acceleration value (1.0s)
PGAd	1.024	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.54972773620536, -118.1502535834671

Elevation: 3116 ft

Timestamp: 2021-04-09T16:41:41.594Z

Hazard Type: Seismic

Reference ASCE7-10

Document:

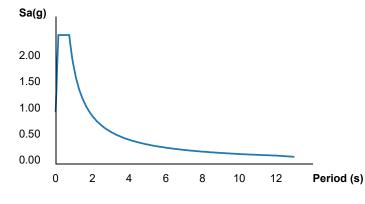
Risk Category: IV

Site Class: D

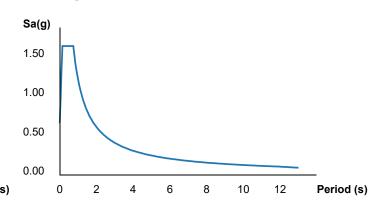
3116 ft & Accienda Dr. Wan data @2021 Imagery @2021 Maxar Technologies, U.S. Geological Surve

wan data ©2021 Imagery ©2021 , Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



MCER Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.458	MCE _R ground motion (period=0.2s)
S ₁	1.214	MCE _R ground motion (period=1.0s)
S _{MS}	2.458	Site-modified spectral acceleration value
S _{M1}	1.82	Site-modified spectral acceleration value
S _{DS}	1.639	Numeric seismic design value at 0.2s SA
S _{D1}	1.214	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.916	Coefficient of risk (0.2s)
CR ₁	0.906	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 10:41 AM

PGA	0.945	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.945	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.335	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.642	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.458	Factored deterministic acceleration value (0.2s)
S1RT	1.566	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.728	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.214	Factored deterministic acceleration value (1.0s)
PGAd	0.945	Factored deterministic acceleration value (PGA)

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Search Information

36809 El Camino Dr, Palmdale, CA 93551, USA Address:

34.54952240000001, -118.1326806 Coordinates:

Elevation: 2925 ft

2021-04-09T16:20:57.078Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: IV

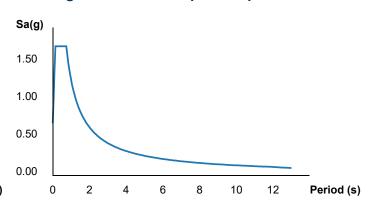
Site Class:

2925 ft wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum

Sa(g) 2.50 2.00 1.50 1.00 0.50 0.00 0 10 12 Period (s)

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.571	MCE _R ground motion (period=0.2s)
S ₁	1.27	MCE _R ground motion (period=1.0s)
S _{MS}	2.571	Site-modified spectral acceleration value
S _{M1}	1.905	Site-modified spectral acceleration value
S _{DS}	1.714	Numeric seismic design value at 0.2s SA
S _{D1}	1.27	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.916	Coefficient of risk (0.2s)

1 of 2 4/9/2021, 10:21 AM

CR ₁	0.904	Coefficient of risk (1.0s)
PGA	0.986	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.986	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.426	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.74	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.571	Factored deterministic acceleration value (0.2s)
S1RT	1.613	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.783	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.27	Factored deterministic acceleration value (1.0s)
PGAd	0.986	Factored deterministic acceleration value (PGA)

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Search Information

Coordinates: 34.53840630847815, -118.13288506137695

Elevation: 3359 ft

Timestamp: 2021-04-09T20:04:43.993Z

Hazard Type: Seismic

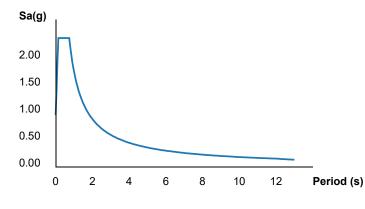
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

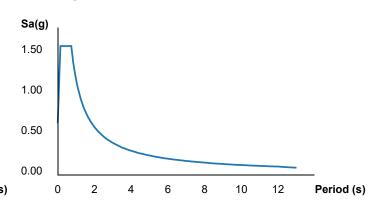
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.375	MCE _R ground motion (period=0.2s)
S ₁	1.171	MCE _R ground motion (period=1.0s)
S _{MS}	2.375	Site-modified spectral acceleration value
S _{M1}	1.756	Site-modified spectral acceleration value
S _{DS}	1.583	Numeric seismic design value at 0.2s SA
S _{D1}	1.171	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _V	1.5	Site amplification factor at 1.0s
CRS	0.925	Coefficient of risk (0.2s)
CR ₁	0.908	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 2:04 PM

PGA	0.917	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.917	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.236	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.499	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.375	Factored deterministic acceleration value (0.2s)
S1RT	1.505	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.657	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.171	Factored deterministic acceleration value (1.0s)
PGAd	0.917	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:04 PM



Search Information

34.56128566737895, -118.12898168848265 Coordinates:

Elevation: 2924 ft

Timestamp: 2021-04-09T20:40:24.218Z

Hazard Type: Seismic

ASCE7-10 Reference

Document:

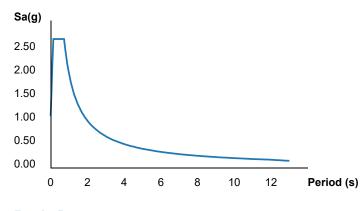
Risk Category: IV

Site Class: D

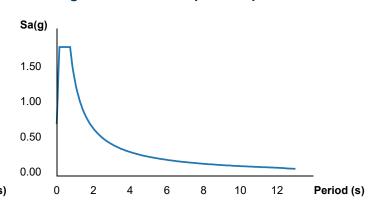
2924 ft Map data ©2021 Imagery ©2021, CNES / Airbus, Maxar Technologies, U.S.

Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.733	MCE _R ground motion (period=0.2s)
S ₁	1.331	MCE _R ground motion (period=1.0s)
S _{MS}	2.733	Site-modified spectral acceleration value
S _{M1}	1.997	Site-modified spectral acceleration value
S _{DS}	1.822	Numeric seismic design value at 0.2s SA
S _{D1}	1.331	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CRS	0.92	Coefficient of risk (0.2s)
CR ₁	0.904	Coefficient of risk (1.0s)

4/9/2021, 2:40 PM 1 of 2

PGA	1.055	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.055	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	3.306	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.594	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.733	Factored deterministic acceleration value (0.2s)
S1RT	1.547	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.71	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.331	Factored deterministic acceleration value (1.0s)
PGAd	1.055	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:40 PM

Search Information

34547 Address:

34.538438, -118.132863 Coordinates:

Elevation: 3360 ft

2021-04-08T22:06:10.243Z Timestamp:

Hazard Type: Seismic

Reference ASCE7-10

Document:

Risk Category: Ш

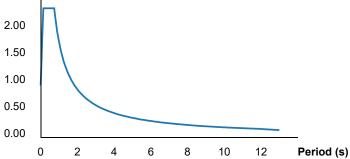
Site Class:

3360 ft

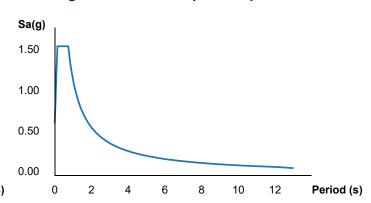
wan data ©2021 Imagery ©2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

MCER Horizontal Response Spectrum

Sa(g)



Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.376	MCE _R ground motion (period=0.2s)
S ₁	1.171	MCE _R ground motion (period=1.0s)
S _{MS}	2.376	Site-modified spectral acceleration value
S _{M1}	1.757	Site-modified spectral acceleration value
S _{DS}	1.584	Numeric seismic design value at 0.2s SA
S _{D1}	1.171	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.925	Coefficient of risk (0.2s)

4/8/2021, 4:06 PM 1 of 2

CR ₁	0.908	Coefficient of risk (1.0s)
PGA	0.917	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.917	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.236	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.5	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.376	Factored deterministic acceleration value (0.2s)
S1RT	1.505	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.657	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.171	Factored deterministic acceleration value (1.0s)
PGAd	0.917	Factored deterministic acceleration value (PGA)

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2 of 2 4/8/2021, 4:06 PM

Search Information

Coordinates: 34.598759799594845, -118.09844223112182

Elevation: 2583 ft

Timestamp: 2021-04-09T20:48:48.917Z

Hazard Type: Seismic

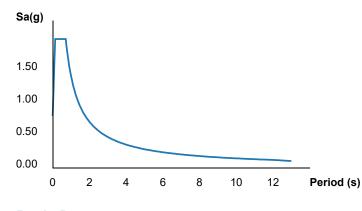
Reference ASCE7-10

Document:

Risk Category: IV

Site Class: D

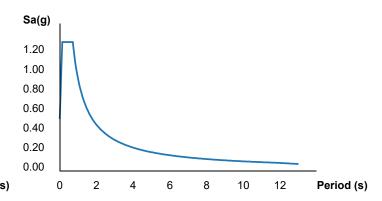
MCER Horizontal Response Spectrum





Map data ©2021 Imagery ©2021 , CNES / Airbus, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	1.971	MCE _R ground motion (period=0.2s)
S ₁	0.937	MCE _R ground motion (period=1.0s)
S _{MS}	1.971	Site-modified spectral acceleration value
S _{M1}	1.406	Site-modified spectral acceleration value
S _{DS}	1.314	Numeric seismic design value at 0.2s SA
S _{D1}	0.937	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	F	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.937	Coefficient of risk (0.2s)
CR ₁	0.911	Coefficient of risk (1.0s)

1 of 2 4/9/2021, 2:48 PM

PGA	0.77	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	0.77	Site modified peak ground acceleration
T _L	12	Long-period transition period (s)
SsRT	2.602	Probabilistic risk-targeted ground motion (0.2s)
SsUH	2.776	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	1.971	Factored deterministic acceleration value (0.2s)
S1RT	1.168	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.282	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	0.937	Factored deterministic acceleration value (1.0s)
PGAd	0.77	Factored deterministic acceleration value (PGA)

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2 of 2 4/9/2021, 2:48 PM

Search Information

Address: 1036 Barrel Spring Road palmdale, ca

Coordinates: 34.5457226, -118.1085956

Elevation: 2817 ft

Timestamp: 2021-05-04T20:11:47.998Z

Hazard Type: Seismic

Reference

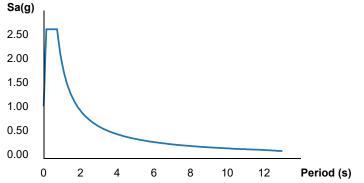
ASCE7-10

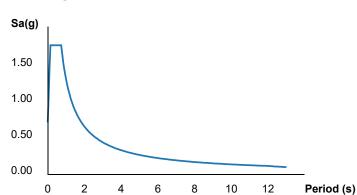
Document:

Risk Category:

Site Class: D

MCER Horizontal Response Spectrum Design Horizontal Response Spectrum





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E Barrel Springs Rd

Basic Parameters

Name	Value	Description
S _S	2.674	MCE _R ground motion (period=0.2s)
S ₁	1.311	MCE _R ground motion (period=1.0s)
S _{MS}	2.674	Site-modified spectral acceleration value
S _{M1}	1.967	Site-modified spectral acceleration value
S _{DS}	1.782	Numeric seismic design value at 0.2s SA
S _{D1}	1.311	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.919	Coefficient of risk (0.2s)

1 of 2 5/4/2021, 2:13 PM

CR ₁	0.902	Coefficient of risk (1.0s)
PGA	1.029	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.029	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.49	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.799	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.674	Factored deterministic acceleration value (0.2s)
S1RT	1.643	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.821	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.311	Factored deterministic acceleration value (1.0s)
PGAd	1.029	Factored deterministic acceleration value (PGA)

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2 of 2 5/4/2021, 2:13 PM

Search Information

Address: 15 4640 Barrel Spring Road palmdale, ca

Coordinates: 34.5268275, -118.0540864

Elevation: 3036 ft

Timestamp: 2021-05-04T20:14:23.952Z

Hazard Type: Seismic

Reference ASCE7-10

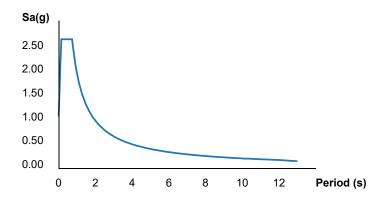
Document:

Risk Category:

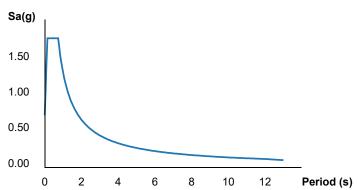
Site Class: D

3036 ft 3036 ft Religion Religion Ballely Common data © 2021 Imagery © 2021, Maxar Technologies, U.S. Geological Survey, USDA Farm Service Agency

Design Horizontal Response Spectrum



MCER Horizontal Response Spectrum



Basic Parameters

Name	Value	Description
S _S	2.7	MCE _R ground motion (period=0.2s)
S ₁	1.323	MCE _R ground motion (period=1.0s)
S _{MS}	2.7	Site-modified spectral acceleration value
S _{M1}	1.984	Site-modified spectral acceleration value
S _{DS}	1.8	Numeric seismic design value at 0.2s SA
S _{D1}	1.323	Numeric seismic design value at 1.0s SA

▼Additional Information

Name	Value	Description
SDC	E	Seismic design category
Fa	1	Site amplification factor at 0.2s
F _v	1.5	Site amplification factor at 1.0s
CR _S	0.924	Coefficient of risk (0.2s)

1 of 2 5/4/2021, 2:14 PM

CR ₁	0.905	Coefficient of risk (1.0s)
PGA	1.04	MCE _G peak ground acceleration
F _{PGA}	1	Site amplification factor at PGA
PGA _M	1.04	Site modified peak ground acceleration
TL	12	Long-period transition period (s)
SsRT	3.149	Probabilistic risk-targeted ground motion (0.2s)
SsUH	3.409	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	2.7	Factored deterministic acceleration value (0.2s)
S1RT	1.464	Probabilistic risk-targeted ground motion (1.0s)
S1UH	1.617	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.323	Factored deterministic acceleration value (1.0s)
PGAd	1.04	Factored deterministic acceleration value (PGA)

Disclaimer

Hazard loads are provided by the U.S. Geological Survey Seismic Design Web Services.

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